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ENDO ATMOSPHERIC-EXO ATMOSPHERIC RADAR MODELING. APPENDICES, A---ETC(U)  
JUN 76 'R J HANCOCK, F H CLEVELAND F30602-73-C-0380

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Final Technical Report  
June 1976



ENDO ATMOSPHERIC-EXO ATMOSPHERIC RADAR MODELING  
(Appendices A-K, M)

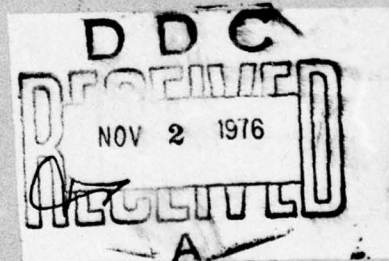
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ROME AIR DEVELOPMENT CENTER  
AIR FORCE SYSTEMS COMMAND  
GRIFFISS AIR FORCE BASE, NEW YORK 13441



ENDO ATMOSPHERIC-EXO ATMOSPHERIC RADAR MODELING  
(APPENDICES A-K M)



This report has been reviewed by the RADC Information Office (OI) and is releasable to the National Technical Information Service (NTIS). At NTIS it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This effort is concerned with the development and implementation of a set of digital computer programs that will augment the RADC digital computer radar simulation model procured under Contr F30602-72-C-0393 (01707201). The computer programs shall consist of a sequence of subroutines that correspond to separate functions such as a chaff model, target model, propagation effects and clutter model. The original radar simulation model will be expanded to include a bistatic capability and will include ECM and phase coded pulse compression		

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receiver techniques. In addition, an interactive system has been designed for the simulation. Using an interactive display, an engineer would be able to understand what is happening by being able to observe results at several intermediate points in the problem. A picture is worth a thousand words. For example, an antenna pattern or waveform response to a target is more meaningful than a long table of numerical listings. Parts of the simulation were used by RADC for Deep Space Surveillance Radar (DSSR) waveform analysis, generating antenna patterns and tradeoffs involving phase shifter bit-size for the Advanced Space Defense Program (ASDP). The RADC radar simulation model is being used to support Seek Sail, Cobra Judy, Digital Coded Radar and Seek Sentry.

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This report contains Vol I, Pt 1 (Sections 1-7 and 9-10) (Pages 1-1 thru 1-5, 2-1 thru 2-24, 3-1 thru 3-35, 4-1 thru 4-23, 5-1 thru 5-6, 6-1 thru 6-39, 7-1 thru 7-30, 9-1 thru 9-3 and 10-1 thru 10-2).

Vol I, Pt 2 contains Section 8 (Pages 8-1 thru 8-174).

Vol I, Pt 3 contains Section 8 (Pages 8-175 thru 8-418).

Vol II, Pt 1 contains (Sections 1-8 and 10 & 11) (Pages 1-1, 2-1 thru 2-24, 3-1 thru 3-15, 4-1 thru 4-137, 5-1 thru 5-16, 6-1 thru 6-44, 7-1, 8-1 thru 8-26, 10-1 thru 10-4 and 11-1 thru 11-2).

Vol II, Pt 2 contains Sections 9 and 10 (Pages 9-1 thru 9-234 and Pages 10-1 thru 10-4).

Vol III contains Sections 1 thru 6 (Pages 1-1 thru 1-2, 2-1 thru 2-22, 3-1 thru 3-53, 4-1 thru 4-141, 5-1 thru 5-3 and 6-1).

Vol IV, Pt 1 contains Appendices A-K and Appendix M.

Vol IV, Pt 2 contains Appendix L.

BECAUSE THIS DOCUMENT IS A COMPUTER SOFTWARE PROGRAM MANY CONSECUTIVE PAGES CONTAIN ILLEGIBLE AREAS WITH VERY MINOR (1, 2 or 3 LINES) CHANGES FROM ONE PAGE TO THE NEXT. FOR THAT REASON THE OVERALL VALUE OF THE PROGRAM AFTER CONSIDERING THE LOSS OF THE ILLEGIBLE PAGES IS NOT DEGRADED TO ANY DEGREE AND THE SOFTWARE PROGRAM REMAINS CLEARLY UNDERSTANDABLE. FOR CLARIFICATION OF ANY PORTION, CONTACT RADC/OCSA.

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# APPENDIX A GLOSSARY OF ABBREVIATIONS AND SYMBOLS

CARDIN	- TSS subsystem which allows submission of batch jobs from a remote terminal.
CFG	- Simulation configuration
CPU	- Central Processor Unit. The central and arithmetic portion of a computer.
$\delta(t-t_i)$	- Dirac delta function. Unit impulse at time equal to $t_i$
DFT	- Discrete Fourier Transform
DSRN	- Data Set Reference Number
ECM	- Electronic Counter Measures
ECCM	- Electronic Counter Counter Measures
EDITOR	- TSS subsystem which facilitates modification or correction of TSS files
$F[ ]$	- Fourier transform operator
$F^{-1}[ ]$	- Inverse Fourier transform operator
FFT	- Fast Fourier Transform algorithm
GCOS	- Honeywell General Comprehensive Operating Supervisor
GHz (Gc)	- Gigahertz
$H[ ]$	- Hilbert transform operator
HIS 635	- Honeywell/GE 635 computer system
IF	- Intermediate Frequency
LSB	- Least Significant Bit

LTI	- Linear Time Invariant
MCC	- Module Classification Code
MRN	- Module Reference Number
MSB	- Most Significant Bit
MTI	- Moving Target Indication
ns (or NS)	- nanosecond ( $10^{-9}$ second)
PASS	- Pass through a simulation configuration
PRMFL	- Permanent disc storage file
RADSIM	- Radar System Simulation Model
RCS	- Radar Cross Section
RF	- Radio (Radiated) Frequency
RV	- Reentry Vehicle
STF	- Stimulus/Transfer Function
$s^*(t)$ or $S^*(f)$	- Complex conjugate of $s(t)$ or $S(f)$
$s_*(t)$	- A function composed of samples of $s(t)$
$S_*(f)$	- The Fourier transform of a sampled function, such as $s_*(t)$
$\hat{s}(t)$	- Hilbert transform of $s(t)$
$S_+(f)$	- Positive frequency components of the signal $s(t)$
$S_-(f)$	- Negative frequency components of the signal $s(t)$
$s_+(t)$	- The function of time which corresponds to the positive frequency components of $s(t)$

- $s_{-}(t)$  - The function of time which corresponds to the negative frequency components of  $s(t)$
- $s_I(t)$  - In-phase video channel representation of the bandlimited signal  $s(t)$
- $s_Q(t)$  - Quadrature video channel representation of the bandlimited signal  $s(t)$
- TSS - Time-sharing system



A P P E N D I X    B

S O F T W A R E   M O D U L E S   U S E D   I N

T H E   R A D A R   S I M U L A T I O N   M O D E L

The software modules used in the radar simulation module are listed herein by module name and by reference number.

B.1   S O F T W A R E   M O D U L E S   L I S T E D   B Y   M O D U L E   N A M E

The following table includes all of the software modules listed in alphabetical order by module name. Column headings in the list are defined as follows:

1.    Module Ref. Number: This is the number by which the module is called in any system model program.
2.    Input: Locations where input data to module must be located before execution.
3.    Output: These are the locations where output data is placed.
4.    Subroutine Name: This column contains a list of subroutines used by module.
5.    Subroutine PRMFL: This column contains a list of the permanent file where the subroutine is located. This file must be loaded in any system model program that uses module.
6.    System Parameters: The system parameters are constants that are used in the module and are defined by module number 301, (SYS). Parameters are described in Appendix C.
7.    Module Parameters: Module parameters are constants that are used in module and are defined in a namelist immediately following the module call in the system model program.
8.    Comments: This column is provided for a short term description of the module.

Table B.1-1 SOFTWARE MODULES LISTED BY MODULE NAME

MODULE		ARGUMENTS		SUBROUTINES & SYMKEYS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
ADDA	207	XT,XA	XT	CONV	OMISC1	-	-	-	-	ARRAY ADDITION
ADDA	239	YT,XB	YT	CONV	OMISC1	-	-	-	-	ARRAY ADDITION
ADDRND	235	XT	XT	RNDARY RRAND	OSUP2 OSUP1	-	-	NTYPER	45	ADD SAMPLES OF RANDOM DISTRIBUTION TO XT
ADDRND	236	YT	YT	RNDARY RRAND	OSUP2 OSUP1	-	-	NTYPER	45	ADD SAMPLES OF RANDOM DISTRIBUTION TO YT
ADDRND	237	XT,YT	XT,YT	RNDARY RRAND	OSUP2 OSUP1	-	-	NTYPER	45	ADD SAMPLES OF RANDOM DISTRIBUTION TO XT+YT
ANTARY	413	--	XT,YT	ANTARY	OANT1	N2 RFF0	1 3	RFF0 IDDUIMP NTSAR DX THETAS NR0WS NRPSCG IRPSCG NRPSR IRPSR NPULS TSRLDS(1)	3 21 76 77 78 79 80 81 82 83 85 401	PHASED ARRAY ANTENNA  Narrow Bandwidth Waveforms
ANTPAT	504	--	XT,YT	ANTARY ZFFT	OANT1 OZFFT	N2 RFF0	1 3	RFF0 IDDUIMP NTSAR DX THETAS NR0WS NRPSCG IRPSCG NRPSR IRPSR INORM NPULS TSRLDS(1)	3 21 76 77 78 79 80 81 82 83 84 85 401	PHASED ARRAY FAR FIELD PATTERN GENERATION Output independent variable = Sine 8  Narrow bandwidth waveforms
ATOD	216	XT	IXT	ATOD	ODFIN	-	-	XLSB NBITS IROFF ADCS	103 104 105 149	ANALOG TO DIGITAL CONVERTER
ATOD	217	YT	IYT	ATOD	ODFIN	-	-	XLSB NBITS IROFF ADCS	103 104 105 149	ANALOG TO DIGITAL CONVERTER

MODULE	ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
	NAME	#	INPUT	OUTPUT	NAME	LOC	NAME	LOC	
CDFNCL	404		XT,YT	XT,YT	-	-	FFR FFI FBR FBI	68 69 70 71	DIGITAL FILTER-COMPLEX Storage registers not zeroed
CDIGFL	403		XT,YT	XT,YT	-	-	FFR FFI FBR FBI	68 69 70 71	DIGITAL FILTER-COMPLEX Storage registers zeroed
CFAR	459		XT	XA	TI	12	TAUG	198	CONSTANT FALSE ALARM RATE PROCESSOR
CFAR	460		YT	XB	TI	12	TAUG	198	CONSTANT FALSE ALARM RATE PROCESSOR
CGEN	425		--	XT,YT (XA)*	RFF0 SINF0 TI	3 8 12	RFF0 IDDUMP DX THETAS NRWS NBPSCG IRPSCG NPULS NCGPLS TCGNOM FMBW NFWTX RISTIM FALTIM TIMLSB WTX(I,J)	3 21 77 78 79 80 81 85 88 89 93 94 98 99 115 201	TSAR CONTROL GENERATOR * Array XA used for scratch storage
CGENCW	455		--	XT,YT	RFF0 SINF0	3 8	DX THETAS NRWS TCGNOM	77 78 79 89	FSAR CONTROL GENERATOR FOR FREQUENCY SCANNED PHASED ARRAY
CGENSF	453		--	XT,YT	RFF0 SINF0	3 8	RFF0 DX THETAS NRWS NCGPLS TCGNOM	3 77 78 79 88 89	CONTROL GENERATOR - BURST Pulse to pulse phase shift deleted
CLINT	302		--	--	TI LAMBDA RNGCEL	12 13 14	RNGCEL IDDUMP NRCS RMPH WINDVEL VELANG	14 21 46 48 49 50	CLUTTER MODEL INITIALIZER



MODULE	ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS	
	NAME	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME		LOC
CLINT(cont.)										
CLUTTR	503	--	XT,YT (XB)*	CLUTTR AZGAIN ELGAIN	OTGCL OSUP2 OSUP2	TIME FS RNGCEL TI	16 2 14 12	RNEXT RN0 AZEXT AZ0 MM ELEXT EL0 NN	51 52 53 54 55 56 57 58	CLUTTER MODEL (Initialized by CLINT) * Array XB used for scratch storage
CUMDIS	208	XT	XA	CUMDIS	OSUP2	-	-	TLIM BLIM NHIST NCPACK NDPACK	39 40 41 42 43	HISTOGRAM GENERATION
CUMDIS	209	YT	XA	CUMDIS	OSUP2	-	-	TLIM BLIM NHIST NCPACK NDPACK	39 40 41 42 43	HISTOGRAM GENERATION
CONV	204	XT,YT, XA,XB	XT,YT	CONV	OMISC1	-	-	-	-	ARRAY MULTIPLICATION Complex rectangular
CONVMP	205	XT,YT, XA,XB	XT,YT	CONV	OMISC1	-	-	-	-	ARRAY MULTIPLICATION Complex polar
(DATA XFER)	114	XT,YT	XA,XB	DBLKX	OSUP1	-	-	-	-	
(DATA XFER)	115	XA,XB	XT,YT	DBLKX	OSUP1	-	-	-	-	
DCFAR	440	IXT	IXT	DCFAR	ODFIN	-	-	NCELL	170	DIGITAL CFAR VIDEO PROCESSOR
DCFAR	441	IYT	IYT	DCFAR	ODFIN	-	-	NCELL	170	DIGITAL CFAR VIDEO PROCESSOR
DFT	201	--	XT,YT	DFT	OMISC2	NORMFT FI TI SIMBW	9 11 12 4	SIMBW IDDUMP NIMP DFTIN(I,J)	4 21 200 201	DISCRETE FOURIER TRANSFORM Video data

MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
DFTF0	234	--	XT,YT	DFT	OMISC2	NORMFT FI TI SIMBW SIMF0	9 11 12 4 8	SIMBW SIMF0 IDDUIMP NIMP DFTIN(I,J)	4 8 21 200 201	DISCRETE FOURIER TRANSFORM Intermediate Frequency(IF) data
DFTRF	233	-	XT,YT	DFT	OMISC1	NORMFT FI TI SIMBW RFF0	9 11 12 4 3	RFF0 SIMBW IDDUIMP NIMP DFTIN(I,J)	3 4 21 200 201	DISCRETE FOURIER TRANSFORM Radio Frequency(RF) data
DIGFSF	463	XT,YT	XT,YT	DIGFSF	ODFIN	-	-	RADIUS NSAM NDFZ FSAM(I,J)	195 196 197 201	DIGITAL FILTER-FREQUENCY SAMPLING DESIGN Low Pass filter only
DIGFIL	461	XT,YT	XT,YT	DIGFIL	ODFIN	-	-	SF NSEC FRCOEF(I,J) FFCOEF(I,J)	74 199 201 251	DIGITAL FILTER-MULTIPLE SECTION Storage registers zeroed
DIGFNC	462	XT,YT	XT,YT	DIGFIL	ODFIN	-	-	SF NSEC FRCOEF(I,J) FFCOEF(I,J)	74 199 201 251	DIGITAL FILTER-MULTIPLE SECTION Storage registers not zeroed
DIGTFL	422	IXT	IXT	DIGTFL	ODFIN	-	-	NTAPS ITAP(I,J)	101 201	DIGITAL TRANSVERSAL FILTER
DIGTFL	423	IYT	IYT	DIGTFL	ODFIN	-	-	NTAPS ITAP(I,J)	101 201	DIGITAL TRANSVERSAL FILTER
DIVA	206	XT,YT, XA,XB	XT,YT	CONV	OMISC1	-	-	-	-	COMPLEX POLAR ARRAY DIVISION
DTOA	218	IXT	XT	ATOD	ODFIN	-	-	-	-	DIGITAL TO ANALOG CONVERSION
DTOA	219	IYT	YT	ATOD	ODFIN	-	-	-	-	DIGITAL TO ANALOG CONVERSION
DTOA	220	IYT	XA	ATOD	ODFIN	-	-	-	-	DIGITAL TO ANALOG CONVERSION
DTOA	228	IXT	XA	ATOD	ODFIN	-	-	-	-	DIGITAL TO ANALOG CONVERSION
ECM	512	XT,YT	XT,YT	ECM DIGFSF	ODFIN ODFIN	N2 TIME	1 16	JVEL JPEROD JRNJ JRSIM JMAY	156 157 171 172 173	NOISE JAMMER

MODULE	ARGUMENTS		SUBROUTINES & SYNTAXES REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
	NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	
EUR(cont.)									
ERGYCF		118	XT,YT	SYSOUT		OMTSC1	-	JGJT JERF JFMRW JPW JF0 RADIUS NSAM NDFZ FSAM(I,J)	174 175 176 177 178 195 196 197 201 -
ERGYRE		116	XT	SYSOUT		OMTSC1	-	-	-
ERGYRE		117	YT	SYSOUT		OMTSC1	-	-	-
FGERMP		421	--	XT,YT		OXMR2	N2 FS TI SINF0 NORMFT	1 2 12 8 9	8 21 90 93 94 95 96 97 98 99 100 201 451 92 129 91
FGENXY		420	--	XT,YT		OXMR2	N2 FS TI SINF0 NORMFT	1 2 12 8 9	8 21 90 93 94 95 96 97 98 99 100 201 451 92 129 91



MODULE	ARGUMENTS		SUBROUTINES & SYMPREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
	NAME	LOC	NAME	LOC	NAME	LOC	NAME	LOC	
FILT	407	XT,YT	FILT	OMISC1	-	-	NZ NP SF FZERO(I,J) FPOLE(I,J)	72 73 74 201 301	TRANSFER FUNCTION SPECIFIED IN S-PLANE
FILT	408	XA,XB	FILT	OMISC1	-	-	NZ NP SF FZERO(I,J) FPOLE(I,J)	72 73 74 201 301	TRANSFER FUNCTION SPECIFIED IN S-PLANE
FWDET	416	XT	HWDET	OMISC2	-	-	-	-	FULL-WAVE DETECTOR
FWDET	417	YT	HWDET	OMISC2	-	-	-	-	FULL-WAVE DETECTOR
HLIM	438	XT	HWDET	OMISC2	-	-	-	-	HARD LIMITER
HLIM	439	YT	HWDET	OMISC2	-	-	-	-	HARD LIMITER
HWDET	414	XT	HWDET	OMISC2	-	-	-	-	HALF-WAVE DETECTOR
HWDET	415	YT	HWDET	OMISC2	-	-	-	-	HALF-WAVE DETECTOR
IFWDET	447	IXT	HWDET	OMISC2	-	-	-	-	DIGITAL FULL-WAVE DETECTOR
IFWDET	448	IYT	HWDET	OMISC2	-	-	-	-	DIGITAL FULL-WAVE DETECTOR
IHLIM	442	IXT	HWDET	OMISC2	-	-	-	-	DIGITAL HARD LIMITER
IHLIM	443	IYT	HWDET	OMISC2	-	-	-	-	DIGITAL HARD LIMITER
IHWDET	445	IXT	HWDET	OMISC2	-	-	-	-	DIGITAL HALF-WAVE DETECTOR
IHWDET	446	IYT	HWDET	OMISC2	-	-	-	-	DIGITAL HALF-WAVE DETECTOR
INGTOR	409	XT	INGTOR	ODFIN	-	-	FBCK	75	INTEGRATOR
INGTOR	410	YT	INGTOR	ODFIN	-	-	FBCK	75	INTEGRATOR
IONOS	511	XT,YT	IONOS	OTGCL	RFF0	3	SEDENS	148	IONOSPHERIC DISPERSION EFFECTS
ISQDET	449	IXT	HWDET	OMISC2	-	-	-	-	DIGITAL SQUARE LAW DEVICE
ISQDET	450	IYT	HWDET	OMISC2	-	-	-	-	DIGITAL SQUARE LAW DEVICE
LAMPFCP	458	XT,YT	LAMPFCP	OMISC1	-	-	GAIN	145	LINEAR AMPLIFIER
LAMPRE	456	XT	LAMPFCP	OMISC1	-	-	GAIN	145	LINEAR AMPLIFIER

MODULE	NAME	ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
		INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
LAMPRE	457	YT	YT	LAMPFC	OMISC1	-	-	GAIN	145	LINEAR AMPLIFIER
	430	XT or IXT*	XT or IXT*	MTIFLT	ODIG	-	-	FF0	68	DOUBLE DELAY MTI FILTER Delay line storage zeroed * XT used for MODEDF=1 (Floating point arithmetic) IXT used for MODEDF=2 (Integer arithmetic)
								FF1	69	
								FB1	70	
MTIFLT								FB2	71	
								IFF0N	160	
								IFF0D	161	
								IFF1N	162	
								IFF1D	163	
								IFB1N	164	
								IFB1D	165	
								IFB2N	166	
								IFB2D	167	
								MODEDF	168	
								NBITDF	169	
								FF0	68	DOUBLE DELAY MTI FILTER Delay line storage zeroed * YT used for MODEDF=1 (Floating point arithmetic) IYT used for MODEDF=2 (Integer arithmetic)
								FF1	69	
								FB1	70	
								FB2	71	
MTINCL								IFF0N	160	
								IFF0D	161	
								IFF1N	162	
								IFF1D	163	
								IFB1N	164	
								IFB1D	165	
								IFB2N	166	
								IFB2D	167	
								MODEDF	168	
								NBITDF	169	
								FF0	68	DOUBLE DELAY MTI FILTER Delay line storage not zeroed * XT used for MODEDF=1 (Floating point arithmetic) IXT used for MODEDF=2 (Integer arithmetic)
								FF1	69	
								FB1	70	
								FB2	71	
								IFF0N	160	
								IFF0D	161	
								IFF1N	162	
								IFF1D	163	
								IFB1N	164	
								IFB1D	165	
								IFB2N	166	
								IFB2D	167	
								MODEDF	168	
								NBITDF	169	





MODULE		Arguments		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
PHENC(cont.)										
PHENC	507	-	XT,YT	PHENC FGENXY	DXMTR1 DXMTR2	N2 FS TI SIMF0 NORMFT	1 2 12 8 9	NSR MODEPH IFY(I) ICORE CHIRP FSIRT SPW NSURF SWTIM TSTART SIMF0 VPEAK RISTIM FALTIM	184 183 186 194 92 91 95 96 97 100 8 129 98 99	PHASE ENCODED TRANSMITTER Complex polar output
PLOTTR	307	XT	PRMFL OR MAG TAPE	PLOTTR	OFLOTS	-	-	ST RNG NSKP IFCODE VIL(I) VDL(I) GLBL(I)	59 60 63 113 201 251 301	OUTPUT DATA FOR OFF-LINE PLOTTER Floating point format
PLOTTR	308	YT	PRMFL OR MAG TAPE	PLOTTR	OFLOTS	-	-	ST RNG NSKP IFCODE VIL(I) VDL(I) GLBL(I)	59 60 63 113 201 251 301	OUTPUT DATA FOR OFF-LINE PLOTTER Floating point format
PLOTTR	309	XA	PRMFL OR MAG TAPE	PLOTTR	OFLOTS	-	-	ST RNG NSKP IFCODE VIL(I) VDL(I) GLBL(I)	59 60 63 113 201 251 301	OUTPUT DATA FOR OFF-LINE PLOTTER Floating point format

MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INFUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
PLOTR	310	XB	PRMFL OR MAG TAPE	PLOTR	OPLOTS	-	-	ST RNG NSKP IFCODE VIL(1) VDL(1) GLRL(1)	59 60 63 113 201 251 301	OUTPUT DATA FOR OFF-LINE PLOTTER Floating point format
PLTFMT	113	XT,YT	XA	PLTFMT	OPLOTS	-	-	ADLT ASTRT ASTOP	33 34 35	TRANSFORMATION OF DATA IN SINE SPACE TO ANGLE SPACE Output data in dB
PTLIST	303	XT	PRMFL	PTLIST	OPLOTS	-	-	ST RNG LF NSKP NAUTO TH TL IFCODE VDL(1)	59 60 62 63 64 65 66 113 251	OUTPUT DATA FOR OFF-LINE PLOTTER Integer format-13 Bit accuracy
PTLIST	304	YT	PRMFL	PTLIST	OPLOTS	-	-	ST RNG LF NSKP NAUTO TH TL IFCODE VDL(1)	59 60 62 63 64 65 66 113 251	OUTPUT DATA FOR OFF-LINE PLOTTER Integer format-13 Bit accuracy
PTLIST	305	XA	PRMFL	PTLIST	OPLOTS	-	-	ST RNG LF NSKP NAUTO TH TL IFCODE VDL(1)	59 60 62 63 64 65 66 113 251	OUTPUT DATA FOR OFF-LINE PLOTTER Integer format-13 Bit accuracy
PTLIST	306	XB	PRMFL	PTLIST	OPLOTS	-	-	ST RNG LF NSKP NAUTO TH TL	59 60 62 63 64 65 66	OUTPUT DATA FOR OFF-LINE PLOTTER Integer format-13 Bit accuracy

MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
PTLIST(cont.)								IFCODE VUL(1)	113 251	
PXFRM	454	--	XT,YT	PXFRM	OTSAR1	SIMBW FI SIMF0	4 11 8	SIMF0 SFV ASUBF BPRI	8 95 96 114	FOURIER TRANSFORM OF SINGLE PULSE OF MULTIPLE PULSE BURST Closed form solution
RDENCL	406	XT,YT	XT,YT	RDIGFL	ODFIN	-	-	FF0 FF1 FB1 FB2	68 69 70 71	DIGITAL FILTER-REAL Storage registers not zeroed
RDIGFL	405	XT,YT	XT,YT	RDIGFL	ODFIN	-	-	FF0 FF1 FB1 FB2	68 69 70 71	DIGITAL FILTER-REAL Storage registers zeroed
RECF	451	XT,YT XA,XB *	XT,YT	RECF DFT	OTSAR1 OMISC2	-	-	FBCK DX NR0WS RECDL RECIRT THETAR	75 77 79 117 118 119	TSAR RECEIVER PROCESSOR * XA and XB are used for temporary storage
RECFTF	452	--	XT,YT	RECF DFT	OTSAR1 OMISC2	-	-	FBCK DX NR0WS RECDL RECIRT THETAR	75 77 79 117 118 119	TSAR RECEIVER PROCESSOR TRANSFER FUNCTION
RNDARY	214	--	XT	RNDARY	OSUP2	-	-	NRNDPT NTYPER	44 45	LOADS ARRAY WITH RANDOM NUMBERS
RNDARY	215	--	YT	RNDARY	OSUP2	-	-	NRNDPT NTYPER	44 45	LOADS ARRAY WITH RANDOM NUMBERS
RRAND	101	--	--	RRAND	OSUP1	-	-	IRND IADD1 JRND UMEAN UEXT XMEAN SIGMA NRAND(1)	22 23 24 25 26 27 28 201	EXECUTION OF MODULE NUMBER 101 INITIALIZES THE RANDOM NUMBER GENERATOR



MODULE	ARGUMENTS		SUBROUTINES & SYMBOLES REQUIRED		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
	NAME	INPUT	OUTPUT	NAME	NAME	LOC	NAME	LOC	
KRAND	102	—	—	KRAND	OSUF1	—	UMCAN UEXT XMEAN SIGMA	25 26 27 28	SAME AS 101 EXCEPT ONLY DISTRIBUTION PARAMETERS ARE INITIALIZED
KSHIFT	229	XT,YT	XT,YT	SHIFT	OMISC1	8	SIMF0 SHT0 SHPHAS TJIT	8 180 181 182	WAVEFORM TIME SHIFT WITH JITTER
KSHIFT	230	XT,YT	XA,XB	SHIFT	OMISC1	8	SIMF0 SHT0 SHPHAS TJIT	8 180 181 182	WAVEFORM TIME SHIFT WITH JITTER
RSHIFTS	231	XT,YT	XA,XB	SHIFT	OMISC1	8	SIMF0 SHT0 SHPHAS TJIT	8 180 181 182	WAVEFORM TIME SHIFT WITH JITTER
RSHIFTS	232	XT,YT	XA,XB*	SHIFT	OMISC1	8	SIMF0 SHT0 SHPHAS TJIT	8 180 181 182	WAVEFORM TIME SHIFT WITH JITTER * XA & XB are zeroed prior to execution
RTOPDB	103	XT,YT	XA,XB	RTOPDB	OSUF2	—	—	—	RECTANGULAR TO POLAR CONVERSION Modulus in dB
RTOPM	110	XT,YT	XA,XB	RTOPDB	OSUF2	—	—	—	RECTANGULAR TO POLAR CONVERSION Modulus in linear units
RTOPM2	111	XT,YT	XA,XB	RTOPDB	OSUF2	—	—	—	RECTANGULAR TO POLAR CONVERSION Modulus in squared units
SCANNER	313	XA	SYSOUT	SCANNER	OANT2	—	—	—	DATA SCANNER (determines main lobe and side lobe parameters)
SHIFT	224	XT,YT	XT,YT	SHIFT	OMISC1	8	SIMF0 SHT0 SHPHAS	8 180 181	WAVEFORM TIME SHIFT
SHIFT	225	XT,YT	XA,XB	SHIFT	OMISC1	8	SHT0 SHPHAS SIMF0	180 181 8	WAVEFORM TIME SHIFT
SHIFTS	226	XT,YT	XA,XB	SHIFT	OMISC1	8	SHT0 SHPHAS SIMF0	180 181 8	WAVEFORM TIME SHIFT

MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
SHIFTS	227	XT, YT	XA, XB*	SHIFT	OMISC1	SIMF0	8	SH0 SHPHAS SIMF0	180 181 8	WAVEFORM TIME SHIFT * XA and XB are zeroed prior to execution
SFCAVG	312	XA	SYSOUT	SFCAVG	OANT2	-	-	-	-	ANTENNA OUTPUT INTEGRATED OVER ALL SPACE
SQDET	418	XT	XT	HUDET	OMISC2	-	-	-	-	SQUARE LAW DETECTOR
SODET	419	YT	YT	HUDET	OMISC2	-	-	-	-	SQUARE LAW DETECTOR
SWPINT	434	XT	XT	SWPINT	ODIG	-	-	FBCK	75	SWEEP INTEGRATOR Delay line storage is zeroed
SWPINT	435	YT	YT	SWPINT	ODIG	-	-	FBCK	75	SWEEP INTEGRATOR Delay line storage is zeroed
(SYS)	301	--	--	MAIN1 MAIN2 AZGAIN ELGAIN ANTINT IPACK RRAND B DATA DBLNX	DLODR OSINEX OSUP2 OSUP2 OMISC2 OSUP1 OSUP1 OSUP1 OSUP1	N2 FS RFF0 SIMBW ISDUMP ICINV ICFOR SIMF0 NORMFT WSCAN FI TI LAMBDA RNGCEL TIME ANTAZ0 ANTEL0 PRI(I) NPRIS IPRIPT NREPET AZBST NPTAZ ELBST NPTL ANTAZ(I,J) ANTEL(I,J)	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 18 20 130 142 143 144 150 151 152 153 201 351		EXECUTION OF MODULE NUMBER 301 INITIALIZES THE SYSTEM PARAMETER TABLE	
TARGET	501	--	XT, YT*	TARGET AZGAIN ELGAIN	OTGCL OSUP2 OSUP2	RFF0 SIMBW SIMF0 FI TIME	3 4 8 11 16	RFF0 IDUMP HTGT RTGT ANGTGT	3 21 106 107 108	TARGET MODEL TRANSFER FUNCTION * XT & YT zeroed before execution

If FS is specified, TI will be computed  
If RFF0 is specified, LAMBDA will be computed

MODULE	NAME	ARGUMENTS		SUBROUTINES & SYMKEYS REF'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
		INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
	TARGET (cont.)							TGINT RSIM NSCAT TGTVEL TSCAT(I,J)	109 110 111 112 201	
	TGINCL	--	XT,YT	TARGET	OTGCL	REF0 SIMBW SIMF0 FI TIME	3 4 8 11 16	REF0 IDUMP HTGT RTGT ANGTGT TGINT RSIM NSCAT TGTVEL TSCAT(I,J)	3 21 106 107 108 109 110 111 112 201	TARGET MODEL TRANSFER FUNCTION
	TSARY	--	XT,YT XA,XB *	TSARY DFT	OTSAR OMISC2	REF0 SIMBW SIMF0 FI	3 4 8 11	REF0 IDUMP NSAR DX THETAS NRDWS NRPSR IRPSR TDLN ANGLE MODTSR RECDL THETAR TDLN TSLRLOS(I)	3 21 76 77 78 79 82 83 86 87 116 117 119 185 401	PHASED ARRAY ANTENNA TRANSFER FUNCTION - INITIAL EXECUTION Wide bandwidth waveforms * XA and XB are used for scratch storage
	TSARY1	--	XT,YT XA,XB *	TSARY DFT	OTSAR OMISC2	REF0 SIMBW SIMF0 FI	3 4 8 11	REF0 IDUMP NSAR DX THETAS NRDWS NRPSR IRPSR TDLN ANGLE MODTSR RECDL THETAR TDLN	3 21 76 77 78 79 82 83 86 87 116 117 119 185	PHASED ARRAY ANTENNA TRANSFER FUNCTION - SUBSEQUENT EXECUTIONS Wide bandwidth waveforms * XA and XB are used for scratch storage



MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
TSRPAT	505	XT,YT	XT,YT XA,XB *	TSRPAT TSARY DFT REF	OTSAR OTSAR OMISC2 OTSAR1	RFF# SIMBW SINF# FI	3 4 8 11	ADEL ASTRT ASTOP FBCK NTSAR DX THETAS NRWS NBPSR IRPSR TDLIN MODISR RECDL RECIR THETAR TDLN TSRLOS(I)	33 34 35 75 76 77 78 79 82 83 86 116 117 118 119 185 401	PHASED ARRAY FAR FIELD PATTERN GENERATION  Wide bandwidth waveforms  * XA and XB are used for scratch storage
WEITCP	222	XT,YT	XT,YT	WEITRE	OMISC1	-	-	NPWT ORIG WT(I,J)	37 38 201	WEIGHTING FUNCTION Rectangular complex on rectangular complex
WEITMF	223	XT,YT	XT,YT	WEITRE	OMISC1	-	-	NPWT ORIG WT(I,J)	37 38 201	WEIGHTING FUNCTION Polar on polar
WEITRE	221	XT,YT	XT,YT	WEITRE	OMISC1	-	-	NPWT ORIG WT(I,J)	37 38 201	WEIGHTING FUNCTION Real on rectangular complex
WVGUID	510	XT,YT	XT,YT	WVGUID	OTGCL	RFF#	3	CFREQ XMLENG	146 147	TRANSFER FUNCTION OF PERFECTLY CONDUCTING WAVEGUIDE
XYTODB	104	XT,YT	XA	RTOPDB	OSUP2	-	-	-	-	RECTANGULAR TO MAGNITUDE CONVERSION Output in dB
XYTODB	108	XT,YT	XT	RTOPDB	OSUP2	-	-	-	-	RECTANGULAR TO MAGNITUDE CONVERSION Output in dB
XYTOM	105	XT,YT	XA	RTOPDB	OSUP2	-	-	-	-	RECTANGULAR TO MAGNITUDE CONVERSION Output in linear units
XYTOM2	106	XT,YT	XA	RTOPDB	OSUP2	-	-	-	-	RECTANGULAR TO MAGNITUDE CONVERSION Output in squared units

MODULE	NAME	ARGUMENTS		SUBROUTINES & SYMKEYS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
		INFILE	OUTFILE	NAME	PRMT	NAME	LOC	NAME	LOC	
ZFFT	202	XT,YT	XT,YT	ZFFT	OZFFT	N2 SIMBW ICINV ICFOR NORMFT	1 4 6 7 9	N2 SIMBW ICINV ICFOR NORMFT FSHIFT	1 4 6 7 9 15	FAST FOURIER TRANSFORM
	203	XT,YT	XT,YT	ZFFT	OZFFT	N2 SIMBW ICINV ICFOR NORMFT	1 4 6 7 9	N2 SIMBW ICINV ICFOR NORMFT FSHIFT	1 4 6 7 9 15	INVERSE FOURIER TRANSFORM
A D D E N D A										
(BISTAT -SYS)	311	--	--	MAIN2	OSIMEX	WSCANB BASLIN ANBAZ0 ANBEL0 NPTAZ AZBST NPTCL ELBST ANTAZ ANTEL	17 19 150 151 321 322 323 324 331 481	-		Bistatic Antenna Initialization
CHAFF	514	--	XT,YT	CHAFF	OCHAFF	RFF0 FEXT FI	3 4 11	NDIPOL CHFRNG CHFHGT CHFAZ DORINT (I,J) DIPLNG DIPDIA	212 213 214 215 321 219 220	Chaff Model XT,YT cleared prior to execution

MODULE		ARGUMENTS		SUBROUTINES & SYMREFS REQ'D		SYSTEM PARAMETERS		MODULE NAMELIST PARAMETERS		COMMENTS
NAME	#	INPUT	OUTPUT	NAME	PRMFL	NAME	LOC	NAME	LOC	
CHAFF	515	XT, YT	XT, YT	CHAFF	0CHAFF*	RFFØ FEXT FI	3 4 11	NDIPOL CHFRNG CHFHGT CHFAZ DORINT (I, J) DIPLNG DIPDIA	212 213 214 215 321 219 220	Chaff Model Transfer functions summed into XT, YT
DIPOLE	464	--	XT, YT	DIPOLE	0CHAFF*	RFFØ FEXT FI	3 4 11	THETAD RHOD TSHFTD DIPLNG DIPDIA	216 217 218 219 220	Thin wire dipole scatterer XT, YT cleared prior to execution
DIPOLE	465	XT, YT	XT, YT	DIPOLE	0CHAFF*	RFFØ FEXT FI	3 4 11	THETAD RHOD TSHFTD DIPLNG DIPDIA	216 217 218 219 220	Thin wire dipole scatterer Transfer function summed into XT, YT
SCYL	513	XT, YT	XT, YT	SCYL	OCYL*	RFFØ BASLIN	3 19	HTGT RTGT ANGTGT TORINT RSIM ACYL HCYL IPOL	106 107 108 109 110 201 202 205	Target model - right circular cylinder

\* These modules are located in BECAVUØ1 and the SELECT cards must be of the form:  
\$:SELECT:BECAVUØ1/RCSM\$JR/---

\* These modules are located in BECAVUØ1 and the SELECT cards must be of the form:

\$: SELECT: BECAVUØ1/RCSM\$JR / ---



## B.2 SOFTWARE MODULES LISTED BY REFERENCE NUMBER

This table includes all of the software modules listed in numerical order by module reference number.

100 SERIES: Basic transfer and input/output operations

200 SERIES: Basic mathematical operations

300 SERIES: Initialization and output configuration routines

400 SERIES: Radar block simulation modules (black box models)

500 SERIES: Radar system modules (radar system models)

Table B.2-1a 100 SERIES MODULES

101	RRAND	Parameter Initialization
102	RRAND	Parameter Initialization
103	RTOPDB	
104	XYTODB	
105	XYTOM	
106	XYTOM2	
108	XYTODB	
110	RTOPM	
111	RTOPM2	
113	PLTFMT	
114	(DATA XFER)	
115	(DATA XFER)	
116	ERGYRE	
117	ERGYRE	
118	ERGYCP	

Table B.2-1b 200 SERIES MODULES

201	DFT	231	RSHFTS
202	ZFFT	232	RSHFTS
203	ZIFFT	233	DFTRF
204	CONV	234	DFTFØ
205	CONVMP	235	ADDRND
206	DIVA	236	ADDRND
207	ADDA	237	ADRND
208	CUMDIS	239	ADDA
209	CUMDIS		
210	OUTCUM		
211	OUTCUM		
212	PDF		
213	PDF		
214	RNDARY		
215	RNDARY		
216	ATOD		
217	ATOD		
218	DTOA		
219	DTOA		
220	DTOA		
221	WEITRE		
222	WEITCP		
223	WEITMP		
224	SHIFT		
225	SHIFT		
226	SHIFTS		
227	SHIFTS		
228	DTOA		
229	RSHIFT		
230	RSHIFT		



Table B.2-1c 300 SERIES MODULES

301	(SYSTEM)
302	CLINT
303	PTLIST
304	PTLIST
305	PTLIST
306	PTLIST
307	PLOTTR
308	PLOTTR
309	PLOTTR
310	PLOTTR
311	(BISTATIC ANTENNA INITIALIZATION)
312	SPCAVG
313	SCANNR

Table B.2-1d 400 SERIES MODULES

401	NONLIN	438	HLIM
402	NONLIN	439	HLIM
403	CDIGFL	440	DCFAR
404	CDFNCL	441	DCFAR
405	RDIGFL	442	IHLIM
406	RDFNCL	443	IHLIM
407/408	FILT	445	IHWDET
409	INGTOR	446	IHWDET
410	INGTOR	447	IFWDET
413	ANTARY	448	IFWDET
414	HWDET	449	ISQDET
415	HWDET	450	ISQDET
416	FWDET	451	RECF
417	FWDET	452	RECFTF
418	SQDET	453	CGENSF
419	SQDET	454	PXFRM
420	FGENXY	455	CGENCW
421	FGENMP	456	LAMPRE
422	DIGTFL	457	LAMPRE
423	DIGTFL	458	LAMPCP
425	CGEN	459	CFAR
426	TSARY	460	CFAR
427	TSARY1	461	DIGFIL
430	MTIFLT	462	DIGFNC
431	MTIFLT	463	DIGFSF
432	MTINCL	464	DIPOLE
433	MTINCL	465	DIPOLE
434	SWPINT		
435	SWPINT		
436	NCSWPI		
437	NCSWPI		

Table B.2-1e 500 SERIES MODULES

501	TARGET
502	TGTNCL
503	CLUTTR
504	ANTPAT
505	TSRPAT
506	PHENC
507	PHENC
508	PHDEC
509	PHDEC
510	WVGUID
511	IONOS
512	ECM
513	SCYL
514	CHAFF
515	CHAFF



A P P E N D I X   C

V A R I A B L E S   U S E D   I N   T H E

R A D A R   S I M U L A T I O N   M O D E L

This list includes all the system and module parameters used in the modules in Appendix B. Column headings in the list are defined as follows:

1. NAME: Name of variable used in the system model program.
2. SYMBOL: Symbol of variable used in text.
3. UNITS: Dimensions of variable used in module program.
4. LOC: Location of variable in module program.
5. MODULE NUMBER and NAME: Modules that use variable.
6. NAME IN MODULE: Name of variable used in the module program.
7. COMMENTS: Short description, restrictions, and default value.

Note that the variable names in column 1 are the system variable names, which are referred to in Volume 1. The variable names in column 6 are the module or subroutine variable names, which are referred to in Volume 2. Table C-2 lists in alphabetical order those module names which are different from their corresponding system names.

Table C-1 VARIABLES USED IN THE RADAR SIMULATION MODEL

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
ADCFS	$f_{ADC}$	GHZ	149	216 217	ATOD ATOD	ADCFS ADCFS	A-10-D converter sampling rate (Default = FS)
ADEL	$\Delta\theta$	Degrees	33	113 505	PLTFMT TSRPAT	DELTHE ADELT	Angle increment
ANGLE	$\theta$	Degrees	87	426 427 505*	TSARY TSARY1 TSRPAT	ANGLE ANGLE ANGLE	Angle of ISAR response evaluation
ANGTGT	$\psi_T$	Degrees	108	501 502	TARGET TGTNCL	ANGTGT ANGTGT	Target azimuth angle with respect to radar
ANTAZ(1,J) ANTAZ(2,J) J=1,NPTAZ	$G_p(J)$ $\psi(J)$	Magnitude Degrees	201	301	(SYS) ANTINT	ANTAZ(2,75) ANTP(2,75)	Sampled antenna azimuth gain pattern (Power Units)
ANTAZ0	$\psi_0$	Degrees	18	301	(SYS)	ANTAZ0	Initial antenna azimuth angle
ANTEL(1,J) ANTEL(2,J) J=1,NPTEL	$G_e(J)$ $\epsilon(J)$	Magnitude Degrees	351	301	(SYS) ANTINT	ANTEL(2,75) ANTP(2,75)	Sampled antenna elevation gain pattern (normalized)
ANTEL0	$\epsilon_0$	Degrees	20	301	(SYS)	ANTEL0	Initial antenna elevation angle
ASTOP	—	Degrees	35	113 505	PLTFMT TSRPAT	STOPT ASTOP	Stop angle
ASTRT	—	Degrees	34	113 505	PLTFMT TSRPAT	STARPT ASTRT	Start angle
AZANG	$\psi$	Degrees	17	FUNCTION	AZGAIN	ANTANG	Antenna azimuth angle
AZBST	$\psi_{BS}$	Degrees	150	301	(SYS) ANTINT	AZBST BSIT	Antenna azimuth boresight with respect to gain pattern
AZEXT	—	Degrees	53	302	CLINT	AZEXT	Clutter volume azimuth extent
AZ0	—	Degrees	54 (9)	302 503*	CLINT CLUTTR	AZ000 AZ000	Clutter volume initial azimuth angle
BLIM	—	—	40	208 209	CUMDIS CUMDIS	BLIM BLIM	Lower bound of histogram
BPRI	$T_B$	Ns	114	453* 454 455*	CGENSF PXFRH CGENCW	BPRI BPRI BPRI	Burst pulse repetition interval
CFREQ	$f_c$	GHZ	146	510	WUGUID	CFREQ	Cutoff Frequency of Waveguide

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
CHIRP	$\mu$	GHz/Hz	92	420 421 425* 506 507	FGENXY FGENHP CGEN PHENC/FGENXY PHENC/FGENHP	CHIRP CHIRP CHIRP CHIRP CHIRP	The rate of frequency change (User specified only if NPMIX $\neq$ 0 or NSURP $\neq$ 0; otherwise CHIRP = FMBW/PW)
DELAZ	$\Delta\psi$	Degrees	123 (17)	302* 503*	CLINT CLUTR	DELAZ DELAZ	Azimuth spacing of clutter scatterers
DELEL	$\Delta\epsilon$	Degrees	124 (18)	302* 503*	CLINT CLUTR	DELEL DELEL	Elevation spacing of clutter scatterers
DFTINC(1,J) DFTINC(2,J) DFTINC(3,J) J=1,NIMP	$\phi(j)$ $\epsilon(j)$ $d(j)$	Degrees Ns Magnitude	201	201 233 234 426* 427* 451* 452* 508* 509*	DFT DFTF DFTF0 TSARY TSARY1 REC RECFT RECFTF PHDEC PHDEC	DIN(3,100) DIN(3,100) DIN(3,100) DIN(3,100) DIN(2,100) DIN(3,100) DIN(3,100) DIN(3,100) DIN(3,100)	DFT input samples to be transformed
DOFFRQ	$f_{dw}$	Hz*	127 (21)	302* 503*	CLINT CLUTR	DOFFRQ DOFFRQ	Doppler frequency shift of clutter induced by wind. *Always in Hz.
DX	d	Meters	77	413 425 426 427 451 452 453 455 504 505	ANTARY CGEN TSARY TSARY1 REC RECFT CGENSF CGENCW ANTFAT TSRFAT	DX DX DX DX DX DX DX DX DX DX	Antenna element spacing
ELANG	$\epsilon$	Degrees	19	FUNCTION	ELGAIN	ANTANG	Antenna elevation angle
ELBST	$\epsilon_{BS}$	Degrees	152	301	(SYS) ANTINT	ELBST BSIT	Antenna elevation boresight with respect to gain pattern
ELEXT	-	Degrees	56	302	CLINT	ELEXT	Clutter volume elevation extent
EL0	-	Degrees	57 (12)	302 503*	CLINT CLUTR	EL000 EL000	Clutter volume initial elevation angle



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
FALTIM	$t_f$	Ns	99	420 421 425 506 507	FGENXY FGENMP CGEN PHENC/FGENXY PHENC/FGENMP	FALTIM FALTIM FALTIM FALTIM FALTIM	Pulse fall time (Default = 11)
FBCK	-	Gain	75	409 410 434 435 436 437 451 452 505	INGTOR INGTOR SWPINT SWPINT NCSWPI NCSWPI RECF RECFTF TSRPAT	FBCK FBCK FBCK FBCK FBCK FBCK FBCK --	Integration feedback constant
FBCOEF(1,J) FBCOEF(2,J) J=1,NSEC	- -	1 Delay Gain 2 Delay Gain	201	461 462	DIGFIL DIGFNC	FB(2,25) FB(2,25)	Feedback coefficients for recursive digital filter
FBI	-	Gain	71	403 404	CDIGFL CDFNCL	FBXY FBXY	Imaginary component of feedback coefficient
FBR	-	Gain	70	403 404	CDIGFL CDFNCL	FBX FBX	Real component of feedback coefficient
FB1	-	Gain	70	405 406 430 431 432 433	RDIGFL RDFNCL MTIFLT MTIFLT MTINCL MTINCL	FB1 FB1 FB1 FB1 FB1 FB1	One delay feedback coefficient
FB2	-	Gain	71	405 406 430 431 432 433	RDIGFL RDFNCL MTIFLT MTIFLT MTINCL MTINCL	FB2 FB2 FB2 FB2 FB2 FB2	Two delay feedback coefficient
FFCOEF(1,J) FFCOEF(2,J) J=1,NSEC	- -	0 Delay Gain 1 Delay Gain	251	461 462	DIGFIL DIGFNC	FF(2,25) FF(2,25)	Feed forward coefficients for recursive digital filter
FFI	-	Gain	69	403 404	CDIGFL CDFNCL	FFXY FFXY	Imaginary component of feed forward coefficient
FFR	-	Gain	68	403 404	CDIGFL CDFNCL	FFX FFX	Real component of feed forward coefficient

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
FF0	-	Gain	68	405 406 430 431 432 433	RDIGFL RDFNCL MTIFLT MTIFLT MTINCL MTINCL	FF0 FF0 FF0 FF0 FF0 FF0	Zero delay feed forward coefficient
FF1	-	Gain	69	405 406 430 431 432 433	RDIGFL RDFNCL MTIFLT MTIFLT MTINCL MTINCL	FF1 FF1 FF1 FF1 FF1 FF1	One delay feed forward coefficient
FI	$\Delta f$	GHz	11	201+ 233+ 234+ 301 426+ 427+ 454+ 501+ 502+ 505+	DFT DFTF DFTF0 (SYS) TSARY TSARY1 PXERM TARGET TGINCL TSRPAT	FI FI FI FI FI FI FI FI FI FI	Frequency sampling increment
FMBW	$B_{fm}$	GHz	93	420 421 425	FGENXY FGENMP CGEN	FMBW FMBW FMBW	Frequency modulation bandwidth
FFOLE(1,J) FFOLE(2,J) J=1,NP	$\sigma_p(J)$ $f_p(J)$	Real-GHz Imag-GHz	301	407 408	FILT FILT	FFOLE(2,50) FFOLE(2,50)	S-Plane filter specification pole location(s)
FS	$f_s$	GHz	2	301 420+ 421+ 504+ 507+ 503+	(SYS) FGENXY FGENMP FGENMP PHENC/FGENXY PHENC/FGENMP CLUTTR	FS FS FS FS FS FS	Time domain sampling rate IF (FS = 0.0 AND TI $\neq$ 0.0) FS = 1.0/TI
FSAM(1,J) FSAM(2,J) J=1,NSAM	-	Real Gain Imag Gain	201	443 512	DIGFSF ECM	FSAM(2,100) --	Equi-spaced samples of filter transfer function
FSHIFT	$f_{het}$	GHz	15	202 203	ZFFT ZIFFT	FSHIFT FSHIFT	Frequency shift
FSTRT	$f_{st}$	GHz	91	420 421 422*	FGENXY FGENMP CGEN	FSTART FSTART FXYMT	Starting frequency (User specified only if NPWIX $\neq$ 0 or NSUBF $\neq$ 0 and CHIRP $\neq$ 0.0)

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
FSTRT(cont.)				506 507	PHENC/FGENXY PHENC/FGENHF	FSTART FSTART	
FZERO(1,J) FZERO(2,J) J=1,NZ	$\sigma_z(J)$ $f_z(J)$	Real-GHz Imag-GHz	201	407 408	FILT FILT	FZERO(2,50) FZERO(2,50)	S-Plane filter specification zero location(s)
FDEC		GHz	102	508 509	PHDEC PHDEC	FDEC FDEC	Phase decoder center frequency (User specified only if INPTF = 1 ; otherwise set equal to SIMFO)
GAIN	9	Volts(out)/ Volts(in)	145	456 457 458	LAMPRE LAMPRE LAMPFCP	GAIN GAIN GAIN	Linear Amplifier Voltage Gain
GLBL(J) J=1,18	-	-	301	307 308 309 310	PLOTTT GLBL(18) PLOTTR GLBL(18) PLOTTR GLBL(18)	GLBL(18) GLBL(18) GLBL(18) GLBL(18)	Plot label
HTGT	H <sub>T</sub>	Meters	106	501 502	TARGET TGNCNCL	HTGT HTGT	Height of target
IADD1			23	101	RRAND	MAD1	Random number generator starting address (Default = 1)
ICFLG	-	-	126 (20)	302* 503*	CLINT CLUTTR	ICFLG ICFLG	Clutter data flag ICFLG = 0; Clutter model parameters not initialized 1; Clutter model parameters initialized
ICFOR	-	-	7	202 301	ZFFT (SYS)	ICPLXF ICFOR	Fourier transform complex data flag (Default = 1) ICFOR = 0; Real signal data 1; Complex signal data
ICINV	-	-	6	203 301	ZIFFT (SYS)	ICPLXI ICINV	Inverse Fourier transform complex data flag (Default = 1) ICINV = 0; Real signal data 1; Complex signal data
ICODE	-	-	194	506 507	PHENC PHENC	CODE CODE	User specified phase code (MODEPH = 3)
IDDUMP	-	-	21	101 102 201 233	RRAND RRAND DFT DTRF	IDMY1 IDMY1 IDMP IDMP	Data dump flag IDDUMP = 0; Suppress data dump 1; Dump diagnostic data from modules



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
IDDUMF (cont.)				234 302 413 425 426 427 501 502 503* 504 505	DTF0 CLINT ANTARY CBEN TSARY TSARY1 TARGET IGINCL CLUTR ANTFAT TSRFAT	IDMP IDMP IDMY IDMP IDMY IDMY IDMY IDMY IDMP IDMY IDMY	
IFB1D	-	Gain	165	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFB1D IFB1D IFB1D IFB1D	One delay integer feedback coefficient - denominator (Default = 1)
IFR1N	-	Gain	164	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFR1N IFR1N IFR1N IFR1N	One delay integer feedback coefficient - numerator
IFB2D	-	Gain	167	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFB2D IFB2D IFB2D IFB2D	Two delay integer feedback coefficient - denominator (Default = 1)
IFB2N	-	Gain	166	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFB2N IFB2N IFB2N IFB2N	Two delay integer feedback coefficient - numerator
IFCODE	-	-	113	303 304 305 306 307 308 309 310	PLIST PLIST PLIST PLIST PLOTTR PLOTTR PLOTTR PLOTTR	IFCODE IFCODE IFCODE IFCODE IC IC IC IC	Output data file code
IFF0D	-	Gain	161	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFF0D IFF0D IFF0D IFF0D	Zero delay integer feed forward coefficient - denominator (Default = 1)
IFF0N	-	Gain	160	430 431 432 433	MTFLT MTFLT MTINCL MTINCL	IFF0N IFF0N IFF0N IFF0N	Zero delay integer feed forward coefficient - numerator

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
IFF1D	-	Gain	163	430 431 432 433	MTIFLT MTIFLT MTINCL MTINCL	IFF1D IFF1D IFF1D IFF1D	One delay interser feed forward coefficient - denominator (Default = 1)
IFFIN	-	Gain	162	430 431 432 433	MTIFLT MTIFLT MTINCL MTINCL	IFFIN IFFIN IFFIN IFFIN	One delay interser feed forward coefficient - numerator
INORM	-	-	84	413 504	ANTARY ANTPAT	INORM INORM	Antenna gain normalization flag
INPTF	-	-	155	508 509	PHDEC PHDEC	INPTF INPTF	Flag to indicate user provided inputs are available
IPY(J) J=1,NSR	-	-	186	506 507	PHENC PHENC	IPY(8) IPY(8)	Shift register initial values
IPRIPT	-	-	143	301	(SYS)	IPRIPT	Pulse repetition interval pointer (Default = 1 ; 1 ≤ IPRIPT ≤ NPRIS ≤ 11)
IRND	-	-	22	101	RRAND	IRND	Random number generator variable
IROFF	-	-	105	216 217	ATOD ATOD	IROFF IROFF	A-to-D converter round off flag IROFF= 0: No roundoff 1: Roundoff used
IRPSCG	-	-	81	413 425 504	ANTARY CGEN ANTPAT	IRPSCG IRPSCG IRPSCG	Control generator phase shifter round off flag IRPSCG= 0: No Roundoff 1: Roundoff Used
IRPSR	-	-	83	413 426 427 504 505	ANTARY TSARY TSARY1 ANTPAT TSRPAT	IRPSR IRPSR IRPSR -- --	Antenna feed network phase shifter round off flag IRPSR= 0: No Roundoff 1: Roundoff Used
ISDUMP	-	-	5	301	(SYS)	ISDUMP	System data dump flag ISDUMP= 0: Only first EXEC block printed 1: EXEC Blocks Printed 2: EXEC & DATA Blocks Printed 3: DATA Blocks Printed

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
ITAP(1,J)	$g_N(J)$	Gain	201	422	DIGTFL	ITAF(3,100)	Digital transversal filter tap specifications
ITAP(2,J)	$g_D(J)$	Gain		423	DIGTFL	ITAF(3,100)	
ITAP(3,J) J=1,NTAPS	$I_s(J)$	Demoninator Time Increments					
JERP	$P_J$	Watts	175	512	ECM	JERP	Jammer Effective Radiated Power
JFRBW	$B_J$	GHz	176	512	ECM	JFRBW	Jammer sweep Bandwidth
JF $\theta$	$f_{\theta,J}$	GHz	178	512	ECM	JF $\theta$	Jammer center frequency with respect to SIM $\theta$
JHGT	$H_J$	Meters	174	512	ECM	JHGT	Jammer height
JMAZ	$\phi_J$	Degrees	173	512	ECM	JMAZ	Jammer azimuth angle
JPEROD	$T_J$	Ns	157	512	ECM	JPEROD	Noise burst repetition interval
JFW	$T_J$	Ns	177	512	ECM	JFW	Length of noise burst
JRND	-	-	24	101	RRAND	JRND	Random number generator variable
JRNG	$R_J$	Meters	171	512	ECM	JRNG $\theta$	Jammer range at TIME = 0.0
JRSIM	$R_J^*$	Meters	172	512	ECM	JRSIM	Jammer range in simulation for TIME = 0.0 (used to compute time delay only)
JVEL	$V_J$	Meters/sec	156	512	ECM	JVEL	Jammer radial velocity
KCELL	-	Samples	128 (22)	302* 503*	CLINT CLUTTR	KCELL KCELL	Number of impulses which represent clutter as a function of range
KK	-	Cells	120 (14)	302* 503*	CLINT CLUTTR	KK KK	Number of clutter volume range increments
LAMBDA	$\lambda$	Meters	13	301+ 302+	(SYS) CLINT	LAMBDA LAMBDA	Wavelength IF(RFF $\theta$ $\neq$ 0.0) LAMBDA = 1.0/RFF $\theta$
LF	-	-	62	303 304 305 306	FTLIST FTLIST FTLIST FTLIST	LF LF LF LF	Data type flag LF= 0: Magnitude scaling 1: Decibel scaling 2: Dependent variable is converted to log10 before plotting 3: Dependent variable is converted to dB before plotting, i.e. 10*log10 DV(J)



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
MM	-	Cells	55 (10)	302 503*	CLINT CLUTTR	MM MM	Number of clutter volume azimuth increments
MODE	-	-	122 (16)	302* 503*	CLINT CLUTTR	MODE MODE	Clutter model mode flag MODE=
MODEDF	-	-	168	430 431 432 433	MTIFLT MTIFLT MTINCL MTINCL	-- -- -- --	1) Clutter scatterers fixed during simulation 2) Scatterers phases vary as function of time Digital filter mode flag MODEDF=
MODEPH	-	-	183	506 507	PHENC PHENC	MODEPH MODEPH	1) Floating point arithmetic 2) Integer arithmetic Phase encoder mode flag MODEPH=
MODTSR	-	-	116	426 427 505	TSARY TSARY1 TSRPAT	MODTSR MODTSR MODTSR	1) Stored Barker code 2) Pseudo-random code 3) User specified code TSAR mode flag MODTSR=
NAUTO	-	-	64	303 304 305 306	PTLIST PTLIST PTLIST PTLIST	NAUTO NAUTO NAUTO NAUTO	1) Transmit pencil beam 2) Receive pencil beam 3) Transmit pencil & receive pencil, (THETAR = THETAS, ARYDEL = RECDL) 4) Transmit pencil & receive pencil, (THETAR ≠ THETAS, ARYDEL = RECDL) 5) Transmit pencil & receive pencil, (THETAR ≠ THETAS, ARYDEL ≠ RECDL) 6) Transmit pencil & receive monopulse 7) Receive monopulse Data processing flag NAUTO=
NBIIDF	-	Bits	169	430 431 432 433	MTIFLT MTIFLT MTINCL MTINCL	NBITS NBITS NBITS NBITS	0) the input data scanned to determine Max(TH) and Min(TL) value of the dependent variable 1) the user provided values of TH and TL used. Digital filter data word size (Default = 31 Bits)
NBITS	-	Bits	104	216 217	ATOD ATOD	NBITS NBITS	A-to-D converter output word size (includes sign bit) (Default = 31 Bits)

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
NBLKS	-	Records Of Random Disc File	121	302*	CLINT	NBLKS	Number of records occupied by clutter scatterer data
NBFSCG	-	Bits	80	413 425 504	ANTARY CGEN ANTFAT	NBFSCG NBFSCG NBFSCG	Accuracy of TSAR control generator phase shifter (Default = 15 Bits)
NBFSCR	-	Bits	82	413 426 427 504 505	ANTARY TSARY1 ANTFAT TSRFAT	NBFSCR NBFSCR NBFSCR NBFSCR	Accuracy of TSAR antenna feed network phase shifters (Default = 15 Bits)
NCELL	-	Range Bits	170	440 441	DCFAR DCFAR	NCELL NCELL	Number of range samples to be averaged
NCGFLS	-	Pulses	88	425 453	CGEN CGENSF	NSUBF NCGFLS	Number of TSAR control generator subranges
NCFACK	-	-	42	210 211	OUTCUM OUTCUM	NCFACK NCFACK	Number of histogram samples combined to generate each cumulative distribution sample (Default = 1)
NDFZ	-	-	197	463 512	DIGFSF ECM	NDFZ NDFZ	Number of zeros to be synthesized by comb filter (NDFZ ≤ 256)
NDFPACK	-	-	43	212 213	PDF PDF	NDFPACK NDFPACK	Number of histogram samples combined to generate each probability density sample (Default = 1)
NHIST	-	Intervals	41	208 209	CUMDIS CUMDIS	NIXF NIXF	Number of histogram intervals (NHIST ≤ 8192)
NIMP	-	Samples	200	201 233 234 425* 426* 427* 451* 452 508* 509*	DFT DFTF DFTF0 CGEN TSARY TSARY1 REC RECFTF PHDEC PHDEC	NIMP NIMP NIMP NPT NIMP NIMP NPULS NPULS NIMP NIMP	Number of input samples to be processed by DFT (NIMP ≤ 100)
NN	-	Cells	58 (13)	320 503*	CLINT CLUTR	NN NN	Number of clutter volume elevation increments







VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
NTSAR	-	Elements	76	413 426 427 504 505	ANTARY TSARY TSARY1 ANTPAT TSRPAT	NTSAR NTSAR NTSAR --	Number of elements in TSAR subarray (NTSAR ≤ 100)
NTYPE	-		45	214 215 235 236 237	RNDARY RNDARY ADDRND ADDRND ADDRND	NTYPE NTYPE NTYPE NTYPE NTYPE	Probability distribution flag  NTYPE = 1: Uniform 2: Rayleigh 3: Gaussian 4: Uniform 6: Swerling Target Model Mt. 1 & 2 7: Swerling Target Model Mt. 1 & 4 8: Sine
NZ	Nz	Zeros	72	407 408	FILT FILT	NZ NZ	Number of zeros used in specifying a filter (NZ ≤ 50)
N2	-	Bits	1	202 203 301 420+ 421+ 506+ 507+ 504+ 512+	ZFFT ZFFT (SYS) FGENXY FGENMP PHENC/FGENXY PHENC/FGENMP ANTPAT ECH	N2 N2 N2 N2 N2 N2 N2 N2 N2	2**N2 = Number of points Processed by FFT algorithm (N2 ≤ 13) (Default-Value set by ZFFT/ZIFFT)
ORIG		GHz or Ms	38	221 222 223	WEITRE WEITCP WEITMP	ORIG ORIG ORIG	Weighting function independent variable offset
PCODE(J) J=1,NSUBP	φ(J)	Degrees	451	420 421	FGENXY FGENMP	PCODE(300) PCODE(300)	Transmitted waveform phase code
PRI(J) J=1,NPRIS	T(J)	Seconds	130	301	(SYS)	PRI(11)	Array of pulse repetition intervals
PW	T	Ms	90	420 421 425*	FGENXY FGENMP CGEN	PW PW PW	Transmitted pulsewidth or burst length
RADIUS	-	-	195	463 512	DIOFSF ECH	RADIUS --	Radius of circle in z-plane on which poles and zeros are located

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
RECDEL	-	Ns	117	426 427 451 452 505	TSARY TSARY1 REC RECFTF TSRFAT	RECDEL RECDEL RECDEL --	TSAR antenna receive feed network delay line lengths
RECIRT	-	Ns	118	451 452 505	REC RECFTF TSRFAT	RECIRT RECIRT --	TSAR receiver processor impulse response time span
RFF0	$f_{RF}$	BHz	3	233 301 413 425+ 426+ 427+ 453+ 455+ 501+ 502+ 504 505+ 510+ 511+	DFTRF (SYS) ANTARY CGEN TSARY TSARY1 CGENSF CGENCW TARGET TGNCCL ANTFAT TSRFAT WVGUID IONDS	F0 RFF0 F0 F0 F0 F0 RFF0 RFF0 F0 F0 F0 RFF0 RFF0	Radiation frequency of the radar
RISTIM	$t_r$	Ns	98	420 421 425 506 507	FGENY FGENMP CGEN PHENC/FGENY PHENC/FGENMP	RISTIM RISTIM RISTIM RISTIM RISTIM	Transmitted pulse rise time (Default = 11)
RNEXT	-	Ns	51 (6)	302 503*	CLINT CLUTTR	RNEXT RNEXT	Clutter volume range extent
RNG	-	-	60	303 304 305 306 307 308 309 310	PTLIST PTLIST PTLIST PTLIST PLOTTR PLOTTR PLOTTR PLOTTR	RNG RNG RNG RNG XIVRNG XIVRNG XIVRNG XIVRNG	Range of independent variable to be plotted
RNGCEL	$t_{cell}$	Ns	14	301 302 503*	(SYS) CLINT CLUTTR	RNGCEL ICELL TUELL	Spacing between impulses which represent clutter as a function of range. IF (RNGCEL = 0.0 & SIMBW ≠ 0.0) RNGCEL = 1.0/SIMBW Also RNGCEL = 11



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
RN0	-	Ns	52 (7)	302 503*	CLINT CLUTR	RN000 RN000	Clutter model initial range
RSIM	$R_T^*$	Meters	110	501 502	TARGET TGINCL	R000 R000	Target range in simulation for TIME = 0.0 (used to compute time delay only)
RTGT	$R_T$	Meters	107	501 502	TARGET TGINCL	RTGT0 RTGT0	True target range at TIME = 0.0
RWPH	-	Degrees	48	302 503*	CLINT CLUTR	RWPH RWPH	Maximum pulse-to-pulse scatterer phase variation
SEDENS	$\int_{s1}^{s2} N_e ds$	Electrons/cm**2	148	511	IONOS	SEDENS	Integrated electron density along propagation path
SF	-	Gain	74	407 408 461 462	FILT FILT DIGFIL DIGFNC	SF SF SF SF	Filter scaling factor
SHFHAS	$\phi_{sh}$	Degrees	181	224 225 226 227 229 230 231 232 425*	SHIFT SHIFT SHIFTS SHIFTS RSHIFT RSHIFT RSHIFTS RSHIFT CGEN	THT THT THT THT THT THT THT THT THT	Phase angle change
SHT0	$t_{sh}$	Ns	180	224 225 226 227 229 230 231 232 425*	SHIFT SHIFT SHIFTS SHIFTS RSHIFT RSHIFT RSHIFTS RSHIFT CGEN	T0 T0 T0 T0 T0 T0 T0 T0 T0	Time change
SIGMA	$\sigma$	Depends on distribution generated	28	101 102	RRAND RRAND	SIGMA SIGMA	Standard deviation of Gaussian and Rayleigh distributions. Average RCS for Swerling Target Models
SIG2SQ	$-2\sigma^2$	--	30	101* 102*	RRAND RRAND	SIG2SQ SIG2SQ	Random number generator parameter
SIMBW	$B_{sim}$	GHz	4	201 202 203	DFT ZFFT ZIFFT	FEXT SIMBW SIMBW	Simulation bandwidth (SIMBW < FS) (Default = FS)



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
SWTIM	$t_{sw}$	Ns	97	420 421 506 507	FGENXY FGENMP PHENC/FGENXY PHENC/FGENMP	SWTIM SWTIM SWTIM SWTIM	Switching time between subpulses (Default = 11)
TAVG	$t_{av}$	Ns	198	459 460	CFAR CFAR	TAVG TAVG	CFAR averaging time interval
TAPSPC	$T_c$	Ns	154	508 509	PHDEC PHDEC	TAPSPC TAPSPC	Phase decoder tap spacing (User specified if INPTF = 1; otherwise set to SPW)
TCGNOM	-	Ns	89	425 453 455	CGEN CGENSF CGENCW	TNOM TNOM TNOM	TSAR control generator nominal pulse spacing
TDLIN	$T_a$	Ns	86	426 427 505	TSARY TSARY1 TSRPAT	ARYDEL ARYDEL --	TSAR antenna transmit feed network delay line lengths
TDLMON	-	Ns	185	426 427 505	TSARY TSARY1 TSRPAT	TDLMON TDLMON --	Differential delay used to generate TSAR monopulse receive beam
TFN(1,J) TFN(2,J) J=1,NTFN	$V_{in}(J)$ $V_{out}(J)$	Input Mag. Output Mag.	201 402	401 402	NONLIN NONLIN	TFN(2,50) TFN(2,50)	Nonlinear transfer function
TGTVEL	$V_T$	Meters/Sec	112	501 502	TARGET TGTNCL	TGTVEL TGTVEL	Target radial velocity
TH	-	-	65	303 304 305 306	PTLIST PTLIST PTLIST PTLIST	TH TH TH TH	Upper limit of dependent variable to be plotted (NAUTO=1)
THETAR	$\theta_R$	Degrees	119	426 427 451 452 505	TSARY TSARY1 RECF RECF TSRPAT	THETAR THETAR THETAR THETAR --	Receive beam steering angle
THETAS	$\theta_S$	Degrees	78	413 425 426 427 453 455 504 505	ANTARY CGEN TSARY TSARY1 CGENSF CGENCW ANTPAT TSRPAT	THETAS THETAS THETAS THETAS THETAS THETAS --	Transmit beam steering angle



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
TI	$\Delta t$	Ns	12	2014 2334 2344 301 3024 4204 4214 4254 5034 5064 5074	DFT DTRF DTRF0 (SYS) CLINT FGENXY FGENMP CGEN CLUTR PHENC/FGENXY PHENC/FGENMP	TI TI TI TI TI TI TI TI TI TI TI	Time sampling increment IF(FS $\neq$ 0.0) TI = 1.0/FS
TIME	$t^*$	Seconds	16	301 5014 5024 5034 5124	(SYS) TARGET TGTNCL CLUTR ECM	TIME TIME TIME TIME TIME	Elapsed time
TIME LSB	-	Ns	115	425	CGEN	TIME LSB	Pulse timing least significant bit size
TJIT	-	Ns	182	229 230 231 232	RSHIFT RSHIFT RSHIFTS RSHIFTS	TJIT TJIT TJIT TJIT	Time shift jitter
TL	-	-	66	303 304 305 306	FLIST FLIST FLIST FLIST	TL TL TL TL	Lower limit of dependent variable to be plotted (NAUTO = 1)
TLIM	-	-	39	208 209	CUMDIS CUMDIS	TLIM TLIM	Upper bound of histogram
TORINT	$\phi_T$	Degrees	109	501 502	TARGET TGTNCL	TORINT TORINT	Target orientation angle
TSCAT(1,J) TSCAT(2,J) TSCAT(3,J) J=1,NSCAT	$\sigma(J)$ $r(J)$ $\gamma(J)$	Square Meters Meters Degrees	201	501 502	TARGET TGTNCL	TSCAT(3,100) TSCAT(3,100)	Target discrete scatterer parameters
TSRLDS(J) J=1,NTSAR	$g_a(J)$	Gain	401	413 426 504 505	ANTARY TSARY ANTPAT TSRPAT	TSRLDS(100) TSRLDS(100) TSRLDS(100) ---	TSAR antenna distributed feed network losses
TSTART	-	Ns	100	420 421 422*	FGENXY FGENMP CGEN	TSTART TSTART TSTART	Transmitted pulse starting time

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
TSTART(cont.)				506 507	PHENC/FGENXY PHENC/FGENMP	TSTART TSTART	
UEXT	-	-	26	101 102	RRAND RRAND	UUEXT UUEXT	Width of uniform distribution
UL	-	-	31	101* 102*	RRAND RRAND	UL UL	Lower bound of uniform distribution
UMEAN	-	-	25	101 102	RRAND RRAND	UMEAN UMEAN	Mean of uniform distribution
VDL(J) J=1,12	-	-	251	307 308 309 310	PLOTR PLOTR PLOTR PLOTR	VDL(12) VDL(12) VDL(12) VDL(12)	Plot dependent variable label
VELANG	-	Degrees	50	302	CLINT	VELANG	Wind velocity vector angle
VIL(J) J=1,12	-	-	201	307 308 309 310	PLOTR PLOTR PLOTR PLOTR	VIL(12) VIL(12) VIL(12) VIL(12)	Plot independent variable label
VPEAK	$V_T$	Volts	129	420 421 506 507	FGENXY FGENMP PHENC/FGENXY PHENC/FGENMP	VPEAK VPEAK VPEAK VPEAK	Transmitter peak output voltage (Default = 1.0)
WINDVEL	$V_w$	Meters/Sec	49	302	CLINT	WINDVEL	Wind velocity vector magnitude
WSCAN	$W_s$	Deg/Sec	10	301	(SYS)	WSCAN	Antenna scan rate
WT(1,J) WT(2,J) WT(3,J) J=1,NPWT	$x(J)$ $t(J)\alpha f(J)$ $y(J)$	Real-Gain Ns or GHz Imag.-Gain	201	221 222	WEITRE WEITCP	WT(3,100) WT(3,100)	Array containing sampled weighting function
WT(1,J) WT(2,J) WT(3,J) J=1,NPWT	$g(J)$ $t(J)\alpha f(J)$ $\phi(J)$	Gain Ns or GHz Degrees	201	223	WEITMP	WT(3,100)	Array containing sampled weighting function
WTX(1,J) WTX(2,J) WTX(3,J) J=1,NPWT	$g(J)$ $t(J)$ $\phi(J)$	Gain Ns Degrees	201	420 421 425	FGENXY FGENMP CGEN	WT(3,100) WT(3,100) WT(3,100)	Array containing sampled transmitter complex envelope

VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
XLSB	-	Volts	103	216 217	AT0D AT0D	XLSB XLSB	A-to-D converter least significant bit size
XMEAN	-	-	27	101 102	RRAND RRAND	XMEAN XMEAN	Mean of Gaussian distribution
XUEXT	-	-	32	101* 102*	RRAND RRAND	XUEXT XUEXT	Random number generator parameter
XULANG	-	Radians	125 (19)	302* 503*	CLINT CLUTTR	XULANG XULANG	Clutter model parameter
XWLENG	Z	Meters	147	510	WVGUID	XWLENG	Length of waveguide run
A D D E N D A							
ACYL	-	Inches	201	513	SCYL	A	Radius of cylinder
ANBAZ0	$B\psi_0$	Degrees	150	311	(BISTAT -SYS)	ANBAZ0	Initial receiving antenna azimuth angle
ANBEL0	$BE_0$	Degrees	151	311	(BISTAT -SYS)	ANBEL0	Initial receiving antenna elevation angle
BASLIN	-	Meters	19	311	(BISTAT -SYS)	BASLIN	Baseline length between transmit and receive antennas
CHFAZ	-	Degrees	215	514 515	CHAFF CHAFF	AZCHFF AZCHFF	Azimuth to centroid of chaff cloud
CHFHGT	-	Meters	214	514 515	CHAFF CHAFF	HCHAFF HCHAFF	Height of centroid of chaff cloud
CHFRNG	-	Meters	213	514 515	CHAFF CHAFF	RCCENT RCCENT	Range to centroid of chaff cloud



VARIABLE NAME (SYSTEM)	SYMBOL	UNITS	LOC	MODULE NUMBER	MODULE NAME	VARIABLE NAME (MODULE)	COMMENTS
DIPDIA	a	Inches	220	464 465 514 515	DIPOLE DIPOLE CHAFF CHAFF	DIA DIA - -	Dipole Diameter
DIPLNG	$X_L$	Inches	219	464 465 514 515	DIPOLE DIPOLE CHAFF CHAFF	XL XL - -	Dipole length
DORINT (1,J) (2,J) (3,J)	$\theta_D$ D $r_D$	Degrees Degrees Meters	321	514 515	CHAFF CHAFF	DORINT (3,100)	Chaff cloud dipole orientations
HCYL	-	Inches	202	513	SCYL	H	Half-length of cylinder
IPOL	-	-	205	513	SCYL	IPOL	Polarization Flag =1, VV Polarization =2, HH Polarization
NDIPOL	-	-	212	514 515	CHAFF CHAFF	NDIPOL NDIPOL	Number of dipoles used in chaff model
RHOD	D	Degrees	217	464 465	DIPOLE DIPOLE	RHO RHO	Dipole orientation angle with respect to E-field vector
THETAD	$\theta_D$	Degrees	216	464 465	DIPOLE DIPOLE	THETA THETA	Dipole azimuth angle with respect to propagation vector
TSHFTD	-	Ns	218	464	DIPOLE	TSHFT	Time delay for computing dipole transfer function
WSCANB	-	Deg/Sec	17	311	(BISTAT -SYS)	WSCANB	Receiving antenna scan rate

Table C-2 MODULE VARIABLE NAME/SYSTEM VARIABLE  
NAME CROSS REFERENCE TABLE

<u>MODULE VARIABLE NAME</u>	<u>SYSTEM VARIABLE NAME</u>
ANTANG	AZANG or ELANG
ANTP	ANTAZ or ANTEL
ARYDEL	TDLINE
AZ000	AZ0
BSIT	AZBST or ELBST
CODE	ICODE
DELTHE	ADELT
DIN	DFTIN
EL000	EL0
FB	FBCOEF
FBX	FBR
FBXY	FBI
FEXT	SIMBW
FF	FFCOEF
FFX	FFR
FFXY	FFI
FSTART	FSTRT
F0	RFF0 or SIMF0
F0XMT	FSTRT
IC	IFCODE
ICPLXF	ICFOR
ICPLXI	ICINV
IDMP	IDDUMP
IDMY	IDDUMP
IDMY1	IDDUMP
INORM	NORMFT
MAD1	IADD1
NBITS	NBITDF
NIXF	NHIST
NP	NSEC
NPT	NPTAZ, NPTEL or NIMP
NPTS	NRNDPT or NTFN
NPULS	NIMP
NSUBP	NCGPLS
NTYPE	NTYPER
N2POW	N2
RN000	RN0
RTGT0	RTGT
R000	RSIM
STARPT	ASTRT
STOPT	ASTOP
TCELL	RNGCEL

Table C-2 MODULE VARIABLE NAME/SYSTEM VARIABLE  
NAME CROSS REFERENCE TABLE  
(Page 2 of 2)

<u>MODULE VARIABLE NAME</u>	<u>SYSTEM VARIABLE NAME</u>
THT	SHPHAS
TNOM	TCGNOM
TØ	SHTØ
UEXT	XUEXT
UUEXT	UEXT
WT	WTX
XIVRNG	RNG
XIVST	ST

ADDENDA

A	ACYL
AZCHFF	CHFAZ
DIA	DIPDIA
H	HCYL
HCHAFF	CHFHT
RCCENT	CHFRNG
RHO	RHOD
THETA	THETAD
TSHFT	TSHFTD
XL	DIPLNG



A P P E N D I X   D  
T A B L E   O F  
T I M E   S H A R I N G   F I L E S

The table contained herein is a list of the files in the radar simulation model. In the left column, the file or /catalog/file designation that includes the password is listed. The files beginning with the letter "S" are the Fortran-IV decks, and those beginning with the letter "O" are the object decks. In the right column is the list of modules that are located in the corresponding file in the left columns.

The Job Definition Files are those used to run the sample problems in Section 8 of Volume I and Section 4 of Volume III.

Table D-1 TIME SHARING FILES

BECAGD01 FILES

*LODREX\$RJD	MAIN1
*OLODR\$RJD	MAIN1
*SUPRT1\$RJD	IPACK;RRAND;DBLKX;BLOCK DATA
*OSUP1\$RJD	IPACK;RRAND;DBLKX;BLOCK DATA
*SCLINT\$RJD	CLINT
*OCLINT\$RJD	CLINT
*SXMTR1\$RJD	PHENC
*OXMTR1\$RJD	PHENC
*OARSIN\$RJD	ARSIN
*SIMEX\$RJD	MAIN2
*OSIMEX\$RJD	MAIN2
*SZFFT\$RJD	ZFFT
*OZFFT\$RJD	ZFFT
*SDFIN\$RJD	DCFAR;DIGTEL;CDIGEL;INGTOR;ATOD;RDIGEL; DIGFIL;ECM;DIGFSF
*ODFIN\$RJD	DCFAR;DIGTEL;CDIGEL;INGTOR;ATOD;RDIGEL; DIGFIL;ECM;DIGFSF
*SXMTR2\$RJD	FGENXY;PHDEC;ABORT
*OXMTR2\$RJD	FGENXY;PHDEC;ABORT
*SPLOTS\$RJD	PTLIST;PLOTTR
*OPLOTS\$RJD	PTLIST;PLOTTR
*SMISC1\$RJD	FILT;WEITRE;CONV;SHIFT;CFAR;LAMPDP;ERGVCP
*OMISC1\$RJD	FILT;WEITRE;CONV;SHIFT;CFAR;LAMPDP;ERGVCP
*STSAR1\$RJD	RECF;PXFRM;CGENSF
*OTSAR1\$RJD	RECF;PXFRM;CGENSF
*/BLOCK1\$RJD/SMISC2\$RJD	NONLIN;HWDET;ANTINT;DFT
*/BLOCK1\$RJD/OMISC2\$RJD	NONLIN;HWDET;ANTINT;DFT
*/BLOCK1\$RJD/SUPRT2\$RJD	RNDARY;CUMDIS;RTOPDB;AZGAIN;ELGAIN
*/BLOCK1\$RJD/OSUP2\$RJD	RNDARY;CUMDIS;RTOPDB;AZGAIN;ELGAIN

* /BLOCK1\$RJH/SANT1\$RJH	ANTARY; PLTFMT
* /BLOCK1\$RJH/DANT1\$RJH	ANTARY; PLTFMT
* /BLOCK1\$RJH/SANT2\$RJH	SCANNR; SPCAVG
* /BLOCK1\$RJH/DANT2\$RJH	SCANNR; SPCAVG
* /BLOCK1\$RJH/STGCL\$RJH	TARGET; CLUTTR; WVGUID; IONOS
* /BLOCK1\$RJH/DTGCL\$RJH	TARGET; CLUTTR; WVGUID; IONOS
* SSTSR\$RJH	TSRPAT; CGEN; TSARY
* /BLOCK1\$RJH/OTSAR\$RJH	TSRPAT; CGEN; TSARY
* /BLOCK1\$RJH/SDIG\$RJH	MTIFLT; SWPINT
* /BLOCK1\$RJH/DDIG\$RJH	MTIFLT; SWPINT
* TAPEIN	ASSEMBLY LANG PROG TO READ TAPE INTO BUFF
* CKTAPE	PROGRAM TO VERIFY RCS MAG TAPES
* TAPTEL	TAPES SENT TO RADC

#### JOB DEFINITION FILES

RANJB	1, 8, 2	WGDISP	1, 8, 16
ENDIST	1, 8, 3	IMAGEM	1, 8, 17
DFTPRB	1, 8, 4	CHAFFM	1, 8, 18
NONLNP	1, 8, 5	BISTAT	1, 8, 19
BARKER	1, 8, 6	TXCODE	1, 8, 20
WBTGT1/2	1, 8, 7	DECODE	1, 8, 21
WBTGCL	1, 8, 8	DHPRQB	1, 8, 22
NBTGCL	1, 8, 9	RAINPB	1, 8, 23
WAPCG	1, 8, 10	RCSRP	1, 8, 24
ANTNNA1	1, 8, 11	TSARBP	III, 4, 1
TSARBK	1, 8, 12	CGENOT	III, 4, 2
ECMODL	1, 8, 13	TSARTM	III, 4, 3
DIKFIX	1, 8, 14	TSARJB	III, 4, 4
CFARMD	1, 8, 15	FSANT	III, 4, 5

#### SELECTED BECAVU01 FILES

* SIMAGP	IMAGP; ERRPRC
* DIMAGP	IMAGP; ERRPRC
* /RCSM\$JR/SCHAFF	DIPOLE; CHAFF; EXPI
* /RCSM\$JR/DCHAFF	DIPOLE; CHAFF; EXPI
* /RCSM\$JR/SCYL	SCYL; BISTGT
* /RCSM\$JR/DCYL	SCYL; BISTGT
* /RCSM\$JR/SXSA	GAM; BESS
* /RCSM\$JR/DSXSA	GAM; BESS



A P P E N D I X   E  
T C H E B Y S C H E F F   F I L T E R  
D E S I G N   D A T A

Given the Tschebyscheff approximation of a low-pass filter,  
i.e.

$$|F(j\omega)|^2 = \frac{1}{1 + \delta^2 T_n^2(\omega)},$$

where  $F(j\omega)$  is the transfer function,

$\delta$  is the ripple factor (i.e.,

$1 - \frac{1}{(1 + \delta^2)^{\frac{1}{2}}}$  is the peak-to-peak  
ripple), and

$T_n(\omega)$  is a Tschebyscheff polynomial of  
order  $n$ , i.e.,

$$T_n(\omega) = \cos(n \cos^{-1} \omega), |\omega| \leq 1$$

$$= \cosh(n \cosh^{-1} \omega), |\omega| > 1;$$

then it can be shown that the  $k^{\text{th}}$  pole,  $S_k$ , of the  
transfer function  $F(j\omega)$  is determined as follows:

$$S_k = \sigma_k + j\omega_k$$

$$\sigma_k = -\sinh\left(\frac{1}{n} \sinh^{-1} 1/\delta\right) \sin \frac{(2k-1)\pi}{2n}$$

$$\omega_k = \cosh\left(\frac{1}{n} \sinh^{-1} 1/\delta\right) \cos \frac{(2k-1)\pi}{2n}$$

where  $F(j\omega) = \frac{1}{(1 + \delta^2)^{\frac{1}{2}}}$  when  $\omega = 1$ .

By setting  $1 + \delta^2 T_n^2(\omega) = 2$  and solving for  $\omega$ , we can  
determine a normalization factor for the poles such that  
 $F^2(j1) = \frac{1}{2}$ , i.e., the filter response will be -3 dB with  
respect to the ripple peak at  $\omega = 1$ . This normalization  
factor is derived as follows:

$$\begin{aligned}\cosh(n \cosh^{-1} \omega_1) &= 1/\delta \\ \omega_1 &= \cosh \frac{1}{n} \cosh^{-1} 1/\delta \\ &= \cosh \frac{1}{n} \sinh^{-1} \sqrt{\frac{1-\delta}{\delta^2}}.\end{aligned}$$

If each pole is divided by this factor the response will be -3 db with respect to the peak response. It may be noted that, if the order of the polynomial is odd, the peak response is identical to the response at  $\omega = 0$ . Thus, the above formula will provide normalization to the DC response of the filter. However, if  $n$  is even, the response at  $\omega = 0$  is identical to that at the lower limit of the ripple; and, if it is desired to normalize the Tchebyscheff response with respect to the DC level of an even pole filter, a different factor must be used. This factor is derived as follows:

$$T_n^2(0) = 1 \text{ for even } n$$

$$|F(j0)|^2 = \frac{1}{1 + \delta^2 T_n^2(0)} = \frac{1}{1 + \delta^2}$$

$$|F(j\omega_{3dB})|^2 = \frac{1}{2(1 + \delta^2)} = \frac{1}{1 + \delta^2 T_n^2(j\omega_{3dB})}$$

solving for  $\omega_{3dB}$ ,

$$T_n^2(j\omega_{3dB}) = \frac{2(1 + \delta^2) - 1}{\delta^2} = \frac{2\delta^2 + 1}{\delta^2}$$

$$\cosh(n \cosh^{-1} \omega_{3dB}) = \frac{2\delta^2 + 1}{\delta^2}$$

$$\begin{aligned}\omega_{3dB} &= \cosh \frac{1}{n} \cosh^{-1} \frac{(2\delta^2 + 1)^{\frac{1}{2}}}{\delta} \\ &= \cosh \frac{1}{n} \sinh^{-1} \frac{(1 + \delta^2)^{\frac{1}{2}}}{\delta}\end{aligned}$$

Table B-1 contains the pole locations for Tchebyscheff filters of order 1 through 10 for various ripple factors. The poles are normalized for  $|F(1)|^2 = F(\omega_{peak})^2/2$ .

TABLE E-1 TCHEBYSCHOFF FILTER NORMALIZED POLE LOCATIONS

 $\delta = 0.15262042$  RIPPLE = 0.1 dB

Pole Nr. Poles	1		2		3		4		5	
	$\sigma$	$j\omega$	$\sigma$	$j\omega$	$\sigma$	$j\omega$	$\sigma$	$j\omega$	$\sigma$	$j\omega$
1	-1.0	0								
2	-.61041904	.71064977								
3	-.34895944	.86836557	-.69791888	0						
4	-.21775331	.92540643	-.52570299	.38331590						
5	-.14676218	.95210617	-.38422837	.58843397	-.47493238	0				
6	-.10494112	.96668431	-.28670448	.70766203	-.39164560	.25902228				
7	-.07850274	.97549887	-.21995978	.78228936	-.31785109	.43413784	-.35278809	0		
8	-.06082185	.98122944	-.17320598	.83184615	-.25922107	.55582183	-.30577210	.19517867		
9	-.04845365	.98516257	-.13951672	.86633742	-.21375202	.64301920	-.26220567	.34214337	-.27903344	0
10	-.03948065	.98797802	-.11457731	.89126784	-.17845835	.70731417	-.22487063	.45412365	-.24927102	.15648035

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.



TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.21709111$  RIPPLE = 0.2 dB

Pole Nr. Poles	1	2	3	4	5
1	-1.0	0			
2	-.57550005	.71384111			
3	-.31735974	.87031820	0		
4	-.19441483	.92662976			
5	-.12972133	.95292837			
6	-.09220663	.96727048	-.41978704		
7	-.06871748	.97593635	-.34411983	.25917934	
8	-.05310658	.98156780	-.27823139	.43433254	0
9	-.04223279	.98543177	-.22633880	.55601349	.19524597
10	-.03436782	.98819715	-.18630885	.64319491	.34223686
			-.15534761	.70747105	-.24320893
				-.19574941	-.21698990
					.15651505

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.26743094$  RIPPLE = 0.3 dB

Pole Nr.	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.55032824	.71684276								
3	-.29668017	.87209522	-.59336034	0						
4	-.17979926	.92772716	-.43407381	.38427717						
5	-.11929080	.95366066	-.31230736	.58939470	-.38603313	0				
6	-.08451407	.96779045	-.23089673	.70847178	-.31541080	.25931867				
7	-.06285494	.97632347	-.17611562	.78295063	-.25449444	.43450482	-.28246752	0		
8	-.04850939	.98186672	-.13814307	.83238641	-.20674571	.55618282	-.24387320	.19530543		
9	-.03854011	.98566934	-.11097183	.86678307	-.17001871	.64334997	-.20855883	.34231937	-.22194367	0
10	-.03134120	.98839038	-.09095571	.89163984	-.14166684	.70760939	-.17851063	.45431319	-.19788056	.15654566

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.34931140$  RIPPLE = 0.5 dB

Pole Nr.	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.51290914	.72246593								
3	-.26829311	.87532371	-.53658623	0						
4	-.16041786	.92969636	-.38728296	.38509284						
5	-.10569927	.95496685	-.27672429	.59020197	-.34205003	0				
6	-.07458969	.96871487	-.20378283	.70914851	-.27837252	.25956637				
7	-.05533807	.97701031	-.15505382	.78350144	-.22405927	.43481050	-.24868702	0		
8	-.04263892	.98239640	-.12142538	.83283546	-.18172593	.55648286	-.21436034	.19541079		
9	-.03383799	.98608991	-.09743261	.86715292	-.14927542	.64362448	-.18311341	.34246545	-.19486522	0
10	-.02749505	.98873224	-.07979375	.89194824	-.12428167	.70785413	-.15660404	.45447033	-.17359692	.15659980

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.



$\delta = 0.41820755 \quad \text{RIPPLE} = 0.7 \text{ dB}$ 

**Note:** Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

TABLE E-1 TCHEBYSCHOFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.50884714$  RIPPLE = 1.0 dB

Pole Nr. Poles	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.45076823	.73514239								
3	-.22567588	.88229691	-.45135176	0						
4	-.13251257	.93388164	-.31991365	.38682644						
5	-.08653231	.95772210	-.22654452	.59190481	-.28002442	0				
6	-.06075675	.97065684	-.16599053	.71057012	-.22674728	.26008672				
7	-.04493586	.97844963	-.12590747	.78465568	-.18194156	.43545105	-.20193990	0		
8	-.03455338	.98350459	-.09839970	.83377493	-.14726555	.55711060	-.17371156	.19563123		
9	-.02738277	.98696887	-.07884554	.86792586	-.12079837	.64419818	-.14818114	.34277069	-.15769107	0
10	-.02222734	.98944613	-.06450624	.89259225	-.10047083	.70836522	-.12660063	.45479847	-.14033788	.15671287

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

$\delta = 0.64229086$  RIPPLE = 1.5 dB

Pole Nr. Poles	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.40779353	.74658558								
3	-.19865287	.88835170	-.39730574	0						
4	-.11541929	.93746599	-.27864681	.38831113						
5	-.07498787	.96006691	-.19632080	.59335398	-.24266585	0				
6	-.05250299	.97230390	-.14344084	.71177586	-.19594383	.26052805				
7	-.03876473	.97966790	-.10861635	.78563265	-.15695517	.43599323	-.17420710	0		
8	-.02977466	.98444135	-.08479106	.83456908	-.12689879	.55764123	-.14968733	.19581756		
9	-.02357751	.98771119	-.06788874	.86857865	-.10401158	.64468269	-.12758909	.34302850	-.13577747	0
10	-.01912789	.99004866	-.05551131	.89313580	-.08646089	.70879659	-.10894708	.45507542	-.12076877	.15680830

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.



TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.76478310$  RIPPLE = 2.0 dB

Pole Nr. Poles	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.37416689	.75720472								
3	-.17860959	.89382276	-.35721919	0						
4	-.10299556	.94067582	-.24865328	.38964068						
5	-.06667806	.96215824	-.17456543	.59464650	-.21577474	0				
6	-.04659352	.97376976	-.12729586	.71284894	-.17388937	.26092082				
7	-.03436071	.98075074	-.09627656	.78650103	-.13912367	.43647514	-.15441562	0		
8	-.02637157	.98527329	-.07509987	.83527436	-.11239489	.55811249	-.13257882	.19598304		
9	-.02087161	.98837008	-.06009740	.86915806	-.09207456	.64511275	-.11294616	.34325733	-.12019480	0
10	-.01692620	.99058325	-.04912174	.89361806	-.07650891	.70917931	-.09640685	.45532115	-.10686781	.15689297

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

TABLE E-1 TCHEBYSCHIEFF FILTER NORMALIZED POLE LOCATIONS (cont'd)

 $\delta = 0.99762835$  RIPPLE = 3.0 dB

Pole Nr. Poles	1		2		3		4		5	
	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$	$\sigma$	$\omega$
1	-1.0	0								
2	-.32225836	.77669610								
3	-.14927069	.90357584		0						
4	-.08515775	.94634388	-.29854138	.39198847						
5	-.05485466	.96583567	-.20558900	.59691927	-.17751340	0				
6	-.03822699	.97634157	-.14361136	.71473163	-.14266507	.26160993				
7	-.02814428	.98264803	-.10443808	.78802253	-.11395386	.43731951	-.12647924			
8	-.02157736	.98672971	-.07885851	.83650906	-.09196210	.55893748	-.10847669	.19627274		
9	-.01706470	.98952288	-.06144711	.87017182	-.07528048	.64586519	-.09234518	.34365769	-.09827169	0
10	-.01383163	.99151820	-.04014096	.89446149	-.06252102	.70984866	-.07878108	.45575089	-.08732949	.15704105

Note: Only the poles in the second quadrant are shown. The conjugate of all complex poles is implied.

# APPENDIX F

## DIGITAL FILTER DESIGN

### F.1 THE BILINEAR Z-TRANSFORMATION

The bilinear Z-transformation is a convenient means of converting an S-domain transfer function into a Z-domain transfer function which is compatible with digital filter design techniques. Of particular interest in this appendix is the use of the Z-transform to obtain high-pass or low-pass digital filter designs from normalized (i.e.,  $\omega_{3db} = 1$ ) S-domain low-pass filter transfer functions. The bilinear Z-transformation is defined by the following expression:

$$S = \frac{2}{T} \frac{1-Z^{-1}}{1+Z^{-1}} \quad (F-1)$$

where T is the discrete sampling interval. This transformation maps the entire left-half of the S-plane into the area inside the Z-plane unit circle, and maps the right-half S-plane into the area outside of the unit circle. The S-plane  $j\omega$  axis becomes the unit circle with  $j\omega=0$  mapped to  $Z = +1$  and  $j\omega=\pm\infty$  mapped to  $Z = -1$ . This results in a non-linear warping of the frequency scale according to the relation

$$\frac{\omega_c T}{2} = \tan\left(\frac{\omega_d T}{2}\right) = \Omega \quad (F-2)$$

where  $\omega_c$  is the S-plane frequency and  $\omega_d$  is the corresponding Z-plane frequency. For convenience, the parameter  $\Omega$  will be used to represent  $\tan\left(\frac{\omega_d T}{2}\right)$  in the remainder of this appendix. Compensation can be made for the warping effect of the bilinear Z-transform by prewarping the filter cutoff frequency. This is accomplished by solving equation F-2 for T/2 and substituting the resulting expression into equation F-1.

$$S = \frac{\omega_c}{\Omega} \frac{1-Z^{-1}}{1+Z^{-1}} \quad (F-3)$$



### F.1.1 Low Pass to Low Pass (High Pass to High Pass) Transformation

In order to transform a normalized S-plane filter design ( $\omega_c=1$ ) to a Z-plane representation with cutoff frequency  $\omega_d$ , equation F-3 is solved for Z after 1.0 is substituted for  $\omega_c$ . The following equation gives the relationship between the S-plane and Z-plane poles (zeros).

$$Z = \frac{1/\Omega + S}{1/\Omega - S} \quad (F-4)$$

### F.1.2 Low Pass to High Pass (High Pass to Low Pass) Transformation

In order to transform a low pass S-plane transfer function to its high pass complement in the Z-plane, the following complementary transformation in the S-plane is performed first

$$S = 1/S' \quad (F-5)$$

where  $S'$  is the new pole (zero) location in the S-plane. When the substitution specified by equation F-5 is made in equation F-4 the following transform is obtained

$$\begin{aligned} Z &= \frac{1/\Omega + 1/S'}{1/\Omega - 1/S'} \\ &= \frac{S' + \Omega}{S' - \Omega} \end{aligned} \quad (F-6)$$

## F.2 DETERMINING DIGITAL FILTER COEFFICIENTS

Once the transfer function of a filter has been determined in the Z-plane, it is a simple procedure to determine the feedforward and feedback coefficients of a digital filter.

Assume the Z-plane transfer function is defined by the following equation.

$$H(Z) = K_1 K_2 \frac{(Z-Z_{01})(Z-Z_{01}^*)(Z-Z_{02})(Z-Z_{02}^*)}{(Z-Z_{p1})(Z-Z_{p1}^*)(Z-Z_{p2})(Z-Z_{p2}^*)}$$

where the asterisk indicates the complex conjugate. This equation can be rewritten in the form

$$H(Z) = K_1 \frac{(Z-Z_{01})(Z-Z_{01}^*)}{(Z-Z_{p1})(Z-Z_{p1}^*)} \cdot K_2 \frac{(Z-Z_{02})(Z-Z_{02}^*)}{(Z-Z_{p2})(Z-Z_{p2}^*)} \quad (F-7)$$

The second form of this equation indicates that any physically realizable transfer function can be implemented by cascading quadratic filter sections. Therefore, the analysis can be limited to a single quadratic section with no loss in generality. One section of equation F-7 is expanded to give the following

$$G(Z) = K \frac{Z^2 - 2Z\text{Re}\{z_o\} + |z_o|^2}{Z^2 - 2Z\text{Re}\{z_p\} + |z_p|^2}, \quad (F-8)$$

where  $\text{Re}\{ \}$  represents the real part of  $\{ \}$ .

Since this is a quadratic in  $Z$ , it should be possible to implement the function by a double delay filter as shown in Figure F.1-1. The transfer function for this filter will now be determined and compared with equation F-8 above.

$$E_o = \left[ \frac{1}{Z^2} E_2 + B_2 \frac{1}{Z} E_2 + B_1 E_2 \right] C \quad (F-9)$$

$$E_2 = E_i + A_1 \frac{1}{Z} E_2 + A_2 \frac{1}{Z^2} E_2. \quad (F-10)$$

By solving equation F-10 for  $E_2$  and substituting into equation F-9, the following expression is obtained.

$$\frac{E_o}{E_i} = C \left[ \frac{B_1 Z^2 + B_2 Z + 1}{Z^2 - A_1 Z - A_2} \right]. \quad (F-11)$$

If  $B_1$  is factored from the numerator, the following expression results:

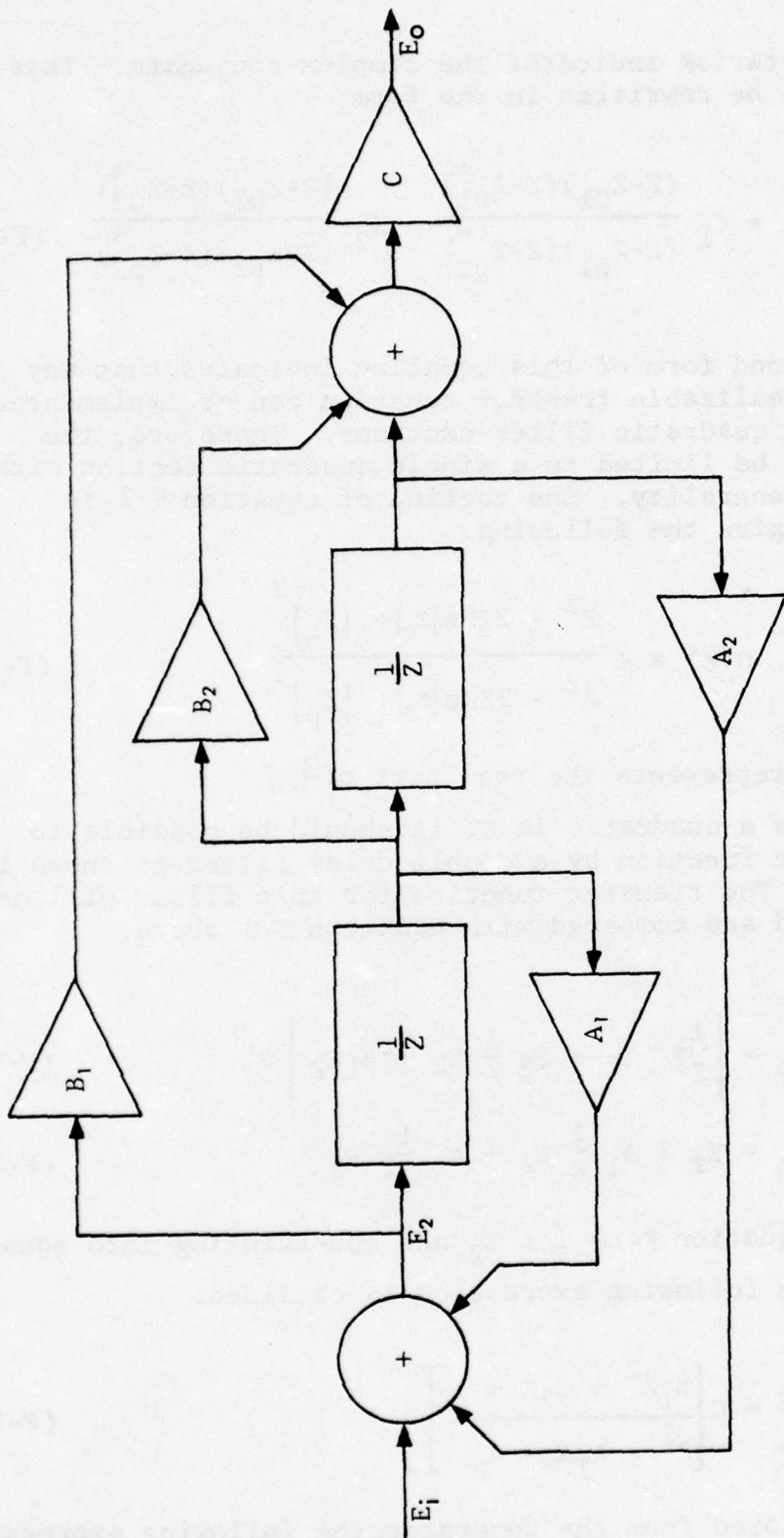


Figure F.1-1 DOUBLE-DELAY DIGITAL FILTER DIAGRAM



$$\frac{E_o}{E_i} = CB_1 \left[ \frac{z^2 + \frac{B_2}{B_1} z + \frac{1}{B_1}}{z^2 - A_1 z - A_2} \right] \quad (F-12)$$

By comparing F-12 with equation F-8, the values of the feed-forward and feedback coefficients shown in Figure F-1 can be determined from the Z-plane pole/zero locations:

$$B_1 = \frac{1}{|Z_o|^2} \quad (F-13)$$

$$B_2 = -2B_1 \operatorname{Re}(Z_o) \quad (F-14)$$

$$C = \frac{K}{B_1} \quad (F-15)$$

$$A_1 = 2\operatorname{Re}(Z_p) \quad (F-16)$$

$$A_2 = -|Z_p|^2. \quad (F-17)$$

### F.3 EXAMPLES OF DIGITAL FILTER DESIGNS

#### F.3-1 Low Pass Filter Design

This example will demonstrate the design of a 2-pole Tchebyscheff low-pass filter with a 0.5 dB pass-band ripple, a 3 dB cutoff frequency of 10 Hz, and a pass-band gain of 1. The sample rate is 100 Hz. The S-plane representation (from the table in Appendix E) of the low-pass filter is

$$G(S) = \frac{1}{(s+.5129091-j.7224659)(s+.5129091+j.7224659)}.$$

Substituting the above parameters into equations F-2 and F-4 the following results are obtained.

$$\Omega = \tan \left( \frac{f_d \times 180}{f_s} \right) = \tan 18^\circ = 0.3249197, \text{ and}$$

$$z_p = \frac{\frac{1}{\Omega} + s}{\frac{1}{\Omega} - s} = .6475996 + j.3315148$$

$$z_p^* = .6475996 - j.3315148.$$

The double zero at infinity is represented by

$$z_{01} = z_{02} = -1.0.$$

Thus, the transfer function in the Z-plane is

$$H(Z) = \frac{(Z + 1)(Z + 1)}{(Z - .6475996 - j.3315148)(Z - .6475996 + j.3315148)}.$$

From the roots in the Z-plane, the filter coefficients are determined using equations F-13 through F-17:

$$B_1 = \frac{1}{1^2} = 1$$

$$B_2 = -2(1)(-1) = 2$$

$$A_1 = 2(.6475996) = 1.295199$$

$$A_2 = -(.6475996^2 + .3315148^2) = -.5292872.$$

The impulse response of this filter is shown in Figure F.3.1-1.

### F.3.2 High Pass Filter Design

This example problem demonstrates the design of a 2-pole Tchebyscheff high-pass filter with a 100 Hz stopband, 1-dB

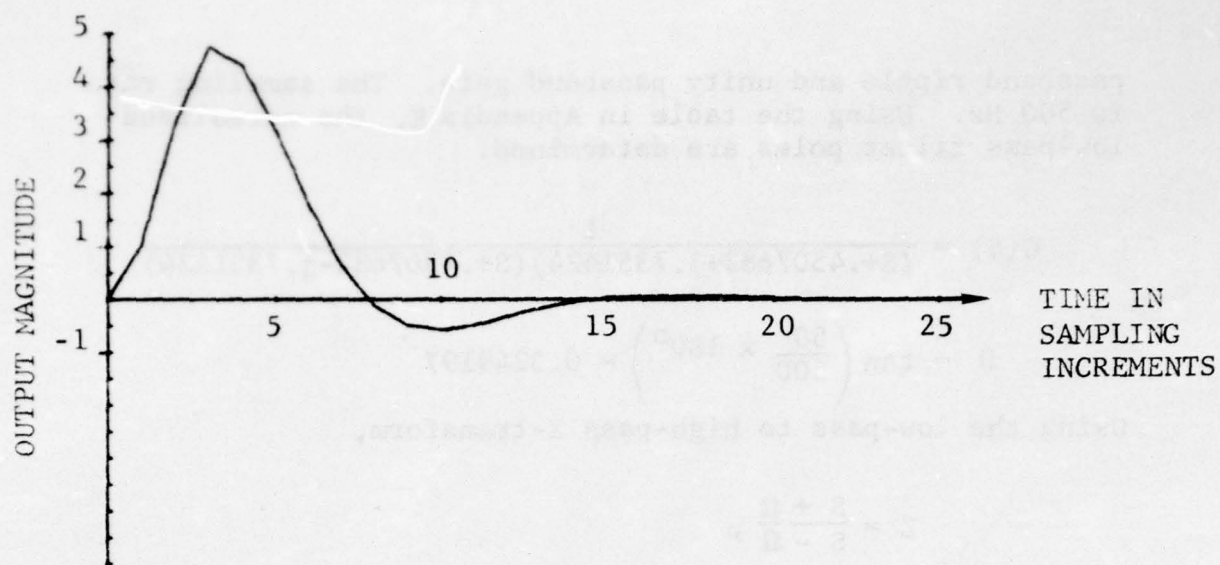


Figure F.3.1-1 IMPULSE RESPONSE - 0.5 dB TCHEBYSCHIEFF  
LOWPASS FILTER

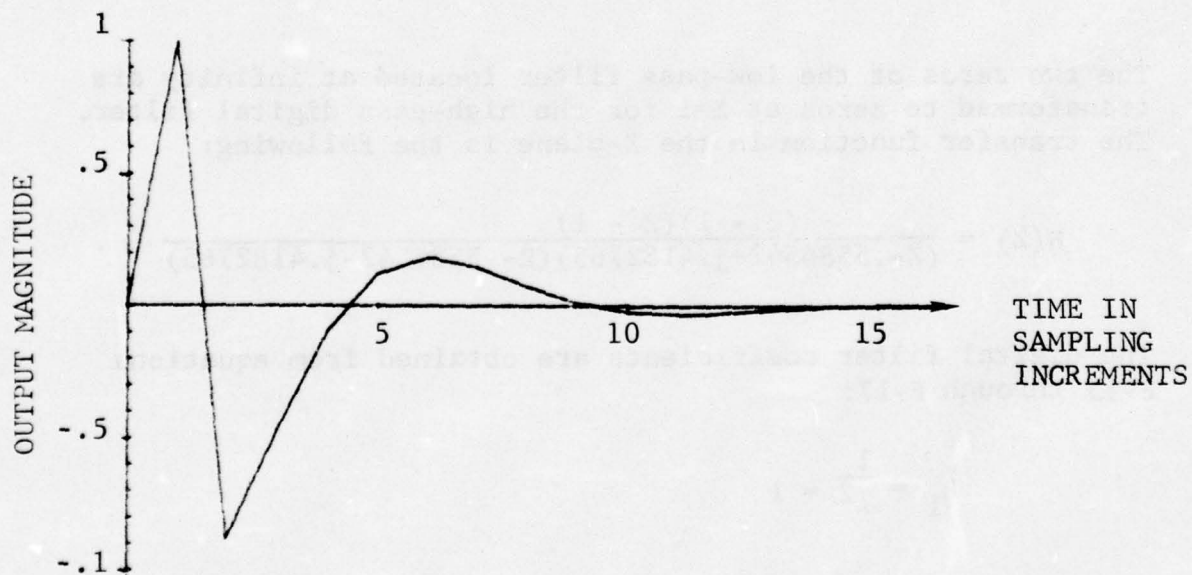


Figure F.3.2-1 IMPULSE RESPONSE - 1dB TCHEBYSCHIEFF  
HIGHPASS FILTER



passband ripple and unity passband gain. The sampling rate is 500 Hz. Using the table in Appendix E, the normalized low-pass filter poles are determined:

$$G(S) = \frac{1}{(S+.4507682+j.7351424)(S+.4507682-j.7351424)}$$

$$\Omega = \tan\left(\frac{50}{500} \times 180^\circ\right) = 0.3249197$$

Using the low-pass to high-pass Z-transform,

$$Z = \frac{S + \Omega}{S - \Omega},$$

the roots of the denominator are determined to be

$$Z_p = .5586542 - j.4182765$$

$$Z_p^* = .5586542 + j.4182765.$$

The two zeros of the low-pass filter located at infinity are transformed to zeros at  $Z=1$  for the high-pass digital filter. The transfer function in the Z-plane is the following:

$$H(Z) = \frac{(Z - 1)(Z - 1)}{(Z - .5586542 + j.4182765)(Z - .5586542 - j.4182765)}.$$

The digital filter coefficients are obtained from equations F-13 through F-17:

$$B_1 = \frac{1}{1^2} = 1$$

$$B_2 = -2(1)(1) = -2$$

$$C = 1$$

$$A_1 = 2(.5586542) = 1.117308$$

$$A_2 = -.4870497.$$

The impulse response of this filter is shown in Figure F.3.2-1.

### F.3.3 Integrator Design

This example will demonstrate the design of a simple integrator with a 3 dB cutoff of one tenth the sampling rate and no Z-plane zeros. The S-plane representation of an integrator is the following

$$G(S) = \frac{1}{S + 1}$$

Substituting  $S_p = -1$  and  $\Omega = .3249197$  into equation F-4, the Z-plane pole is determined to be

$$Z = 0.5095254.$$

Since no Z-plane zeros are to be simulated, the Z-plane transfer function is

$$H(Z) = \frac{1}{Z - .5095254}.$$

The filter coefficients are the following:

$$B_1 = 0$$

$$B_2 = 0$$

$$C = 1$$

$$A_1 = 0.5095257$$

$$A_2 = 0.$$

The integrator impulse response is shown in Figure F.3.3-1.

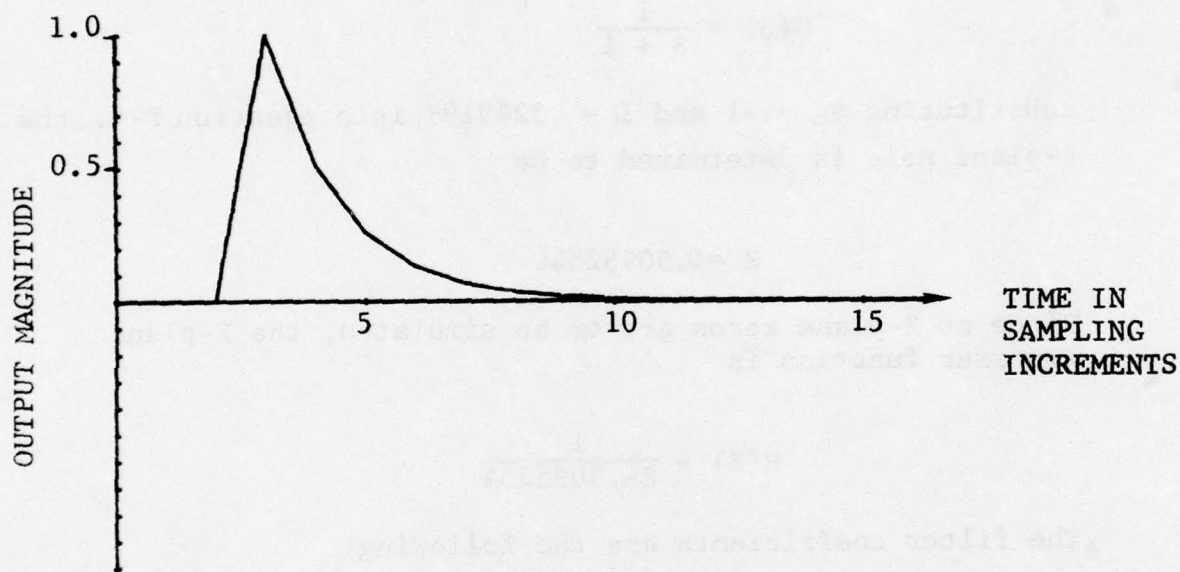


Figure F.3.3-1 IMPULSE RESPONSE - DIGITAL INTEGRATOR



A P P E N D I X   G  
C O M P U T E R   P R O G R A M  
U S E D   I N   R E A D I N G  
R A D A R   C R O S S   S E C T I O N   T A P E S

The documentation and listing of the computer program used in reading radar cross-section tapes is provided in this appendix.

SUBROUTINE DATAIN

1. MODULE IDENTIFICATION:

<u>Name</u>	<u>Classification Code</u>	<u>Reference Number</u>
DATAIN	Subroutine	Not user referenced

2. PURPOSE:

This subprogram is used to read Radar Cross Section data types generated by the General Dynamics/Ft. Worth RCS measurement range.

3. INPUT PARAMETERS:

None

4. CALLING SEQUENCES:

CALL DATAIN

Where: Data is passed via blank common.

5. RESTRICTIONS, REQUIREMENTS, AND MISCELLANEOUS DATA:

- (a) Data read from the magnetic tape is placed in an array INDAT. In addition, a status word IERW is generated to indicate errors during read, if any. The specification in Fortran of the blank common area containing the above follows:

COMMON INDAT(309), IDUM(3), IERW

IDUM(3) allocates storage for status words used by the subroutine.

- (b) The character sets of the RCS tapes and the Honeywell computer differ in the representation of "=" and "+" signs. Therefore, this routine connects all occurrences of the above 2 characters into their appropriate representation in the Honeywell character set.
- (c) The following GCOS Master Mode Entry (MME) routines are used in this subroutine:  
  
GEINDS and GEROAD. Reference GCOS manual BR43C for an explanation of these routines.
- (d) The file code allocated for the magnetic tape is 13. If a different file code is desired, the variable FA should be changed accordingly.
- (e) This subroutine is structured to read records that are 1850 characters in length.

## 6. THEORY OF OPERATION

Upon entry to the subroutine, the necessary control words for GEINDS are set up and GEINDS is called. GEROAD is called to halt execution of the program until a record is read from the magnetic tape unit. Upon completion of the read, the status word returned by GEINDS is processed to determine if an error occurred and a status word, IERR, is generated for use by the calling program. The values of IERR are the following:

IERR = 0 No error detected  
      = 1 End of file  
      = 2 Longitudinal parity error detected  
      = 3 Lateral parity error detected  
      = 4 Error detected but not one of the above  
      = 16 Blank tape on read

If the last word of the record is incomplete, the 10 is added to IERR. If the record is short by more than 1 word, then 20 is added to IERR.

10		SYNDEF	DATAIN	
20		BLOCK		BLANK COMMON
30	INDAT	BSS	309	BUFFER AREA
40	IPEF	BSS	1	CHAR/WORD XMITTAL STATUS
50	STATW	BSS	2	STATUS RETURN WORD
60	IERR	BSS	1	ERROR RETURN TO CALLING PROGRAM
70		USE	PREVIOUS	
80	DATAIN	SAVE		ENTRY POINT
90		LDA	DCW1	
100		STA	DCW	
110		LDA	=-2	
120		STA	STATR	
130		MME	GEINOS	
140		RTD		
150		ZERO	FA,DCW	FILE CODE WORD, DATA CONTROL WORD
160		ZERO	STATR	STATUS RETURN WORD
170		MME	GEROAO	
180		LDQO	STATR	
190		STAQ	STATW	
200		ANA	=0070000, DU	
210		TZE	ERRF	NO ERRORS DETECTED BY TAPE CONTR
220		CMFA	=0040000, DU	
230		TZE	EOF	END OF FILE DETECTED
240		CMFA	=0030000, DU	
250		TZE	DALRT	DATA ALERT DETECTED
260		LDA	=4, DL	
270		TRA	ERRF	UNKNOWN ERROR DETECTED
280	EOF	LDA	=1, DL	END OF FILE
290	EXIT	STA	IERR	
300		TRA	RTURN	
310	DALRT	LDA	STATR	DATA ALERT
320		ANA	=0007700, DU	
330		CMFA	=0000200, DU	TEST FOR BLANK TAPE ON READ
340		TNZ	PCK	
350		LDA	=16, DL	
360		TRA	EXIT	
370	PCK	ANA	=0001000, DU	
380		TNZ	LATPC	LONGITUDINAL PARITY CHECK
390		LDA	=2, DL	
400		TRA	ERRF	LATERAL PARITY CHECK
410	LATPC	LDA	=3, DL	
420	ERRF	STA	IERR	TEST RECORD LENGTH READ
430		AND	=0707777, DL	CHAR/WORD REMAINING TO XFER
440		STQ	IPEF	
450		TZE	TEST3	
460		LLS	21	A=NUMBER OF CHAR IN LAST WORD
470		QRS	21	Q=NUMBER OF WORDS NOT XMITTED
480		CMFQ	=1, DL	
490		TZE	SREC	If Q = 1; then ZERO = 1
500		TNC	CARCK	If Q < 1; then CARRY = 0
510		LDQ	=20, DL	SHORT REC- MORE THAN 1 WORD DEFECTIVE
520		TRA	ENDE	
530	CARCK	CMFA	=2, DL	
540		LDA	IERR	
550		TNC	SREC	If A < 2; then CARRY = 0
560	TEST3	CMFA	=3, DL	
570		TNZ	CHTL	If A ≠ 3; then ZERO = 0
580		LDA	=0, DL	
590		STA	IERR	
600		TRA	CHTL	
610	SREC	LDQ	=10, DL	SHORT RECORD-LAST WORD DEFECTIVE



620	ENDE	ASQ	IERR	COMBINE REC. LENG. TEST WITH IOC STAT.
630	CHTL	LDX0	=0, DU	CHARACTER TRANSLATE + AND = SIGNS
640	NWORD	CMPX0	=309, DU	BEGINNING OF WORD LOOP
650		TZE	RTURN	
660		LDA	INDAT, 0	X0 IS INDEX REGISTER
670		LDX1	=6, DU	
680		LQ0	=0777777777700	
690	TESTC	NOP		BEGINNING OF CHAR. LOOP
700		CMK	=013, DL	TEST RIGHT MOST CHAR FOR =
710		TZE	EQUAL	
720		CMK	=032, DL	TEST RIGHT MOST CHAR FOR +
730		TZE	PLUS	
740	ROTAT	ALR	6	
750		SBX1	=1, DU	
760		TNZ	TESTC	END OF CHAR. LOOP
770		STA	INDAT, 0	
780		ADX0	=1, DU	
790		TRA	NWORD	END OF WORD LOOP
800	EQUAL	ERA	=0000066, DL	CORRECT = SIGN
810		TRA	ROTAT	
820	PLUS	ERA	=0000052, DL	CORRECT + SIGN
830		TRA	ROTAT	
840	RTURN	RETURN	DATAIN	RETURN TO CALLING PROGRAM
850	FA	BCI	1, 000013	
860	STATR	EBSS	2	
870	DCW1	IOTD	INDAT, 309	BUFFER ARRAY, NUMBER OF WORDS XMITTED
880	DCW	BSS	1	
890		END		

	1	2	4	8	A	B	C	
1	1	1	1	1	1	1	1	Record Prefix (*)
2	/	/	/	/	/	/	/	MSD Model Number
3	/	/	/	/	/	/	/	LSD or Calibration Data Code
4	/	/	/	/	/	/	/	Run Number (Used when all other identifiers are repeated)
5	/	/	/	/	/	/	/	Frequency (1-UHF, 2-L-Band, 3-S-Band, 4-C-Band, 5-X-Band)
6	/	/	/	/	/	/	/	Blank
7	/	/	/	/	/	/	/	Polarization (Trans-RCV: 1-VV, 2-HH, 3-VH, 4-HV)
8	/	/	/	/	/	/	/	MSD
9	/	/	/	/	/	/	/	Full Scale Range Sweep in Inches
10	/	/	/	/	/	/	/	LSD
11	/	/	/	/	/	/	/	Blank
12	/	/	/	/	/	/	/	MSD
13	/	/	/	/	/	/	/	Record Number (Progressive from 0000)
14	/	/	/	/	/	/	/	LSD
15	/	/	/	/	/	/	/	Data Prefix (/)
16	1	/	/	/	/	/	/	MSD Block Number
17	/	/	/	/	/	/	/	LSD (00 for this application)
18	/	/	/	/	/	/	/	Blank
19	/	/	/	/	/	/	/	Blank
20	/	/	/	/	/	/	/	Blank
21	/	/	/	/	/	/	/	Sign
22	1	/	/	/	/	/	/	MSD
23	1	/	/	/	/	/	/	$\pm$ 9999
24	1	/	/	/	/	/	/	LSD
25	1	/	/	/	/	/	/	Sign
26	/	/	/	/	/	/	/	MSD
27	X	X	X	X	X	X	X	In-phase component
28	X	X	X	X	X	X	X	in Millivolts
29	X	X	X	X	X	X	X	LSD
30	X	X	X	X	X	X	X	Sign
31	/	/	/	/	/	/	/	MSD
32	X	X	X	X	X	X	X	Quadrature component
33	X	X	X	X	X	X	X	in Millivolts
34	X	X	X	X	X	X	X	LSD
35	X	X	X	X	X	X	X	Sign
36	/	/	/	/	/	/	/	MSD
37	X	X	X	X	X	X	X	Amplitude Component
38	X	X	X	X	X	X	X	in Millivolts
39	X	X	X	X	X	X	X	LSD
40	X	X	X	X	X	X	X	
1821	/	/	/	/	/	/	/	Blank
1822	/	/	/	/	/	/	/	Blank
1823	/	/	/	/	/	/	/	Sign
1824	X	X	X	X	X	X	X	MSD
1825	X	X	X	X	X	X	X	Attenuation Level
1826	X	X	X	X	X	X	X	LSD
1827	X	X	X	X	X	X	X	MSD
1828	X	X	X	X	X	X	X	Cal Phase on Cal Runs in Degrees
1829	X	X	X	X	X	X	X	LSD
1830	/	/	/	/	/	/	/	Sign
1831	X	X	X	X	X	X	X	MSD
1832	X	X	X	X	X	X	X	Pitch Angle in Tenths of Degrees
1833	X	X	X	X	X	X	X	LSD
1834	X	X	X	X	X	X	X	MSD
1835	X	X	X	X	X	X	X	Roll Angle in Tenths of Degrees
1836	X	X	X	X	X	X	X	LSD
1837	/	/	/	/	/	/	/	Sign
1838	X	X	X	X	X	X	X	MSD
1839	X	X	X	X	X	X	X	Yaw, Azimuth, or Aspect in Tenths of Degrees
1840	X	X	X	X	X	X	X	LSD
1841	X	X	X	X	X	X	X	MSD
1842	X	X	X	X	X	X	X	Yaw, Azimuth, or Aspect in Tenths of Degrees
1843	X	X	X	X	X	X	X	LSD
1844	/	/	/	/	/	/	/	Sign
1845	X	X	X	X	X	X	X	MSD
1846	X	X	X	X	X	X	X	Yaw, Azimuth, or Aspect in Tenths of Degrees
1847	X	X	X	X	X	X	X	LSD
1848	X	X	X	X	X	X	X	MSD
1849	X	X	X	X	X	X	X	Yaw, Azimuth, or Aspect in Tenths of Degrees
1850	X	X	X	X	X	X	X	LSD
X X X X X X X X								Longitudinal Parity
1 1 1 1 1 1 1 1								Next Record

Notes:

- 1) All Recordings @ 800 BPI in BCD Code
- 2) 

1	Fixed Format Bits
1	Fixed Format Zero
1	Auto or Preset
1	Bit Changes
X	Data Bit Changes

Fig. C-1 MAGNETIC TAPE FORMAT FOR SHORT PULSE DATA

A P P E N D I X   H  
C O M P U T E R   P R O G R A M   F O R  
I M A G I N G   C O H E R E N T  
S H O R T   P U L S E   T A R G E T   D A T A

A printed-out listing of the computer program for imaging coherent short pulse target data is provided in this appendix. The computer program documentation together with a sample program is located in Volume I, Part 3, Section 8.17.



```

10      C      FILE=IMAGP
20          COMMON INDAT(309), IPEF, STATW(2), IERW
30          CHARACTER INDAT1*480, INDAT2*480, INDAT3*480, INDAT4*414
40          EQUIVALENCE (INDAT(1), INDAT1), (INDAT(81), INDAT2),
50          *      (INDAT(161), INDAT3), (INDAT(241), INDAT4)
60          COMMON/BLOCK1/NPTS, ITC, KAY, DELTAY, DATA(540)
70          COMMON /BLOCK3/ THOLD, DRANG, IA, ITH, ICTRL
80          COMMON/BLOCK9/ ICTRL, RP, RN, SP, SN, ISET, NEND, THT
90          COMMON/BLK1/BK1(500)
100         COMMON/BLCK11/XFI( 40,250), XFO( 40,250), XFII( 64,250)
110         1, ITI, TOI, DELI, DDI, XRI(128), ITQ, TOQ, DELQ, DDQ, XRO(128)
120         DIMENSION          IDATA(540)          , IDATAI(540)          , IDATAQ(540)          ,
130         1IIA(2)          , HEADR(3)          , TRAILR(3)          , ITHETA(2)          ,
140         2THDES(40)          , IFSKP(20)          , SYSATT(4)          , THMISS(30)          ,
150         3TSWNDQ(10)
160         DIMENSION W(40), TGTID(10)
170         CHARACTER TGTID
180         EQUIVALENCE(M2, BK1(1))
190         DATA PI, PIO2, DTR, RTD/3. 14159265, 1. 5707963, 1. 74533E-02, 57. 29578/
200         DIMENSION CTABL(50)
210         DATA CTABL/020, 020, 020, 052, 071, 070, 067, 066, 065, 064, 063,
220         *      062, 051, 050, 047, 046, 045, 044, 043, 042, 041, 031, 030,
230         *      027, 026, 025, 024, 023, 022, 021, 011, 010, 007, 006, 005, 004,
240         *      003, 002, 001, 000, 013, 060, 032, 033/
250         NAMELIST/CARD1/ TGTID, NBRTGT
260         NAMELIST/CARD2/ KAY, DELTAY, NWNDOS
270         NAMELIST/CARD3/ DRANG, CTGT, THINC, THOLD, FREQ
280         NAMELIST/CARD4/ NFILES          , NRPS, IR0, LAST, INOISE, NTH, M2, INCX
290         NAMELIST/CARD5/ M2C, NTH0, ADELV
300         NAMELIST/CARD6/ NFSKP, IFSKP
310         NAMELIST/CARD8/ SYSATTQ, TSWNDQ, IFSEP
320         5 READ (5, CARD1)
330         WRITE(6, 2060) TGTID, NBRTGT
340         2060 FORMAT( ' TARGET =', 10A6, ' NBRTGT=', 15)
350         READ (5, CARD2)
360         WRITE (6, CARD2)
370         IF( NWNDOS .GT. 0 ) GO TO 6
380         WRITE (6, 1002)
390         1002 FORMAT( ' NWNDOS IS INCORRECT ' )
400         CALL EXIT
410         6 CONTINUE
420         NWNDQ = 1
430         READ (5, CARD3)
440         WRITE (6, CARD3)
450         C
460         ALMDA = 11. 8/FREQ
470         AK =(2*PI)/ALMDA
480         AKR = AK*DRANG
490         ACTGT = AK*CTGT
500         THOLD1 = 20. 0*ALOG10(THOLD)
510         THTEST = 10. *THINC
520         DTH = 0. 5*THINC
530         READ (5, CARD4)
540         WRITE (6, CARD4)
550         ZNS = INOISE
560         NPTS = LAST - IR0 + 1
570         NPTSF = NPTS/INCX
580         NTH1 = NTH + 1
590         NTHN = 2**M2

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600      ITI=NTHN
610      ITQ=NTHN
620      XNTH = NTH
630      NTH02= NTHN/2
640      NT02 = NTH/2
650      XNT2=(NTH - NT02)
660      AKN=PI02/XNT2
670
680      C
690      C ***** WEIGHTING FUNCTION DEFINITION *****
700      C
710      NT02X=NT02-1
720      DO 17 I=1,NTH
730      NTH = AKN*(NT02X-I)
740      CXTH = COS(XTH)
750      W(I)=0.08+0.92*CXTH*CXTH
760      17 CONTINUE
770      WRITE(6,7676) W
780      7676 FORMAT(' WEIGHTING FUNCT=',6F10.5,(' /6F10.5'))
790      C
800      WRITE (6, 7500) NPTS, NTH, ZNS, NPTSF
810      7500 FORMAT (' NPTS =',15,'/' NTH =',15,'/' ZNS =',F10.3,'/'
820      1 ' NPTSF =',15 ' )
830      C
840      IF (NFILES .GT. 0 .AND. NFILES .LT. 30) GO TO 8
850      WRITE (6,1004)
860      1004 FORMAT (' NFILES INCORRECT ')
870      CALL EXIT
880      8 CONTINUE
890      NWDS = 90*NRPS
900      NBA = 1852
910      IF( NRPS .GT. 0 .AND.
920      1 NRPS .LE. 6 ) GO TO 10
930      WRITE (6,2020)
940      2020 FORMAT(' NRPS INCORRECT ' )
950      CALL EXIT
960      10 CONTINUE
970      C
980      READ (5,CARD5)
990      NPTSS = 2**M2C
1000      WRITE(6,4001) NPTSS, NTHN, NTH0, ADELV
1010      4001 FORMAT (' NUMBER OF POINTS TRANSFORMED IN TIME DOMAIN =',15,'/'
1020      1 ' NUMBER OF POINTS IN ANGLE TRANSFORM =',15,'/' NUMBER OF THRES
1030      2HOLDS IN RTI =',15,'/' EXPECTED MAXIMUM AMPLITUDE OF IMAGE =',
1040      3F8.4)
1050      XU = NPTSF+NTHN*KAY
1060      YL = 0.0
1070      YU = ADELV + NTHN*DELTAY
1080      READ (5,CARD6)
1090      WRITE (6,2030)( IFSKP(J),J=1,NFSKP )
1100      2030 FORMAT(' FILES TO BE SKIPPED ',/' ',10(2X,15) )
1110      C
1120      C
1130      JMISS = 0
1140      IFILE = 1
1150      ISKP = 1
1160      C***** ***** *****
1170      C
1180      READ (5,CARD8)
1190      SYSATT(1)=SYSATQ
1200      TSWNDO(1)=TSWNDO
1210      11 CONTINUE
1220      ITHFG = 0
1230      THDES(1) = TSWNDO(NWNDO)
1240      DO 40 J=2,NTH
1250      THDES(J) = THDES(J-1) + THINC
40 CONTINUE

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1260      245 THFIN = THDES(NTH)
1270      IF ( THFIN GE. 360.0 ) ITHFG = 1
1280      WRITE (6,7610) NWND0, SYSATT(1), THDES(1), THDES(NTH)
1290      7610 FORMAT(// 'ASPECT WINDOW NUMBER',12,/' SYSATT =',F8.2,/'
1300      1 ' WINDOW FROM ',F6.1,/' TO ',F6.2,/' DEGREES ' )
1310      C
1320      DO 45 J=1,NPTSF
1330      DO 45 JJ=1,NTH
1340      XFO (JJ,J) = 0.0
1350      XFI (JJ,J) = 0.0
1360      45 CONTINUE
1370      C
1380      ICTRL = 1
1390      IOFT = 1
1400      IOFASM = 1
1410      IMISS = 0
1420      NN = 0
1430      ITH = 0
1440      ISPTST = 0
1450      C
1460      250 IF( IFILE .NE. IFSKP(ISKP) ) GO TO 270
1470      WRITE (6,6006)
1480      6006 FORMAT ( ' FILE TEST START ', )
1490      251 CONTINUE
1500      CALL DATIN
1510      IF(IERN.EQ.0) GOTO 251
1520      CALL ERRPRC
1530      IF(IERN.EQ.1) GOTO 255
1540      GOTO 251
1550      C
1560      255 WRITE (6,7000) IFILE
1570      7000 FORMAT( ' BYPASSED FILE ',15 )
1580      265 IFILE = IFILE + 1
1590      IF( ISKP GE. NFSKP ) GO TO 270
1600      ISKP = ISKP + 1
1610      GO TO 250
1620      C
1630      270 WRITE (6,6007)
1640      6007 FORMAT ( ' FILE TEST END - FILE PROCESS BEGIN ',110)
1650      C
1660      IPASS = 1
1670      IGER = 0
1680      IGN = 0
1690      I9TST = 0
1700      IK = 0
1710      275 ITH = ITH + 1
1720      C
1730      278 ISRT = 1
1740      IHD = 3
1750      280 CONTINUE
1760      CALL DATIN
1770      292 ISTP = ISRT + 89
1780      IF( ISRT .EQ. 91 ) IHD = 1
1790      IF( ISRT .EQ. 181 ) IHD = 2
1800      IF(IERN.EQ.0.OR.IERN.EQ.10.OR.IERN.EQ.13) GOTO 52
1810      CALL ERRPRC
1820      IF(IERN.EQ.1) GOTO 310
1830      IF(IERN.GE.20) GOTO 70
1840      GOTO 315
1850      C
1860      C
1870      52 IF ( IHD .EQ. 3 ) GO TO 290
1880      ISRTE=ISRT+22
1890      DECODE(INDAT1,6710) (HEADR(J),J=1,3),
1900      * (IDATAI(J),IDATA0(J),J=ISRT,ISRTE)
1910      6710 FORMAT(3A6,2X,23(5X,2(5,5X))

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1920      ISRTT=ISRTE+1
1930      ISRTE=ISRTE+24
1940      DECODE(INDAT2,6720) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE)
1950 6720  FORMAT(24(5X,215,5X))
1960      ISRTT=ISRTE+1
1970      ISRTE=ISRTE+24
1980      DECODE(INDAT3,6720) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE)
1990      ISRTT=ISRTE+1
2000      ISRTE=ISRTE+19
2010      DECODE(INDAT4,6730) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE),
2020      * IIA(IHD),(TRAILR(J),J=1,2),TRAILR(3),ITHETA(IHD)
2030 6730  FORMAT(19(5X,215,5X),3X,13,2A6,A5,17)
2040      GO TO 300
2050 290  CONTINUE
2060      IF (ISRT .EQ. 1 .AND. 19TST .EQ. 0) GO TO 79
2070      ISRTE=ISRT+22
2080      DECODE(INDAT1,6740) (IDATAI(J),IDATAQ(J),J=ISRT,ISRTE)
2090 5740  FORMAT(T21,23(5X,215,5X))
2100      ISRTT=ISRTE+1
2110      ISRTE=ISRTE+24
2120      DECODE(INDAT2,6720) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE)
2130      ISRTT=ISRTE+1
2140      ISRTE=ISRTE+24
2150      DECODE(INDAT3,6720) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE)
2160      ISRTT=ISRTE+1
2170      ISRTE=ISRTE+19
2180      DECODE(INDAT4,6720) (IDATAI(J),IDATAQ(J),J=ISRTT,ISRTE)
2190  C
2200 300  IF( ISTD .GE. NND5 ) GO TO 320
2210      ISRT = ISRT + 90
2220      IHD = 3
2230      GO TO 280
2240  C
2250  C
2260 70  CONTINUE
2270      NBR=FLD(21,15,IPEF)
2280      IF(NBR.GT.100) GOTO 72
2290 74  CONTINUE
2300      WRITE (6,5140) THDES(ITH), NBR
2310 5140  FORMAT ('0SHORT RECORD FOUND - ANGLE = ',F7.1,5X,'NBR =',16)
2320 76  CALL DATIN
2330      IF(IERN.EQ.0 OR IERN.EQ.10 OR IERN.EQ.13) GOTO 79
2340      CALL ERRPRC
2350      IF(IERN.EQ.1) GOTO 310
2360      IF(IERN.GE.20) GOTO 74
2370      GOTO 315
2380  C
2390 72  WRITE (6,5180)
2400 5180  FORMAT (' SHORT RECORD ASSUMED TO BE GAP NOISE ')
2410      IGN = IGN + 1
2420      IF (IGN .GE. 3) CALL EXIT
2430      IHD = 3
2440      GO TO 280
2450  C
2460 79  CONTINUE
2470      DECODE(INDAT1,6012) 191,192
2480 6012  FORMAT(T21,15,T241,15)
2490      IF ( 191 .LT. 0 .AND. 192 .LT. 0 ) GO TO 80
2500      IF (19TST .EQ. 1) GO TO 76
2510      WRITE (6,9004)
2520 9004  FORMAT ('XXXXXXXXXXXXX FIRST RECORD OF FILE BAD XXXXXXXXXXXX'//)
2530      GO TO 76
2540 80  ISRT = 1
2550      ISTD = 90
2560      IHD = 3
2570      19TST = 1

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2580      IGN = 0
2590      GO TO 52
2600 C
2610 C
2620      310 WRITE (6,7002) IFILE
2630      7002 FORMAT( / ' DFILE ASSUMED AT END OF FILE(' , I2, ') ... REPLACE DATA ST
2640      ARTING WITH RESTART ANGLE' )
2650      IF ( ( THFIN - THDES(ITH) ) .LE. THINC ) GO TO 96
2660      IOFT = 2
2670      IFILE = IFILE + 1
2680      IPTST = 0
2690      GO TO 278
2700      96 WRITE ( 6,5340 ) IFILE
2710      5340 FORMAT( ' FILE', I5, ' IS ASSUMED COMPLETE' )
2720      IOFASM = 2
2730      GO TO 400
2740 C
2750 C
2760      315 CONTINUE
2770      WRITE (6,7003) IFILE, THETA
2780      7003 FORMAT( ' ERROR ATTEMPTING TO READ FILE(' , I2, ') , ASPECT=' , F8.1 )
2790      IOER = IOER + 1
2800      IF (IOER .GE. 10) CALL EXIT
2810      GO TO 76
2820 C
2830 C
2840      320 IGN = 0
2850      ABSITH = ITHETA(1) - ITHETA(2)
2860      IF ( ABS(ABSITH) .GT. THTEST ) GO TO 120
2870      119 THETA = ITHETA(1)/10.
2880      GO TO 130
2890      120 IF( ITH .EQ. 1 ) GO TO 119
2900      T1 = ITHETA(1)/10.
2910      T2 = ITHETA(2)/10.
2920      D1 = ABS( THETA - T1 )
2930      D2 = ABS( THETA - T2 )
2940      IF( D1 .LT. D2 ) GO TO 125
2950      THETA = T2
2960      GO TO 130
2970      125 THETA = T1
2980      130 CONTINUE
2990      IF ( THETA .LT. 300. .AND. ITHFG .EQ. 1 ) THETA = THETA + 360.0
3000 C
3010      ISPTST = ISPTST + 1
3020      IF ( ISPTST .NE. 2 ) GO TO 319
3030      IF( SYSATT(1) .EQ. IIA(1)/10. .OR. SYSATT(1) .EQ. IIA(2)/10. ) GO TO 319
3040      WRITE (6,6015) SYSATT(1), IFILE
3050      6015 FORMAT ( ' ***** ATTENUATION LEVEL OF TAPE WAS NOT EQUAL TO', F8.2,
3060      1/ ' FILE NO. =', I5 )
3070      CALL EXIT
3080      319 CONTINUE
3090      317 CONTINUE
3100      GO TO (324,321), IOFT
3110      321 IOFT = 1
3120      IF( SYSATT(1) .EQ. IIA(1)/10. .OR. SYSATT(1) .EQ. IIA(2)/10. ) GO TO 900
3130      WRITE (6,6015) SYSATT(1), IFILE
3140      CALL EXIT
3150      900 CONTINUE
3160      TEST = THETA
3170      J = 0
3180      322 J = J + 1
3190      IF( ABS( THDES(J) - ABS(THETA) ) .GT. DTH ) GO TO 322
3200      NN = NN + J - ITH
3210 C
3220      328 CONTINUE
3230 C

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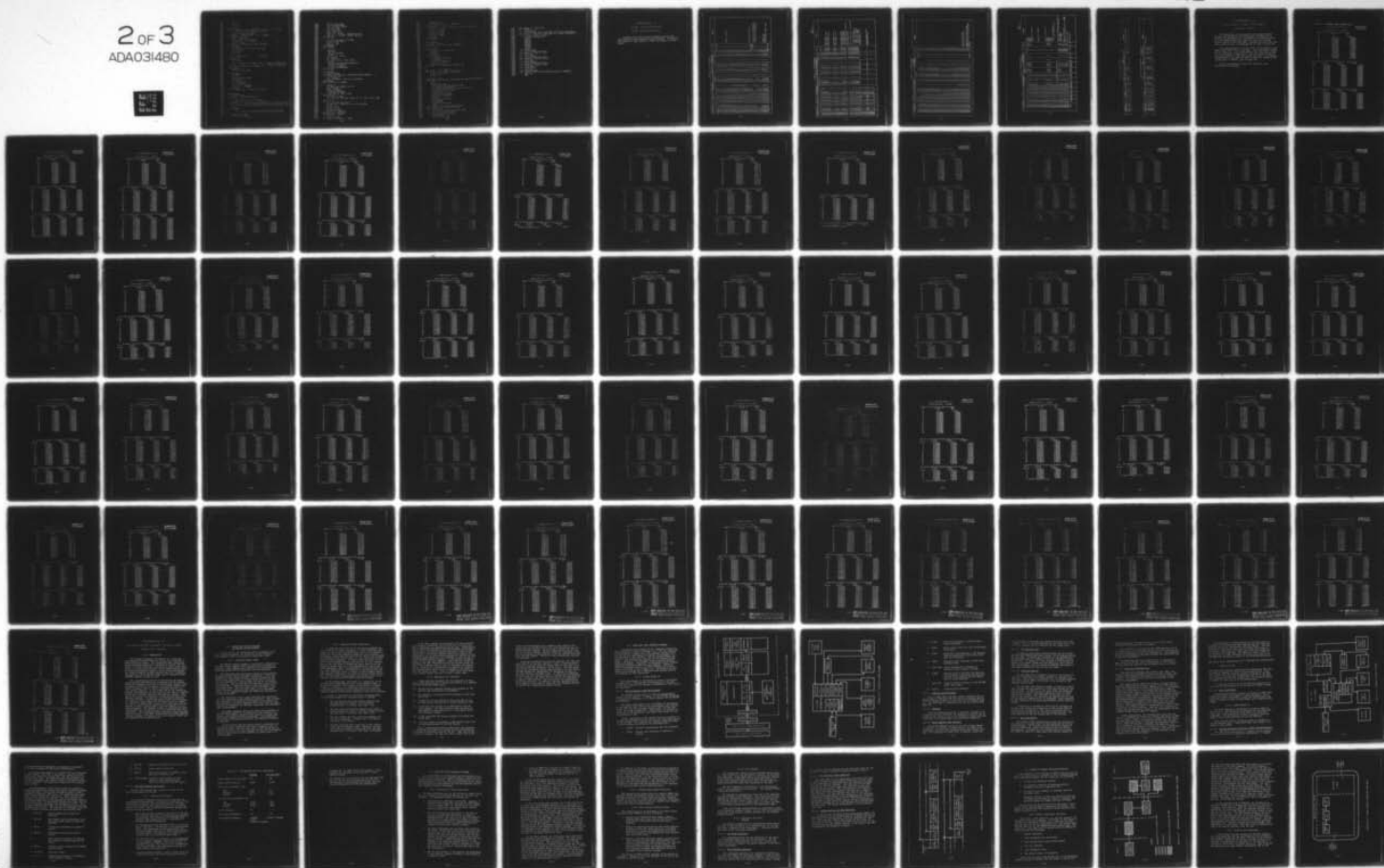
AD-A031 480

GENERAL DYNAMICS FORT WORTH TEX CONVAIR AEROSPACE DIV F/G 17/9  
ENDO ATMOSPHERIC-EXO ATMOSPHERIC RADAR MODELING. APPENDICES, A---ETC(U)  
JUN 76 R J HANCOCK, F H CLEVELAND F30602-73-C-0380

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RADC-TR-76-186-VOL-4-PT-1 NL

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3240 C
3250 ITH = J
3260 IK = J
3270 GO TO 340
3280 C
3290 324 CONTINUE
3300 320 IF( ABS(THDES(ITH) - ABS(THETA) ) LE DTH ) GO TO 340
3310 IF( THETA LT. THDES(ITH) ) GO TO 335
3320 IF( IPASS EQ. 1 ) GO TO 350
3330 WRITE (6,7010) THDES(ITH)
3340 7010 FORMAT( ' ASPECT ANGLE ',F6.1,' MISSING ' )
3350 IMISS = IMISS + 1
3360 JMISS = JMISS + 1
3370 THMISS(JMISS) = THDES(ITH)
3380 IF( IMISS LT. 5 ) GO TO 331
3390 WRITE (6,7011)
3400 7011 FORMAT( ' TOO MANY ASPECT ANGLES MISSING ' )
3410 CALL EXIT
3420 331 CONTINUE
3430 IF( THDES(ITH) GE. THFIN ) GO TO 400
3440 ITH = ITH + 1
3450 IK = IK + 1
3460 GO TO 330
3470 C
3480 335 IF( IPASS EQ. 2 ) GO TO 278
3490 GO TO 350
3500 340 IPASS = 2
3510 NN = NN + 1
3520 C
3530 WRITE (6,7020) NN, ITH, (HEADR(J), J=1, 3), IIR(1), (TRAILR(J), J=1, 2),
3540 1 TRAILR(3), ITHETA(1)
3550 7020 FORMAT( ' OSWEEP(',I3,',', THDES(',I3,', ' ,3A6.3X,I3,2A6,A5.17 )
3560 150 CONTINUE
3570 IMISS = 0
3580 GO TO (278,355), IPASS
3590 C
3600 355 CONTINUE
3610 IK = IK + 1
3620 JF = 0
3630 DO 356 J=1, NPTS, INCX
3640 JF = JF + 1
3650 JJ = IRO + J - 1
3660 XI = IDATAI(JJ)
3670 X0 = IDATHO(JJ)
3680 XFI( IK, JF ) = XI/10000.
3690 XFO( IK, JF ) = X0/10000.
3700 356 CONTINUE
3710 IF( THDES(ITH) LT. THFIN ) GO TO 275
3720 C
3730 C
3740 400 CONTINUE
3750 WRITE (6,3000)
3760 1000 FORMAT( ' FILE PROCESS END ' )
3770 C
3780 IF( JMISS EQ. 0 ) GO TO 464
3790 WRITE(6,7600) (THMISS(J), J=1, JMISS)
3800 7600 FORMAT( '///' //*****// *****
3810 1*****//THE FOLLOWING ASPECT ANGLES WERE MISSING'//, (F10.1
3820 2,///' //*****// *****
3830 3*****//)
3840 464 CONTINUE
3850 C
3860 C ***** APPLY CORRECTION FACTOR AND WEIGHTING FUNCTION
3870 C
3880 DO 459 J=1, NPTSF
3890 CRA = AKR+J -ACTGT

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3900      DO 554 IK= 1, NTH
3910      TH = (IK-NT02)*THINC
3920      XCTH = CRA*COSE( TH*DTR )
3930      XI = COSE( XCTH)
3940      XQ =-SIN( XCTH)
3950      XFIX = XFI( IK,J)
3960      XFQX = XFQ( IK,J)
3970      XRI( IK) = ( XFIX*XI - XFQX*XQ )*N( IK)
3980      XRQ( IK) = ( XFIX*XQ + XFQX*XI )*N( IK)
3990      554 CONTINUE
4000      C
4010      IF ( NTH .GE. NTH1 ) GO TO 556
4020      DO 555 IK=NTH1,NTHN
4030      XRI( IK) = 0.0
4040      XRQ( IK) = 0.0
4050      555 CONTINUE
4060      556 CONTINUE
4070      C
4080      DELI=1.0
4090      DELQ=1.0
4100      CALL IFT(XRI,XRQ)
4110      IK=NTHN
4120      DO 493 IIK = 1,NTHN
4130      XI = XRI( IK)
4140      XQ = XRQ( IK)
4150      XA = SQRT( XI*XI + XQ*XQ )/XNTH
4160      IK=IK-1
4170      IADD=IFIX(40.0+20.0*ALOG10(XA)+0.5)
4180      IF(IADD.GT.43)IADD=44
4190      IF(IADD.LT.5)IADD=4
4200      XFII(IIK,J)=CTABL(IADD)
4210      493 CONTINUE
4220      C
4230      459 CONTINUE
4240      WRITE (6,7510)
4250      7510 FORMAT(1H1,'AMPLITUDE (TRANSFORM IN THETA DOMAIN) ' )
4260      DO 460 J=1,NPTSF
4270      RJ = J*DRANG
4280      WRITE (6,7520)RJ, (XFII( IK, J), IK=1,NTHN)
4290      460 CONTINUE
4300      7520 FORMAT(1H ,F8.5,100R1)
4310      C
4320      JMISS = 0
4330      IF( NWND0 EQ. NWND05 ) GO TO 5
4340      NWND0 = NWND0 + 1
4350      READ (5,CARD8)
4360      SYSATT(1)=SYSATQ
4370      TSWND0(NWND0)=TSWNDQ
4380      GO TO (599, 31, 410) , IFSEP
4390      599 CONTINUE
4400      TEST = TSWND0(NWND0)
4410      IF ( TEST .LE. 300. .AND. ITHFG .EQ. 1 ) TEST = TEST + 360
4420      J = 0
4430      600 J = J + 1
4440      IF ( J .GT. NTH) GO TO 606
4450      IF( ABS( TEST - THDES( J) ) .GT. 0.1 ) GO TO 600
4460      IK = 0
4470      DO 602 L=J,NTH
4480      IK = IK + 1
4490      DO 601 LL=1,NPTSF
4500      XFQ( IK, LL) = XFQ( L, LL)
4510      601 XFI( IK, LL) = XFI( L, LL)
4520      602 THDES( IK) = THDES( L)
4530      LL = IK + 1
4540      DO 603 L=LL,NTH
4550      603 THDES( L) = THDES( L-1) + THINC

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4560      ITHFG = 0
4570      DO 604 L= 1,NTH
4580      IF ( THDES(L) .GE. 360. ) ITHFG = 1
4590      604 CONTINUE
4600      WRITE (6,7610) NWNDO, SYSRTT(1), THDES(1), THDES(NTH)
4610      ITH = 1K
4620      THFIN = THDES(NTH)
4630      DO 605 J= 1, NPTSF
4640      DO 605 JJ= LL,NTH
4650      XE0 (JJ,J) = 0.0
4660      XF1 (JJ,J) = 0.0
4670      605 CONTINUE
4680      GO TO 275
4690      C
4700      606 CONTINUE
4710      WRITE (6,7006)
4720      7006 FORMAT ( ' NO MATCH FOUND FOR ANGLE ' )
4730      CALL EXIT
4740      C
4750      410 CONTINUE
4760      IF (IOFASM .EQ. 1) GO TO 415
4770      IOFASM = 1
4780      GO TO 411
4790      415 CONTINUE
4800      CALL DATIN
4810      IF (IERW .EQ. 0) GOTO 410
4820      CALL ERRPRC
4830      IF (IERW .EQ. 1) GOTO 411
4840      WRITE(6,7031)IFILE
4850      GOTO 410
4860      7031 FORMAT ( ' READING TO EOF IN FILE ',15)
4870      C
4880      C
4890      411 WRITE (6,7004) IFILE
4900      7004 FORMAT( ' COMPLETED FILE(',12,') ' )
4910      IF ( IFILE .EQ. NFILES ) GO TO 610
4920      IFILE = IFILE + 1
4930      GO TO 31
4940      C
4950      610 WRITE (6,7620)
4960      7620 FORMAT( ' FILE FOR NEXT WINDOW DOES NOT EXIST ON THIS TAPE ' )
4970      GO TO 5
4980      END
4990      SUBROUTINE ERRPRC
5000      COMMON INDAT(309), IPEF, STATN(2), IERN
5010      DATA 18LBL/00000000002020/
5020      DATA IREAD, IERR1, IERR2, IERR3, IERR4/0, 0, 0, 0, 0/
5030      DATA IERR5, IERR6/0, 0/, IN/6/
5040      IREAD=IREAD+1
5050      IF (IERW .EQ. 0) GOTO 800
5060      ISTAT=FLO(0,12, STATN(1))
5070      IREC=FLO(0,18, INDAT(3))
5080      IERR=IERW
5090      IF (IERR .LT. 10) GOTO 30
5100      IERR=IERR-10
5110      IERR1=IERR1+1
5120      IF (IERR .LT. 10) GOTO 20
5130      IERR=5
5140      20 WRITE(IN,1001) IERN, IPEF, IREC, ISTAT
5150      1001 FORMAT(1H, ,12,1X,06,1X,R3,1X,04)
5160      10 IERR=IERR+1
5170      GOTO(800,550,600,650,700,750,850), IERR
5180      900 ITEST=FLO(12,12, INDAT(304))
5190      IF (ITEST .EQ. 18LBL) RETURN
5200      IERR6=IERR6+1
5210      WRITE(IN,1003) ITEST

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5220      1003 FORMAT(1H , ' ITEST=', 04)
5230      RETURN
5240      550      IREAD=IREAD-1
5250      WRITE(IW,1008) IREAD, IERR1, IERR2, IERR3, IERR4, IERR5, IERR6
5260      1008 FORMAT(1H , 'END OF FILE DETECTED', 14, ' RECORDS PROCESSED BY ',
5270      * ' ERRPRC   ERR=', 6(13,1X))
5280      IF(IERR.EQ.7) CALL EXIT
5290      IREAD=0
5300      IERR1=0
5310      IERR2=0
5320      IERR3=0
5330      IERR4=0
5340      IERR5=0
5350      IERR6=0
5360      RETURN
5370      600      IERR2=IERR2+1
5380      WRITE(IW,1004) IREC, ISTAT
5390      1004 FORMAT(1H , 'LONPCK-', R3, 04)
5400      GO TO 800
5410      650      IERR3=IERR3+1
5420      WRITE(IW,1005) IREC, ISTAT
5430      1005 FORMAT(1H , 'LATPCK-', R3, 04)
5440      GO TO 800
5450      700      IERR4=IERR4+1
5460      WRITE(IW,1006) IREC, ISTAT
5470      1006 FORMAT(1H , 'UNKERR-', R3, 04)
5480      GO TO 800
5490      750      IERR5=IERR5+1
5500      GOTO 800
5510      850      WRITE(IW,1015)
5520      1015 FORMAT(' BLANK TAPE ON READ=THIS JOB WILL TERMINATE')
5530      GOTO 550
5540      END

```

A P P E N D I X   I  
T S A R   S I M U L A T I O N  
R U N   C A T A L O G U E S

Listings of all the computer program runs for the TSAR Simulation are provided in this Appendix. A detailed explanation of these tables is found in Volume 3 of this series.

TABLE I-1 - TSARJB RUN CATALOG

IDENTIFIERS SNMB	DATE	SYSTEM		CONTROL GEN.		THETAS THETAR	NBPSR	ARRAY AND SIGNAL PROCESSING				FNL	DX	COMMENTS
		N2	FS	SINBW	THETAS	NBPSCG		ASTRT	ASTOP	MODTSR	REC PROCS			
6669T	11-20	14	1.0	0.1	0.955	3	4	-5.0	10.0	1	NO	NO	0.299793	NPULS = 3 in CGEN
2790T	11-27	14	1.0	0.1	0.955	3	4	-5.0	30.0	1	NO	NO		
2837T	11-27	14	1.0	0.1	10.0	3	4	-5.0	30.0	1	NO	NO		
3901T	11-27	14	1.0	0.1	20.0	3	4	5.0	40.0	1	NO	NO		
1848T	11-29	14	1.0	0.1	0.955	3	4	-5.0	30.0	1	NO	NO		
7771T	11-30	14	1.0	0.1	0.955	3	4	-5.0	30.0	1	NO	NO		
8601T	11-30	14	1.0	0.1	20.0	3	4	5.0	40.0	1	NO	NO		
2017T	12-03	14	1.0	0.1	40.0	3	4	25.0	40.0	1	NO	NO		
8878T	12-04	14	1.0	0.1	0.955	3	4	-5.0	30.0	1	NO	NO		
1794T	12-13	14	1.0	0.1	0.955	3	4	-5.0	5.0	1	NO	NO		
2872T	12-13	14	1.0	0.1	0.955	3	4	-5.0	5.0	2	YES	YES		Cassette Data Unplotted
3566T	12-13	14	1.0	0.1	0.955	3	4	-5.0	10.0	3	YES	YES		
2827T	1-07	14	1.0	0.1	0.955	10	4	-5.0	10.0	7	NO	NO		
4099T	1-07	14	1.0	0.1	0.955	10	4	-5.0	10.0	1	NO	NO		
7809T	1-08	14	1.0	0.1	0.955	10	4	-5.0	10.0	7	NO	NO		
3667T	1-09	14	1.0	0.1	0.955	10	4	-5.0	10.0	7	NO	NO		
8371T	1-10	14	1.0	0.1	0.950	10	4	0.0	2.0	7	NO	NO		
8812T	1-10	14	1.0	0.1	13.70	10	4	5.0	25.0	2	YES	YES		
8967T	1-10	14	1.0	0.1	13.70	10	4	5.0	25.0	2	YES	YES		
2252T	1-11	14	1.0	0.1	13.70	10	4	5.0	25.0	2	YES	YES		
3901T	1-11	14	1.0	0.1	7.18	10	4	0.0	35.0	2	YES	YES		Contains Scan of CGEN Spectrum Contains Scan of CGEN Spectrum Contains Scan of CGEN Spectrum
8414T	1-14	14	1.0	0.1	7.18	10	4	0.0	35.0	1	NO	NO		
3594T	1-15	14	1.0	0.1	0.950	10	4	0.0	35.0	2	YES	YES		
6700T	1-16	14	1.0	0.1	0.950	10	4	0.0	35.0	1	NO	NO		
7688T	1-16	14	0.5	0.1	0.950	10	4	0.0	15.0	1	NO	NO		
2728T	1-17	14	0.5	0.1	0.950	3	4	0.0	15.0	1	NO	NO		
3805T	1-17	14	1.0	0.1	0.950	3	4	-5.0	35.0	1	NO	NO		
7487T	1-18	14	0.5	0.06	0.950	3	4	-5.0	20.0	1	NO	NO		
2749T	1-21	14	0.5	0.06	0.950	3	4	-5.0	25.0	1	NO	NO	0.299793	
8602T	1-22	14	1.0	0.10	2.0	10	4	-5.0	35.0	1	NO	NO	0.344590	
8902T	1-22	14	1.0	0.10	3.0	10	4	-5.0	35.0	1	NO	NO	0.299793	Contains Scan of CGEN Spectrum Contains Scan of CGEN Spectrum Contains Scan of CGEN Spectrum
8902T	1-22	14	1.0	0.10	4.0	10	4	-5.0	35.0	1	NO	NO		
3751T	1-21	14	1.0	0.10	-61.04	10	4	-70.0	-30.0	1	NO	NO		
4171T	1-21	14	1.0	0.10	2.00	3	4	-5.0	35.0	1	NO	YES		
4171T	1-21	14	1.0	0.10	3.00	3	4	-5.0	35.0	1	NO	YES		
4171T	1-21	14	1.0	0.10	4.00	3	4	-5.0	35.0	1	NO	YES		
4171T	1-23	14	1.0	0.10	5.00	3	4	-5.0	35.0	1	NO	YES		
2141T	2-05	14	0.5	0.10	13.70	10	4	12.0	15.0	7	NO	NO		
8246T	2-06	14	0.5	0.10	13.70	10	4	12.0	15.0	7	NO	NO		
3765T	2-19	14	0.5	0.10	0.950	3	4	-5.0	15.0	3	YES	YES		
7542T	3-06	14	0.5	0.10	0.950	10	4	-5.0	20.0	1	NO	YES		.NCGPLS = 140 .NCGPLS = 240 Data Punched by SNMB = 2689T
7596T	5-06	14	1.0	0.10	0.950	3	4	-5.0	35.0	2	YES	YES	0.299793	



TABLE I-1 - TCAPID RUN CATALOG

IDENTIFIERS		SYSTEM		CONTROL GEN.		ARRAY AND SIGNAL PROCESSING				COMMENTS			
SNMUB	DATE	NZ	FS	STMR	THETAS	THETAS	NBPSR	ASTRT	ASTOP	MODTISR	REC	FXNL	DX
7610T	5-06	14	1.0	0.10	0.950	0.950	4	-5.0	35.0	2	YES	NO	0.299793
2646T	5-07	14	1.0	0.10	0.950	0.950	4	-5.0	35.0	1	NO	YES	↓
2661T	5-07	14	1.0	0.10	0.950	0.950	4	-5.0	35.0	2	NO	YES	
3590T	5-07	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	YES	YES	
7468T	5-08	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	YES	YES	0.299793
8522T	5-08	14	1.0	0.10	0.950	0.950	4	-5.0	35.0	1	NO	YES	2.398342
8712T	5-08	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	YES	NO	0.299793
3575T	5-09	14	1.0	0.10	1.0	1.0	4	-5.0	35.0	1	NO	YES	2.398342
3575T	↓	↓	↓	↓	2.0	2.0	4	↓	↓	1	NO	YES	↓
3575T	↓	↓	↓	↓	3.0	3.0	4	↓	↓	1	NO	YES	↓
3575T	↓	↓	↓	↓	4.0	4.0	4	↓	↓	1	NO	YES	↓
3575T	5-09	14	1.0	0.10	5.0	5.0	4	-5.0	35.0	1	NO	YES	2.398342
8415T	5-14	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	1	NO	YES	0.299793
4288T	5-09	14	1.0	0.10	1.0	1.0	4	-5.0	40.0	3	NO	YES	2.398342
4288T	↓	↓	↓	↓	2.0	2.0	4	↓	↓	3	NO	YES	↓
4288T	↓	↓	↓	↓	3.0	3.0	4	↓	↓	3	NO	YES	↓
4288T	↓	↓	↓	↓	4.0	4.0	4	↓	↓	3	NO	YES	↓
4288T	5-09	14	1.0	0.10	5.0	5.0	4	-5.0	40.0	3	NO	YES	2.398342
2726T	5-09	14	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	NO	YES	2.398342
7478T	5-16	14	1.0	0.10	0.950	0.950	10	-5.0	35.0	1	NO	YES	2.398342
7478T	5-16	14	1.0	0.10	0.950	0.950	10	-5.0	35.0	3	NO	YES	2.398342
2698T	5-17	15	1.0	0.10	13.70	13.70	4	10.0	17.5	6	NO	YES	0.299793
3404T	5-29	15	1.0	0.10	0.950	0.950	--	-5.0	35.0	3	YES	YES	2.398342
3732T	5-29	15	1.0	0.10	1.00	1.00	4	-5.0	35.0	3	YES	YES	0.299793
3732T	5-29	15	1.0	0.10	2.00	2.00	4	-5.0	35.0	3	YES	YES	0.299793
7546T	5-30	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	YES	YES	0.299793
7462T	06-17	15	1.0	0.10	2.0	2.00	4	-5.0	35.0	3	YES	YES	0.299793
8462T	06-17	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	NO	YES	2.398342
8462T	06-17	14	1.0	0.10	2.00	2.00	4	-5.0	35.0	3	NO	YES	2.398342
8430T	06-19	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	NO	YES	0.299793
8430T	06-19	15	1.0	0.10	0.950	0.950	4	-5.0	35.0	3	NO	YES	0.299793
8430T	07-22	14	2.0	0.080	10.0	10.0	4	-5.0	35.0	3	NO	YES	0.299793
2730T	↓	↓	↓	↓	20.0	20.0	↓	---NOT APPLICABLE---					---
2730T	↓	↓	↓	↓	30.0	30.0	↓						
2730T	↓	↓	↓	↓	40.0	40.0	↓						
2730T	↓	↓	↓	↓	60.0	60.0	↓						
2730T	↓	↓	↓	↓	80.0	80.0	↓						
2730T	07-22	14	2.0	0.080	10.0	10.0	10	---NOT APPLICABLE---					---
3389T	07-22	15	1.0	0.100	10.0	10.0	10						
3389T	↓	↓	↓	↓	20.0	20.0	↓						
3389T	↓	↓	↓	↓	30.0	30.0	↓						
3389T	↓	↓	↓	↓	40.0	40.0	↓						
3389T	↓	↓	↓	↓	60.0	60.0	↓						
3389T	07-22	15	1.0	0.100	80.0	80.0	10						

NCPLS = 300  
TSAR SUBARRAY PATTERN  
NCPLS = 300  
TSAR SUBARRAY PATTERN  
  
TSAR SUBARRAY PATTERN  
NCPLS = 300  
TSAR SUBARRAY PATTERN  
  
TSAR SUBARRAY PATTERN  
TSAR SUBARRAY PATTERN  
TSAR SUBARRAY PATTERN  
TSAR SUBARRAY PATTERN  
Punched by 7437T 05/17/74 same Job  
Run as 7474T 05/28/74  
TSAR SUBARRAY PATTERN  
  
Bad Data (Receiver Proc. Set for 1.0°)  
  
Rerun of 3732T Pass 2  
NCPLS = 300 Punched by  
NCPLS = 140 2682T  
NCPLS = 300 Punched by  
NCPLS = 300 2666T  
Control Generator Output  
Spectrum Scan Only  
  
Control Generator Output  
Spectrum Scan Only

TABLE I-2 - TSARTM RUN CATALOG

IDENTIFIERS SNLMB	DATE	SYSTEM		CONTROL		GENERATOR		THETAS THETAR	ANGLE	ANTENNA ARRAY		DX	FNL	COMMENTS
		N2	FS	SIMBW	THETAS	NBPSOG	NCCPLS			NBPSR	MODTSR			
6678T	12-14	12	0.5		0.955	3	62	0.955	0.955	4		0.299793	NO	
3109T	12-17	12	0.5		0.955	3	62	0.955	0.955	4			NO	
7456T	12-18	12	0.5	0.1	0.955	3	62	0.955	0.955	4			NO	
8611T	12-18	12	0.5	0.1	0.955	3	62	0.955	0.955	4			NO	
1935T	12-19	12	0.5	0.1	0.955	3	62	0.955	0.955	4			NO	
3665T	12-19	13	0.5	0.1	0.955	3	62	0.955	0.955	4			NO	
6707T	12-20	13	0.5	0.1	0.955	3	62	0.955	7.65	4			NO	
8697T	12-20	13	0.5	0.2	0.955	3	62	0.955	0.955	4			NO	
1836T	1-07	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
3930T	1-07	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
6693T	1-08	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8676T	1-08	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8762T	1-08	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8843T	1-08	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8946T	1-08	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
3652T	1-09	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
7768T	1-10	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8483T	1-10	13	0.5	0.2	0.955	3	62	0.955	0.955	4	1		NO	
8863T	1-10	13	0.5	0.2	13.7	3	62	13.7	13.7	4	1		NO	
3726T	1-11	13	0.5	0.2	7.18	3	62	7.18	7.18	4	1		NO	
6713T	1-16	13	0.5	0.2	0.95	3	62	0.95	0.95	4	1		NO	
8388T	1-18	13	0.5	0.06	0.95	3	62	0.95	0.95	4	1		NO	
3845T	1-21	13	0.5	0.06	0.95	3	62	0.95	0.95	4	1		YES	
8376T	1-22	13	0.5	0.10	2.0	10	62	2.0	2.0	10	1		YES	
8700T	1-24	13	0.5	0.10	0.950	3	62	0.95	0.95	4	1		YES	
8700T	1-24	13	0.5	0.10	-61.0	3	62	0.95	-61.0	4	1		YES	
2713T	1-25	13	0.5	0.10	7.18	3	62	7.18	7.18	4	1		YES	
2713T	1-25	13	0.5	0.10	-61.0	3	62	-61.0	-61.0	4	1		YES	
8004T	2-06	13	0.5	0.10	7.18	3	62	7.18	7.18	4	1		YES	
3133T	2-07	13	0.5	0.10	0.950	3	62	0.950	7.70	4	1		YES	
3133T	2-07	13	0.5	0.10	0.400	3	62	0.400	0.400	4	1		YES	
3133T	2-07	13	0.5	0.10	0.440	3	62	0.440	0.440	4	1		YES	
7691T	2-08	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7		NO	
7457T	2-12	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7		NO	
8712T	2-12	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7		NO	
6704T	2-14	13	0.5	0.10	13.70	10	62	13.70	13.80	4	7		NO	
6704T	2-14	13	0.5	0.10	13.70	10	62	13.70	13.60	4	7		NO	
2644T	2-19	13	0.5	0.10	13.70	10	62	13.70	13.80	4	7		NO	
2644T	2-19	13	0.5	0.10	13.70	10	62	13.70	13.60	4	7		NO	
2665T	2-19	13	0.5	0.10	0.44	3	62	0.44	0.44	4	1		YES	(Rerun of plots 9 & 10 of 3133T)
1844T	3-05	13	0.5	0.10	13.70	10	62	13.70	13.80	4	7		YES	MONOTM (Error in Correcting TSARY)
1844T	3-05	13	0.5	0.10	13.70	10	62	13.70	13.60	4	7		YES	[NOTE 1] (Error in Correcting TSARY)
1871T	3-05	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7	0.299793	YES	MONOTM (Error in Second Pass) MONOTM (Rerun of 6704T)

TABLE I-2 -TSARTM RUN CATALOG

IDENTIFIERS		SYSTEM		CONTROL GENERATOR		ANTENNA ARRAY				COMMENTS				
SNMB	DATE	N2	FS	SIMBW	THETAS	NBPSGC	NCCPLS	THETAS THETAR	ANGLE	NBPSR	MODTSR	DX	PNL	
7502T	3-06	13	0.5	0.10	13.70	10	62	13.70	13.80	4	7	0.299793	YES	MONOTM
7502T	3-06	13	0.5	0.10	13.70	10	62	13.70	13.60	4	7		YES	MONOTM
1825T	3-07	13	0.5	0.10	13.70	10	62	13.70	13.80	4	7		NO	MONOTM
1825T	3-07	13	0.5	0.10	13.70	10	62	13.70	13.60	4	7		NO	MONOTM
2723T	3-07	13	0.5	0.10	0.950	3	62							CJOB2 Control Generator Spectra
2723T	3-07	13	0.5	0.10	0.40	3	62							
2723T	3-07	13	0.5	0.10	0.44	3	62							
2723T	3-07	13	0.5	0.10	0.950	10	62							
2723T	3-07	13	0.5	0.10	0.40	10	62							
4156T	3-07	13	0.5	0.10	2.0	3	62							CJOB2 Control Generator Spectra
4156T	3-07	13	0.5	0.10	3.0	3	62							
4156T	3-07	13	0.5	0.10	4.0	3	62							
4156T	3-07	13	0.5	0.10	5.0	3	62							
4156T	3-07	13	0.5	0.10	6.0	3	62							
4156T	3-07	13	0.5	0.10	0.44	10	62	13.70	13.90	4	7		YES	Retun as 7550T 03/19/74
7477T	3-08	13	0.5	0.10	13.70	10	62	13.70	13.50	4	7		YES	MONOTM
7477T	3-08	13	0.5	0.10	13.70	10	62	13.70	13.75	4	7		YES	MONOTM
6643T	3-11	13	0.5	0.10	13.70	10	62	13.70	13.65	4	7		YES	MONOTM
6643T	3-11	13	0.5	0.10	13.70	10	62	13.70						MONOTM
8457T	3-06	13	0.5	0.10	0.950	3	62							CJOB2
8457T	3-06	13	0.5	0.10	0.40	3	62							Retun of CGGN output of 3133T with new phase detector
8457T	3-06	13	0.5	0.10	0.44	3	62							
8457T	3-06	13	0.5	0.10	0.44	3	62							
8933T	4-02	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7		NO	Retun of 8712 with Proper Time Reference Same as 1871; but Plotted More Data
8386T	5-02	13	0.5	0.10	13.70	10	62	13.70	13.70	4	7	0.299793	YES	TSAR SUBARRAY
8404T	5-02	13	0.5	0.10	0.950	3	62	0.950	7.70	4	1	2.39834	YES	TSAR SUBARRAY
3887T	05-09	13	0.5	0.10	0.950	10	62	-	31.15	-	1	2.39834	NO	TSAR SUBARRAY
7583T	07-15	13	0.5	0.10	0.950	10	8	-	31.15	-	1	2.39834	NO	
7583T	07-15	13	0.5	0.10	0.950	10	8	-	31.15	-	1	2.39834	NO	Retun of 7583T with different plot param. } punched by 7684T
3604T	07-16	13	0.5	0.10	0.950	10	8	-	31.15	-	1	2.39834	NO	
3604T	07-16	13	0.5	0.10	0.950	10	8	-	15.50	-	1	2.39834	NO	
2808T	07-16	13	0.5	0.10	0.950	10	62	-	15.50	-	1	2.39834	NO	
2808T	07-16	13	0.5	0.10	0.950	10	8	-	15.50	-	1	2.39834	NO	Punched by 7638T

NOTE 1: In runs made prior to this point - the array impulse response was referenced to the First Radiating Element.  
Subsequent runs are referenced to the center of the antenna array.

NOTE 1: In runs made prior to this point - the array impulse response was referenced to the First Radiating Element. Subsequent runs are referenced to the center of the antenna array.



TABLE I-3 - FSANTM RUN CATALOG

IDENTIFIERS		SYSTEM				COENCM				ARRAY			COMMENTS
SNUMB	DATE	N2	FS	SIMBW	RFPO	THETAS	SPW	NSUBP	THETAS	MBPSR	MODTSR	FNL	
8812T	01-14	13	0.5	0.2	0.5	0.955	3000.	1	0.950	4	1	NO	Error in Input Data, Run Aborted
1888T	01-15	13	0.5	0.2	0.5	0.955	3000.	1	0.950	4	1	NO	

Error in Input Data, Run Aborted

TABLE I-4 - FSANT RUN CATALOG

IDENTIFIERS SNUMB	DATE	N2	SYSTEM			COENCM			ARRAY			COMPUTATION LIMITS		COMMENTS
			FS	SIMBW	RFPO	THETAS	SPW	NSUBP	THETAS	MBPSR	FNL	ASTRT	ASTOP	
7608T	01-14	14	1.0	0.1	0.5	0.950	4620.	1	0.950	4	NO	-5.0	15.0	Job Aborted
8765T	01-14	14	1.0	0.1	0.5	0.950	4620.	1	0.950	4	NO	-5.0	15.0	
8516T	01-16	14	1.0	0.1	0.5	10.0	4620.	1	10.0	4	NO	0.0	30.0	
3667T	01-23	14	1.0	0.1	0.5	0.0	4620.	1	14.5	10	NO	-5.0	35.0	
8486T	01-24	14	1.0	0.05	0.5	3.5	4620.	1	18.15	4	NO	-5.0	50.0	

A P P E N D I X   J  
A N T E N N A   L O B E   S C A N N E R  
O U T P U T   D A T A

The output data of the Antenna Lobe Scanner computer program TSAR Simulation runs catalogued in Appendix I is provided in this appendix. The relative gain and direction of the antenna pattern side lobes are given for various absolute gains of the main lobe. Listings are given for side lobes, both in order of magnitude and in order of position.

Each page represents one run, which is identified in the upper right hand corner of the page. The snub number (SNUMB) and the data (e.g. 1-22) correspond to the first two columns of the catalogues in Appendix I. The pass number refers to the entry number for that snub number and date. For example, "SNUMB=8902T, 1-22, Pass #2" shown on page J-3 refers to the second entry of "8902T, 1-22" on page I-2.

Plots illustrated in Volume III use these same identification markings.

Table J-1 ANTENNA LOBE SCANNER OUTPUT

\* \* \* \* ANTENNA LOBE SCANNER \* \* \* \*

SNUMB=8902T

1-22, Pass#1

THE MAIN LOBE GAIN IS 47.8218226

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
 RANK REL. GAIN ANGLE  
 ( DB ) ( DEG )

MAIN	0.0	2.0000000
1	-13.0261264	1.3500000
2	-13.0291300	2.6500000
3	-17.6041594	0.9000000
4	-17.6058664	3.1000000
5	-20.6241126	3.5500000
6	-20.6423063	0.4500000
7	-22.9092073	-0.0000000
8	-22.9405689	4.0000000
9	-24.7926216	-0.4500000
10	-24.7931080	4.4500000
11	-26.3630013	4.9000000
12	-26.3916907	-0.9000000
13	-27.7626324	-1.3500000
14	-27.7920585	5.3500000
15	-28.9807363	-1.8000000
16	-29.0261512	5.8000000
17	-30.0771031	-2.2500000
18	-30.1311698	6.2499999
19	-31.1202965	6.6999999
20	-31.1836765	-2.7000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	2.4500000	
1	-13.0291300	2.6500000	0.6500000
2	-17.6058664	3.1000000	1.1000000
3	-20.6241126	3.5500000	1.5500000
4	-22.9405689	4.0000000	2.0000000
5	-24.7931080	4.4500000	2.4500000
6	-26.3630013	4.9000000	2.9000000
7	-27.7920585	5.3500000	3.3500000
8	-29.0261512	5.8000000	3.8000000
9	-30.1311698	6.2499999	4.2500000
10	-31.1202965	6.6999999	4.7000000
11	-32.0837040	7.1500000	5.1500000
12	-32.9214311	7.6000000	5.6000000
13	-33.7679574	8.0500000	6.0500000
14	-34.4775119	8.5000000	6.5000001
15	-35.0804257	8.9499999	6.9500000
16	-35.6195593	9.4000000	7.4000000
17	-36.1239052	9.9000000	7.9000000
18	-36.5594797	10.3499999	8.3499999
19	-36.9003377	10.8499999	8.8499999
20	-37.2910542	11.3000000	9.3000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.5500000	
1	-13.0261264	1.3500000	-0.6500000
2	-17.6041594	0.9000000	-1.1000000
3	-20.6423063	0.4500000	-1.5500000
4	-22.9092073	-0.0000000	-2.0000000
5	-24.7926216	-0.4500000	-2.4500000
6	-26.3916907	-0.9000000	-2.9000000
7	-27.7626324	-1.3500000	-3.3500000
8	-28.9807363	-1.8000000	-3.8000000
9	-30.0771031	-2.2500000	-4.2499999
10	-31.1836765	-2.7000000	-4.7000000
11	-32.0971685	-3.1500000	-5.1500000
12	-32.9307470	-3.6000000	-5.6000000
13	-33.6758013	-4.0500000	-6.0500000
14	-34.4081964	-4.5000000	-6.4999999
15	-35.0868244	-4.9500000	-6.9499999

NO FURTHER SIDE LOBES ON THIS SIDE



• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=8902T  
1-22, Pass#2

THE MAIN LOBE GAIN IS 47.8174233

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	3.0000000
1	-12.9490614	2.3500000
2	-12.9884882	3.6500000
3	-17.5583038	1.9000000
4	-17.6226730	4.1000000
5	-20.6065463	1.4500000
6	-20.6421523	4.5500000
7	-22.9054661	1.0000000
8	-22.9148593	4.9999999
9	-24.7624536	0.5500000
10	-24.7761493	5.4500000
11	-26.3087053	0.1000000
12	-26.3753686	5.9000000
13	-27.6935997	-0.3500000
14	-27.7253823	6.3500000
15	-28.9198308	-0.8000000
16	-28.9506540	6.8000000
17	-30.0383978	7.2499999
18	-30.1132083	-1.2500000
19	-31.0468960	7.6999999
20	-31.1525440	-1.7000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	3.4500000	
1	-12.9884882	3.6500000	0.6500000
2	-17.6226730	4.1000000	1.1000000
3	-20.6421523	4.5500000	1.5500000
4	-22.9148593	4.9999999	2.0000000
5	-24.7761693	5.4500000	2.4500000
6	-26.3753686	5.9000000	2.9000000
7	-27.7253823	6.3500000	3.3500000
8	-28.9506540	6.8000000	3.8000000
9	-30.0383978	7.2499999	4.2500000
10	-31.0468960	7.6999999	4.7000000
11	-32.0782876	8.1500000	5.1500000
12	-32.9089999	8.5999999	5.6000000
13	-33.7006454	9.0500000	6.0500000
14	-34.5619659	9.4499999	6.4500000
15	-34.4971533	9.5500000	6.5500000
16	-35.0923672	10.0000000	7.0000000
17	-35.6189204	10.4499999	7.4500000
18	-36.1427851	10.9000000	7.9000000
19	-36.5689917	11.4499999	8.4499999
20	-36.9418898	11.9000000	8.9000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	2.5500000	
1	-12.9490614	2.3500000	-0.6500000
2	-17.5583038	1.9000000	-1.1000000
3	-20.6065463	1.4500000	-1.5500000
4	-22.9054661	1.0000000	-2.0000000
5	-24.7424536	0.5500000	-2.4500000
6	-26.3087053	0.1000000	-2.9000000
7	-27.6935997	-0.3500000	-3.3500000
8	-28.9198308	-0.8000000	-3.8000000
9	-30.1132083	-1.2500000	-4.2500000
10	-31.1525440	-1.7000000	-4.7000000
11	-32.0609813	-2.1500000	-5.1500000
12	-32.9259062	-2.6000000	-5.6000000
13	-33.6953616	-3.0500000	-6.0500000
14	-34.4029884	-3.5000000	-6.4999999
15	-35.0466642	-3.9500000	-6.9500000
16	-35.7416568	-4.4000000	-7.3999999
17	-36.2872169	-4.9000000	-7.8999999

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=8902T  
1-22, Pass#3

THE MAIN LOBE GAIN IS 47.8195219

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	4.0000000
1	-12.9868002	3.3500000
2	-13.0212927	4.6500000
3	-17.5588055	2.9000000
4	-17.5960703	5.1000000
5	-20.5808043	2.4500000
6	-20.6431212	5.5500000
7	-22.8563833	2.0000000
8	-22.9253621	5.9999999
9	-24.7384033	1.5500000
10	-24.7682619	6.4499999
11	-26.2969308	1.1000000
12	-26.3245201	6.9000000
13	-27.7062082	7.3500000
14	-27.7198877	0.6500000
15	-28.9366488	7.8000000
16	-28.9457912	0.2000000
17	-30.0452714	-0.2500000
18	-30.0719309	8.2500000
19	-31.0531001	-0.7000000
20	-31.0940461	8.6999999

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	4.4500000	
1	-13.0212927	4.6500000	0.6500000
2	-17.5960703	5.1000000	1.1000000
3	-20.6431212	5.5500000	1.5500000
4	-22.9253621	5.9999999	2.0000000
5	-24.7682619	6.4499999	2.4500000
6	-26.3245201	6.9000000	2.9000000
7	-27.7062082	7.3500000	3.3500000
8	-28.9366488	7.8000000	3.8000000
9	-30.0719309	8.2500000	4.2500000
10	-31.0940461	8.6999999	4.7000000
11	-32.1467724	9.1999999	5.2000000
12	-32.9469175	9.6500000	5.6500000
13	-33.7265306	10.0999999	6.1000000
14	-34.4429808	10.5500000	6.5500000
15	-35.4728622	10.8000000	6.8000000
16	-35.0970087	11.0000000	7.0000000
17	-35.6719203	11.4499999	7.4500000
18	-36.4121616	11.8499999	7.8500000
19	-36.2605467	11.9499999	7.9500000
20	-36.6432958	12.4499999	8.4499999

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	3.5000000	
1	-12.9468002	3.3500000	-0.6500000
2	-17.5588055	2.9000000	-1.1000000
3	-20.5808043	2.4500000	-1.5500000
4	-22.8563833	2.0000000	-2.0000000
5	-24.7384033	1.5500000	-2.4500000
6	-26.2969308	1.1000000	-2.9000000
7	-27.7198877	0.6500000	-3.3500000
8	-28.9457912	0.2000000	-3.8000000
9	-30.0452714	-0.2500000	-4.2500000
10	-31.0531001	-0.7000000	-4.7000000
11	-31.9357543	-1.1500000	-5.1500000
12	-32.9167657	-1.6000000	-5.6000000
13	-33.6852956	-2.0500000	-6.0500000
14	-34.4168429	-2.5000000	-6.4999999
15	-35.0967226	-2.9000000	-6.9000000
16	-35.8800583	-3.2500000	-7.2499999
17	-35.7286062	-3.3500000	-7.3500000
18	-35.8278966	-3.4500000	-7.4500000
19	-36.3107982	-3.9500000	-7.9500000
20	-36.6988506	-4.4000000	-8.4000000

SNUMB=8602T  
1-22, Pass#1

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE NEXT 10 LINES ARE RELATIVE TO THE MAIN LOBE

LOCATION OF RELATIVE MAIN LOBE OF HIGHEST 2 SIDE LOBS  
REL. ANGLE ( DEG )

REL. ANGLE ( DEG )	REL. ANGLE ( DEG )
0.0	0.5500000
-10.9254164	1.0100000
-10.9645414	0.5500000
-17.3264437	-2.0500000
-17.4617777	2.5500000
-17.5116721	-3.1500000
-19.4113469	3.9500000
-27.7744317	2.9700000
-27.5653011	-3.0700000
-27.7347264	2.9500000
-29.4544465	-1.0500000
-27.4455831	-1.4500000
-27.5776974	3.4000000
-24.5271157	6.9999999
-24.41514.0	15.2499999
-24.5538824	4.7000000
-27.3764860	-5.0000000
-27.7745734	-2.8000000
-27.3272771	6.2000000
-27.4655643	-4.2500000
-27.7512517	9.1599999

THE NEXT 10 LINES ARE RELATIVE TO THE MAIN LOBE  
REL. ANGLE ( DEG )

REL. ANGLE ( DEG )	REL. ANGLE ( DEG )
0.0	1.4000000
-10.9254174	1.6000000
-17.4519773	2.0500000
-7.1216431	2.5000000
-22.2447276	2.9500000
-13.5725975	3.4000000
-19.4113469	3.9500000
-27.5776974	4.7000000
-27.1235570	5.2499999
-27.1147512	5.6000000
-27.3272771	6.2000000
-27.5776974	6.9999999
-10.9254174	7.7499999
-10.1147410	8.1000000
-13.7217510	9.1599999
-12.1174149	10.0000000
-14.1411164	10.5000000
-14.3154271	11.0000000
-14.1135373	11.4499999
-14.2521662	12.3000000
-14.7117940	13.2499999

THE NEXT 10 LINES ARE RELATIVE TO THE MAIN LOBE  
REL. ANGLE ( DEG )

REL. ANGLE ( DEG )	REL. ANGLE ( DEG )
0.0	0.5500000
-12.5445414	-0.3000000
-17.5116721	-0.1000000
-17.5116721	-0.5000000
-12.5445414	-1.0500000
-13.4455831	-1.4300000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000
-17.3264437	-2.0500000



SNUMB=3805T

1-17, Pass#1

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 47.5484395

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ( DB ) ANGLE ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-12.7927752	0.3000000
2	-12.9332924	1.6000000
3	-16.9841747	-0.1500000
4	-17.3261299	2.0500000
5	-20.2226043	-0.6000000
6	-20.2434125	2.5000000
7	-20.6797380	7.6999999
8	-22.4736376	-1.0500000
9	-22.4934831	2.9500000
10	-23.3212700	8.5500000
11	-24.0559015	-1.5000000
12	-24.3340569	3.4000000
13	-25.8522973	3.8500000
14	-25.9318614	-1.9500000
15	-26.7540183	4.3000000
16	-26.8770161	15.4000000
17	-27.1035166	-2.4000000
18	-27.9378462	-2.8500000
19	-28.0519300	6.9499999
20	-28.4699359	4.7499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000	
1	-12.9332924	1.6000000	0.6500000
2	-17.3261299	2.0500000	1.1000000
3	-20.2434125	2.5000000	1.5500000
4	-22.4934831	2.9500000	2.0000000
5	-24.3340569	3.4000000	2.4500000
6	-25.8522973	3.8500000	2.9000000
7	-26.7540183	4.3000000	3.3500000
8	-28.4699359	4.7499999	3.8000000
9	-28.5022607	5.2000000	4.2500000
10	-29.7632928	5.7000000	4.7500000
11	-29.5847836	6.1000000	5.1500000
12	-28.0519300	6.9499999	5.9999999
13	-20.6797380	7.6999999	6.7499999
14	-23.3212700	8.5500000	7.6000000
15	-31.0151644	9.3499999	8.4000000
16	-33.7391386	10.2500000	9.3000001
17	-34.5896802	10.5999999	9.6500000
18	-35.3428349	11.0999999	10.1500000
19	-35.3768578	11.5500000	10.6000000
20	-35.8257980	12.0500000	11.1000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000	
1	-12.7927752	0.3000000	-0.6500000
2	-16.9841747	-0.1500000	-1.1000000
3	-20.2226043	-0.6000000	-1.5500000
4	-22.4736376	-1.0500000	-2.0000000
5	-24.0559015	-1.5000000	-2.4500000
6	-25.9318614	-1.9500000	-2.9000000
7	-27.1035166	-2.4000000	-3.3500000
8	-27.9378462	-2.8500000	-3.8000000
9	-29.0754943	-3.2500000	-4.2000000
10	-29.6679810	-3.8000000	-4.7500000
11	-29.5699506	-4.1500000	-5.1000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • •

[illegible]

1	1.0	-81.57002
2	-12.951449	-55.751121
3	-12.942614	-52.401101
4	-12.947597	-45.401101
5	-12.944779	-39.384779
6	-12.944375	-30.101101
7	-12.944975	-24.444975
8	-12.944975	-19.501101
9	-12.944975	-17.151101
10	-12.944975	-16.144975
11	-12.944975	-15.151101
12	-12.944975	-14.151101
13	-12.944975	-13.151101
14	-12.944975	-12.151101
15	-12.944975	-11.151101
16	-12.944975	-10.151101
17	-12.944975	-9.151101
18	-12.944975	-8.151101
19	-12.944975	-7.151101
20	-12.944975	-6.151101
21	-12.944975	-5.151101
22	-12.944975	-4.151101
23	-12.944975	-3.151101
24	-12.944975	-2.151101
25	-12.944975	-1.151101
26	-12.944975	-0.151101
27	-12.944975	0.151101
28	-12.944975	1.151101
29	-12.944975	2.151101
30	-12.944975	3.151101
31	-12.944975	4.151101
32	-12.944975	5.151101
33	-12.944975	6.151101
34	-12.944975	7.151101
35	-12.944975	8.151101
36	-12.944975	9.151101
37	-12.944975	10.151101
38	-12.944975	11.151101
39	-12.944975	12.151101
40	-12.944975	13.151101
41	-12.944975	14.151101
42	-12.944975	15.151101
43	-12.944975	16.151101
44	-12.944975	17.151101
45	-12.944975	18.151101
46	-12.944975	19.151101
47	-12.944975	20.151101
48	-12.944975	21.151101
49	-12.944975	22.151101
50	-12.944975	23.151101
51	-12.944975	24.151101
52	-12.944975	25.151101
53	-12.944975	26.151101
54	-12.944975	27.151101
55	-12.944975	28.151101
56	-12.944975	29.151101
57	-12.944975	30.151101
58	-12.944975	31.151101
59	-12.944975	32.151101
60	-12.944975	33.151101
61	-12.944975	34.151101
62	-12.944975	35.151101
63	-12.944975	36.151101
64	-12.944975	37.151101
65	-12.944975	38.151101
66	-12.944975	39.151101
67	-12.944975	40.151101
68	-12.944975	41.151101
69	-12.944975	42.151101
70	-12.944975	43.151101
71	-12.944975	44.151101
72	-12.944975	45.151101
73	-12.944975	46.151101
74	-12.944975	47.151101
75	-12.944975	48.151101
76	-12.944975	49.151101
77	-12.944975	50.151101
78	-12.944975	51.151101
79	-12.944975	52.151101
80	-12.944975	53.151101
81	-12.944975	54.151101
82	-12.944975	55.151101
83	-12.944975	56.151101
84	-12.944975	57.151101
85	-12.944975	58.151101
86	-12.944975	59.151101
87	-12.944975	60.151101
88	-12.944975	61.151101
89	-12.944975	62.151101
90	-12.944975	63.151101
91	-12.944975	64.151101
92	-12.944975	

[illegible]

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
2	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
3	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
5	1	2	3	4	5	6																																																																																														

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=2728T

1-17, Pass#1

THE MAIN LOBE GAIN IS 47.5448976

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
BANK REL. GAIN ANGLE  
( DB ) ( DEG )

MAIN	0.0	0.9500000
1	-12.7514744	0.3000000
2	-12.9102144	1.6000000
3	-17.3078966	2.0500000
4	-18.3569708	0.
5	-20.2256680	2.5000000
6	-20.6951466	7.7000000
7	-22.5026350	2.9500000
8	-23.3354301	8.5500000
9	-24.3316240	3.4000000
10	-25.8279252	3.8500000
11	-26.7601342	4.3000000
12	-28.0585971	6.9500000
13	-28.4907932	4.7500000
14	-28.5093365	5.2000000
15	-29.4220567	14.9499999
16	-29.5899444	6.1000000
17	-29.7486134	5.7000000
18	-31.0382600	9.3500000
19	-33.6370106	14.3499999
20	-33.7795157	10.2500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000	
1	-12.9102144	1.6000000	0.6500000
2	-17.3078966	2.0500000	1.1000000
3	-20.2256680	2.5000000	1.5500000
4	-22.5026350	2.9500000	2.0000000
5	-24.3316240	3.4000000	2.4500000
6	-25.8279252	3.8500000	2.9000000
7	-26.7601342	4.3000000	3.3500000
8	-28.4907932	4.7500000	3.8000000
9	-28.5093365	5.2000000	4.2500000
10	-29.7486134	5.7000000	4.7500000
11	-29.5899444	6.1000000	5.1500000
12	-28.0585971	6.9500000	6.0000000
13	-20.6951466	7.7000000	6.7500000
14	-23.3354301	8.5500000	7.6000000
15	-31.0382600	9.3500000	8.4000000
16	-33.7795157	10.2500000	9.3000000
17	-34.5925670	10.5999999	9.6499999
18	-35.3558760	11.0999999	10.1499999
19	-35.3683176	11.5999999	10.6499999
20	-35.8125710	12.0500000	11.0999999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000	
1	-12.7514744	0.3000000	-0.6500000

NO FURTHER SIDE LOBES ON THIS SIDE



\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

SNUMB=7487T  
1-18, Pass#1

THE MAIN LOBE GAIN IS 47.549172

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-12.7512550	0.3000000
2	-12.9100733	1.6000000
3	-16.9828191	-0.1500000
4	-17.3075466	2.0500000
5	-20.2204380	-0.6000000
6	-20.7250729	2.5000000
7	-20.4938150	7.6999999
8	-22.4672194	-1.0500000
9	-22.5019064	2.9500000
10	-23.1357440	8.5500000
11	-24.0471101	-1.5000000
12	-24.3307977	3.4000000
13	-25.8273849	3.8500000
14	-25.8989967	-1.9500000
15	-26.7507222	4.3000000
16	-26.9236539	15.4000000
17	-27.0971394	-2.4000000
18	-27.9544759	-2.8500000
19	-28.0612668	6.9499999
20	-28.4913135	4.7499999

RANK	MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** FULL **	1.4000000	
1	-12.9100733	1.6000000	0.6500000
2	-17.3075466	2.0500000	1.1000000
3	-20.2204380	2.9500000	1.5500000
4	-22.5019064	2.9500000	2.0000000
5	-24.3307977	3.4000000	2.4500000
6	-25.8273849	3.8500000	2.9000000
7	-26.7507222	4.3000000	3.3500000
8	-26.9236539	4.7499999	3.8000000
9	-26.9507445	5.2000000	4.2500000
10	-29.7503491	5.7000000	4.7500000
11	-29.5912223	6.1000000	5.1500000
12	-28.0615668	6.9499999	5.9999999
13	-27.6738152	7.6299999	6.7499999
14	-23.3357840	8.5500000	7.6000000
15	-31.0501652	9.3499999	8.4000000
16	-33.7816975	10.2500000	9.3000001
17	-34.5917085	10.9999999	9.6500000
18	-35.3574694	11.0999999	10.1500000
19	-35.3686689	11.9999999	10.6500000
20	-35.8127346	12.6500000	11.1000000

RANK	MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** FULL **	0.5000000	
1	-12.7512550	0.3000000	-0.6500000
2	-16.9828191	-0.1500000	-1.1000000
3	-20.2204380	-0.6000000	-1.5500000
4	-22.4672194	-1.0500000	-2.0000000
5	-24.0471101	-1.5000000	-2.4500000
6	-25.8989967	-1.9500000	-2.9000000
7	-27.0971394	-2.4000000	-3.3500000
8	-27.9544759	-2.8500000	-3.8000000
9	-29.1159067	-3.2500000	-4.2000000
10	-29.6648110	-3.8000000	-4.7500000
11	-29.6658285	-4.1500000	-5.1000000

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=7610T

5-06, Pass#1

\*\*\* ANTENNA LOBE SCANNER \*\*\*

THE MAIN LOBE GAIN IS 47.919 869

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ( DB ) TRUE ANGLE ( DEG )

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )
1	0.0	0.9500000
2	-13.4395596	1.6000000
3	-13.5351152	0.3000000
4	-18.0671434	2.0500000
5	-18.1761332	-0.1500000
6	-21.1343040	2.5000000
7	-21.2782864	-0.6000000
8	-23.3975610	2.9500000
9	-23.6311636	-1.0500000
10	-25.2775530	3.4000000
11	-25.5855074	-1.5000000
12	-26.9033003	3.8500000
13	-26.9253762	15.4000000
14	-27.2742853	-1.9500000
15	-28.2689161	4.3000000
16	-28.6977042	-2.4000000
17	-29.5009871	4.7499999
18	-29.7683477	16.9499999
19	-29.9919432	-2.8500000
20	-30.6564312	5.2000000
21	-31.1275902	31.2499998

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	0.0	1.4000000	0.6500000
2	-13.4395596	1.6000000	1.1000000
3	-18.0671434	2.0500000	1.5500000
4	-18.1761332	2.5000000	2.0000000
5	-21.1343040	2.9500000	2.4500000
6	-21.2782864	3.4000000	2.9000000
7	-23.3975610	3.8500000	3.3500000
8	-23.6311636	4.3000000	3.8000000
9	-25.2775530	4.7499999	4.2500000
10	-25.5855074	5.2000000	4.7000000
11	-26.9033003	5.6500000	5.1500000
12	-26.9253762	6.1000000	5.6000000
13	-27.2742853	6.5500000	6.0500000
14	-28.2689161	6.9999999	6.5000000
15	-28.6977042	7.4499999	6.9499999
16	-29.5009871	7.9000000	7.3999999
17	-29.7683477	8.3499999	7.8500000
18	-29.9919432	8.8000000	8.3000000
19	-30.6564312	9.2500000	8.7500000
20	-31.1275902	9.7000000	9.2000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	0.0	0.5000000	-0.6500000
2	-13.5351152	0.3000000	-1.1000000
3	-18.1761332	-0.1500000	-1.5500000
4	-21.2782864	-0.6000000	-2.0000000
5	-23.6311636	-1.0500000	-2.4500000
6	-25.5855074	-1.5000000	-2.9000000
7	-27.2742853	-1.9500000	-3.3500000
8	-28.2689161	-2.4000000	-3.8000000
9	-28.6977042	-2.8500000	-4.2500000
10	-29.5009871	-3.3000000	-4.7000000
11	-29.7683477	-3.7500000	-5.1500000
12	-30.6564312	-4.2000000	-5.6000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7478T  
5-16, Pass#2

THE MAIN LOBE GAIN IS 55.2212550

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
1	0.0	0.9500000
2	-2.4846993	15.4999999
3	-2.5919332	31.1499999
4	-5.8790169	15.0500000
5	-6.0360947	30.1999998
6	-7.1381884	15.9499999
7	-7.3163519	32.2500000
8	-31.7532466	28.4499998
9	-33.7454100	14.5499997
10	-37.0932474	4.3000000
11	-38.2104859	26.5500000
12	-40.1887589	8.0999999
13	-40.2117572	8.1999999
14	-40.2974110	23.0500000
15	-40.3358025	23.1499999
16	-40.3545470	21.5500000
17	-40.3904519	21.6499999
18	-40.4418159	22.3499999
19	-40.4878526	22.4499998
20	-40.4972458	22.2500000
21	-40.5146139	6.9499999

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
** NULL **			
1	-37.0932474	4.3000000	3.3500000
2	-40.5146139	6.9499999	5.9999999
3	-40.6218129	7.1500000	6.2000000
4	-40.6737127	7.2499999	6.3000000
5	-40.7351275	7.4499999	6.4999999
6	-40.7522106	7.6000000	6.6500000
7	-40.1887589	8.0999999	7.1499999
8	-40.2117572	8.1999999	7.2499999
9	-40.7053356	8.8499999	7.8999999
10	-40.6591134	9.0500000	8.1000000
11	-5.8790169	15.0500000	14.1000000
12	-2.4846993	15.4999999	14.5500000
13	-7.1381884	15.9499999	15.0000000
14	-40.3545470	21.5500000	20.5999999
15	-40.3904519	21.6499999	20.6999998
16	-40.5725279	22.0000000	21.0500000
17	-40.5834646	22.0999999	21.1499999
18	-40.4972458	22.2500000	21.3000000
19	-40.4418159	22.3499999	21.3999999
20	-40.4878526	22.4499998	21.4999998

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )  
NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=2726T  
5-09, Pass#1

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE RAIN IS 55.002494

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN (DB)	ANGLE (DEG)
MAIN	0.0	0.950000
1	-2.4836355	15.4999999
2	-2.5794106	31.1499999
3	-5.865963	15.7500000
4	-5.7999657	30.1999998
5	-7.119832	15.9499999
6	-7.2632599	32.2500000
7	-15.7194564	7.6999999
8	-20.1409578	23.0000000
9	-20.2596867	22.2500000
10	-21.4796637	6.5999999
11	-21.4241047	0.3000000
12	-21.5799198	0.1000000
13	-22.1614588	24.0000000
14	-25.813264	29.1499999
15	-26.286525	16.6999999
16	-26.313611	33.4000001
17	-27.0135508	2.7500000
18	-27.5828614	-0.7000000
19	-24.6923738	17.3999999
20	-28.3593240	-4.9000000

MAIN LOBE FULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	0.0	2.4500000	
1	-27.0135508	2.7500000	1.8000000
2	-17.8790717	3.6000000	2.6500000
3	-12.0056252	4.4799999	3.5900000
4	-12.5952344	4.9500000	4.0000000
5	-12.1635330	5.9000000	4.9500000
6	-28.411231	6.8000000	5.8500000
7	-18.7094564	7.6999999	6.7499999
8	-21.4796637	8.5999999	7.6499999
9	-28.682134	9.4000000	8.4500000
10	-12.129306	10.3499999	9.4000000
11	-13.6987247	11.1500000	10.2000000
12	-15.062518	11.4499999	10.5000000
13	-13.2537105	12.1999999	11.2500000
14	-12.3957516	12.6500000	11.7000000
15	-5.865963	13.0500000	14.1000000
16	-2.4836355	15.4999999	14.5900000
17	-7.119832	15.9499999	15.0000000
18	-26.286525	16.6999999	15.9499999
19	-28.0923738	17.3999999	16.4499998
20	-31.1577692	17.6999999	16.9499995

MAIN LOBE FULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	0.0	0.3500000	
1	-21.4241047	0.3000000	-0.0500000
2	-21.5799198	0.1000000	-0.8500000
3	-27.5828614	-0.7000000	-1.6500000
4	-31.4065728	-1.7000000	-2.6500000
5	-12.6829209	-2.2500000	-3.2000000
6	-13.412725	-3.2500000	-4.2000000
7	-31.1237798	-4.0000000	-4.9500000
8	-28.3593240	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=4288T  
5-09, Pass#1

\*\*\*\*\* LINE 16 LEFT SIDE \*\*\*\*\*

THE MAIN LORR 12 15 18 21

LOCATION RELATIVE MAIN TO HIGHEST 20 SIDE LORR'S  
WAVE REL. MAIN TRUE ANGLE  
( DEG ) ( DEG )

WAVE	REL. MAIN ( DEG )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-2.4924451	11.101000	13.593445
2	-2.5526126	11.249999	13.799999
3	-2.5544749	15.199999	17.744999
4	-2.9624415	16.749999	19.702440
5	-7.1472161	15.999999	8.852783
6	-7.2416349	12.299999	5.058365
7	-11.546410	7.350000	-4.196410
8	-21.1325441	10.250000	-10.882544
9	-21.1342367	21.999999	-3.164237
10	-21.1367953	22.550000	-3.419535
11	-21.1376749	19.599999	-2.457675
12	-21.1235554	9.700000	-11.423555
13	-21.0713722	23.750000	-2.678628
14	-22.5441963	24.500000	-1.955804
15	-21.144454	2.700000	-18.444454
16	-21.1499773	-0.650000	-20.799977
17	-24.4422235	13.749999	-10.702223
18	-21.1772199	16.850000	-5.677220
19	-21.1716776	17.349999	-6.171678
20	-25.2545148	29.199999	-3.944515

MAIN LORR NOSE AND FIRST 20 SIDE LORR'S TO RIGHT OF (REL. MAIN) MAIN LORR  
REL. MAIN TRUE ANGLE REL. ANGLE  
( DEG ) ( DEG ) ( DEG )

WAVE	REL. MAIN ( DEG )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-23.148456	2.700000	-20.448456
2	-22.7413434	3.970000	-18.771343
3	-22.5497827	4.350000	-18.199783
4	-21.2474571	5.690000	-15.557457
5	-16.54410	7.350000	-11.194100
6	-21.242540	9.000000	-12.042540
7	-21.1393341	10.650000	-13.719334
8	-3.142447	11.999999	-15.142447
9	-11.141654	12.349999	-13.491654
10	-11.141650	12.749999	-13.891650
11	-20.1415507	13.149999	-13.291551
12	-11.144766	15.079999	-16.224766
13	-11.1416461	16.550000	-17.691646
14	-11.1452146	18.999999	-20.145215
15	-24.1772199	16.800000	-7.377220
16	-24.1735776	17.349999	-7.823578
17	-25.6131271	17.699999	-7.813127
18	-24.1754131	18.699999	-6.525413
19	-3.1572196	19.199999	-16.347220
20	-3.1268977	20.340000	-17.216898

MAIN LORR NOSE AND FIRST 20 SIDE LORR'S TO LEFT OF (REL. MAIN) MAIN LORR  
REL. MAIN TRUE ANGLE REL. ANGLE  
( DEG ) ( DEG ) ( DEG )

WAVE	REL. MAIN ( DEG )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-22.1499973	-0.650000	-21.499997
2	-14.143416	-1.500000	-12.643416
3	-21.1444771	-1.350000	-19.794477
4	-24.1413456	-2.190000	-21.951346
5	-11.147213	-3.690000	-7.457213

NO FURTHER SIDE LORR'S ON THIS SITE

SNUMB=4288T  
5-09, Pass#5

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE IS 15 54.98 24

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN REL. ANGLE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-2.8382187	19.8499999
2	-2.9299569	16.3499999
3	-4.015441	19.3499999
4	-4.0647071	15.2499999
5	-11.7922754	20.3499999
6	-11.110574	17.4499999
7	-17.3676915	8.0500000
8	-14.837961	14.2999999
9	-19.1645757	2.0000000
10	-19.8695921	19.2500000
11	-19.9679126	22.6999999
12	-21.4859345	23.2500000
13	-21.994282	12.4499999
14	-21.1459393	16.5500000
15	-23.841446	11.5500000
16	-24.1214104	13.4000001
17	-24.5795227	11.0999999
18	-25.315545	-3.2500000
19	-25.335505	26.0999999
20	-25.5411644	-1.0500000

MAIN LOBE GAIN AND FIRST 20 SIDE-LOBES TO RIGHT OF (ARROW) MAIN LOBE  
REL. GAIN REL. ANGLE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-25.141777	6.5000000
2	-27.814644	7.3000000
3	-17.3975715	8.0000000
4	-12.2155323	8.6999999
5	-12.4173613	9.5000000
6	-27.3797410	10.3499999
7	-24.5795227	11.0999999
8	-34.1621324	11.9000000
9	-34.4151394	12.5499999
10	-25.1777427	13.4000000
11	-27.1777221	14.1999999
12	-13.1637222	15.0999999
13	-21.1459393	16.5500000
14	-27.1413112	17.3999999
15	-3.1211041	17.8499999
16	-4.019441	18.3499999
17	-27.8362157	19.8499999
18	-17.7922754	20.3499999
19	-27.2951151	21.2999999
20	-19.942127	22.6999999

MAIN LOBE GAIN AND FIRST 20 SIDE-LOBES TO LEFT OF (ARROW) MAIN LOBE  
REL. GAIN REL. ANGLE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-27.895145	2.7500000
2	-15.180757	2.0000000
3	-17.163759	3.1000000
4	-14.1954716	1.4000000
5	-27.081276	10.3499999
6	-21.0411444	11.0999999
7	-14.174715	11.9000000
8	-17.1224105	12.5499999
9	-20.1155445	13.4000000
10	-17.1445925	14.1999999
11	-17.17371	15.0999999

NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=4288T  
5-09, Pass#4

\*\*\*\*\* ANTENNA LOBE SUMMER \*\*\*\*\*

THE MAIN LOBE IS 150 DEGS FROM THE VERTICAL

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	4.0000000
1	-2.7545234
2	-2.794433
3	-4.4271803
4	-4.4477348
5	-9.4642144
6	-9.765568
7	-17.544549
8	-19.7121213
9	-19.7751868
10	-19.5142791
11	-21.4431177
12	-21.611607
13	-21.7475100
14	-21.8524816
15	-21.9341954
16	-22.7212347
17	-23.7575561
18	-24.7724607
19	-25.1661019
20	-25.643407

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ARROW) MAIN LOBE

REL. GAIN ( DB )	ANGLE ( DEG )
MAIN LOBE	5.4900000
1	-29.2222153
2	-29.7777727
3	-29.7315796
4	-19.7151213
5	-27.9777420
6	-13.197223
7	-25.6424521
8	-25.1661019
9	-32.425636
10	-26.2143774
11	-19.7751868
12	-31.7529331
13	-4.4271803
14	-2.7545204
15	-9.4642144
16	-22.547421
17	-22.6271646
18	-22.7152933
19	-21.7361954
20	-21.8524816

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (ARROW) MAIN LOBE

REL. GAIN ( DB )	ANGLE ( DEG )
MAIN LOBE	3.1000000
1	-25.9435397
2	-3.7655266
3	-17.544549
4	-27.1435351
5	-11.7767904
6	-24.7724607
7	-25.1661019
8	-17.544549
9	-31.6171746

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=4288T  
5-09, Pass#3

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 54.993275

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN (DB) ANGLE (DEG)

RANK	REL. GAIN (DB)	ANGLE (DEG)
1	3.0	3.000000
2	-7.5517938	17.6999999
3	-7.6324990	33.7500000
4	-4.8167753	17.2500000
5	-4.9379954	32.7500000
6	-8.7231207	16.1499999
7	-8.9643269	34.8499999
8	-17.0831227	7.6999999
9	-19.565775	-1.6500000
10	-20.1807222	22.3000000
11	-21.3108320	22.6999999
12	-21.3134561	12.7499999
13	-21.3275315	36.7500000
14	-21.0701521	27.9999999
15	-21.6726430	31.8499999
16	-21.9905556	26.8499999
17	-25.1331339	27.5999999
18	-25.4916690	27.2499999
19	-25.7633295	4.0500000
20	-26.127509	11.7500000
21	-26.8332266	7.5499999

MAIN LOBE GAIN AND FIRST 20 SIDE LOBES TO RIGHT OF (ARROYO) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
1	4.0000000	4.0000000	1.0500000
2	-25.7633295	4.0500000	3.2000000
3	-32.5365181	6.2000000	4.7000000
4	-17.2951227	7.6999999	6.3500000
5	-34.7781565	9.3499999	7.3500000
6	-36.1831332	10.8499999	9.7499999
7	-27.3134661	12.7499999	10.8000000
8	-33.2126605	13.8000000	11.1500000
9	-34.4332542	14.1500000	11.9000000
10	-34.4762616	14.9000000	14.2500000
11	-4.8167753	17.2500000	14.6999999
12	-2.5517938	17.6999999	15.1499999
13	-8.7231207	16.1499999	17.6999999
14	-32.7331543	20.6999999	18.7500000
15	-20.1775319	21.7500000	19.3000000
16	-21.3108320	22.3000000	19.6999999
17	-21.3134561	22.6999999	21.5500000
18	-35.0161936	24.5500000	21.9499999
19	-33.987192	24.9499999	22.3000000
20	-36.8459754	25.8000000	24.2499999
21	-25.4916690	27.2499999	

MAIN LOBE GAIN AND FIRST 20 SIDE LOBES TO LEFT OF (ARROYO) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
1	1.0500000	1.4000000	-1.6000000
2	-33.7564133	0.4000000	-2.6000000
3	-32.9664336	-0.6000000	-3.6000000
4	-19.565775	-1.6000000	-4.6000000
5	-34.4332542	-2.6000000	-5.6000000
6	-36.1831332	-3.6000000	-6.6000000

NO FURTHER SIDE LOBES IN THIS SET

SNUMB=4288T  
5-09, Pass#2

THE MAIN LOBE DATA IS

RELATIVE DATA OF HIGHEST 20 SIDE LOBES  
REL. DATA ( DEG )

REL. DATA ( DEG )	REL. DATA ( DEG )	REL. DATA ( DEG )
1	-1.5492387	16.5999999
2	-2.6395302	32.9999999
3	-5.1331113	16.1999999
4	-5.1912792	31.4999999
5	-7.4391176	33.8499999
6	-1.5896052	17.1999999
7	-17.1571291	6.3999999
8	-13.4467375	3.7999999
9	-14.2712331	30.1999999
10	-12.9293319	14.1999999
11	-2.1494733	34.0999999
12	-2.1372214	18.4499999
13	-21.9427711	17.9499999
14	-22.1575396	15.2499999
15	-22.9354666	29.4999999
16	-23.1945994	14.4499999
17	-23.7319969	-1.3999999
18	-24.4318425	2.3999999
19	-24.4595409	35.0999999
20	-25.4443373	24.3999999

RELATIVE DATA OF HIGHEST 20 SIDE LOBES TO RIGHT OF (REL. DATA) MAIN LOBE  
REL. DATA ( DEG )

REL. DATA ( DEG )	REL. DATA ( DEG )	REL. DATA ( DEG )
1	-1.4467575	3.7999999
2	-24.129713	4.4999999
3	-24.4319375	5.3999999
4	-31.4435431	6.2499999
5	-24.2547361	7.0599999
6	-31.9411276	7.9999999
7	-31.7421495	8.7999999
8	-31.146143	9.6999999
9	-31.4499977	10.3499999
10	-27.7437721	11.3499999
11	-31.4958495	12.0999999
12	-27.637732	13.0999999
13	-33.611791	13.8499999
14	-23.179574	14.4499999
15	-14.2453115	14.8499999
16	-22.757396	15.2499999
17	-3.8311176	16.1999999
18	-1.8993302	16.5999999
19	-1.919594	17.1999999
20	-21.247711	17.8499999

RELATIVE DATA OF HIGHEST 20 SIDE LOBES TO LEFT OF (REL. DATA) MAIN LOBE  
REL. DATA ( DEG )

REL. DATA ( DEG )	REL. DATA ( DEG )	REL. DATA ( DEG )
1	-25.78491	1.9999999
2	-17.347121	0.3999999
3	-17.447311	-0.5999999
4	-21.711735	-1.1999999
5	-35.41544	-2.1999999
6	-27.73531	-3.1999999
7	-3.1999999	-4.1999999
8	-3.1999999	-4.7999999



SNUMB=3404T

5-29, Pass#1

\*\*\* ANTENNA LOBE SCANNER \*\*\*

THE MAIN LOBE GAIN IS 55.5692101

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-2.5167341	15.4999999
2	-2.5661049	31.1499999
3	-5.9850769	15.0500000
4	-6.0276098	30.1999998
5	-7.2518663	15.9499999
6	-7.3308525	32.1999998
7	-25.9125128	0.3000000
8	-26.8225000	1.6000000
9	-30.0418720	14.4000000
10	-31.0144300	16.6499999
11	-31.3967772	29.4499998
12	-32.3351212	33.0000000
13	-34.8490084	2.0000000
14	-34.4856710	40.1000000
15	-35.4602690	17.0999999
16	-35.7845554	28.3999999
17	-36.9889307	33.4000001
18	-37.3338518	2.5500000
19	-37.3935947	40.6500000
20	-37.5218487	13.9000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4500000	
1	-26.0223000	1.6000000	0.6500000
2	-34.0490084	2.0000000	1.0500000
3	-37.3338518	2.5500000	1.6000000
4	-47.8516922	3.4000000	2.4500000
5	-50.4714656	3.8500000	2.9000000
6	-49.2536564	4.4000000	3.4500000
7	-50.2272301	4.6000000	3.6500000
8	-54.4931464	5.1500000	4.2000000
9	-53.9364934	6.1500000	5.2000000
10	-52.8368101	6.8000000	5.8500000
11	-43.9571075	7.6999999	6.7499999
12	-46.1468163	8.5000000	7.5500000
13	-53.4251280	9.5000000	8.5500001
14	-53.4849720	9.7500000	8.8000001
15	-53.5996923	10.1500000	9.2000000
16	-55.9060473	10.5999999	9.6500000
17	-54.3259277	11.3000000	10.3500000
18	-50.4157414	11.6500000	10.7000000
19	-50.1002817	11.9999999	11.0500000
20	-49.9505701	12.5500000	11.6000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.4500000	
1	-25.9125128	0.3000000	-0.6500000
2	-34.4856710	-0.1000000	-1.0500000
3	-37.3935947	-0.6500000	-1.6000000
4	-47.3800077	-1.5000000	-2.4500000
5	-50.9498529	-1.9500000	-2.9000000
6	-49.4613333	-2.4500000	-3.4000000
7	-50.6898768	-2.7000000	-3.6500000
8	-54.9968476	-3.2500000	-4.2000000
9	-53.5686808	-4.2500000	-5.2000000
10	-52.7704592	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

SNUMB=8462T  
6-17, Pass#1

THE MAIN LOBE GAIN IS 55.491246

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-2.5000000	0.9500000
2	-2.5000000	15.4999999
3	-2.5000000	31.1499999
4	-2.5000000	46.8999999
5	-2.5000000	62.6499999
6	-2.5000000	78.3999999
7	-2.5000000	94.1499999
8	-2.5000000	109.8999999
9	-2.5000000	125.6499999
10	-2.5000000	141.3999999
11	-2.5000000	157.1499999
12	-2.5000000	172.8999999
13	-2.5000000	188.6499999
14	-2.5000000	204.3999999
15	-2.5000000	220.1499999
16	-2.5000000	235.8999999
17	-2.5000000	251.6499999
18	-2.5000000	267.3999999
19	-2.5000000	283.1499999
20	-2.5000000	298.8999999

REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN LOBE	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-23.7214378	1.5000000
2	-23.7214378	1.5000000
3	-23.7214378	1.5000000
4	-23.7214378	1.5000000
5	-23.7214378	1.5000000
6	-23.7214378	1.5000000
7	-23.7214378	1.5000000
8	-23.7214378	1.5000000
9	-23.7214378	1.5000000
10	-23.7214378	1.5000000
11	-23.7214378	1.5000000
12	-23.7214378	1.5000000
13	-23.7214378	1.5000000
14	-23.7214378	1.5000000
15	-23.7214378	1.5000000
16	-23.7214378	1.5000000
17	-23.7214378	1.5000000
18	-23.7214378	1.5000000
19	-23.7214378	1.5000000
20	-23.7214378	1.5000000

REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN LOBE	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-23.7214378	1.5000000
2	-23.7214378	1.5000000
3	-23.7214378	1.5000000
4	-23.7214378	1.5000000
5	-23.7214378	1.5000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=8462T  
6-17, Pass#2

THE MAIN LOBE GAIN IS 55.214241

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
1	-2.5463057	16.5999999
2	-2.6141109	32.5000000
3	-5.3408642	16.1999999
4	-5.4335232	31.4999999
5	-7.9490004	17.0999999
6	-8.0633107	33.5499997
7	-31.2033503	29.6999999
8	-40.1503239	9.1999999
9	-40.2632480	24.3499999
10	-40.2913361	24.2500000
11	-40.3630533	-5.0000000
12	-40.4089760	22.8499999
13	-40.4184728	23.5500000
14	-40.4196477	23.6499999
15	-40.4469256	22.9499998
16	-40.4520454	25.3000000
17	-40.4697412	25.1999998
18	-40.4972954	23.0500000
19	-40.5308375	-4.0500000
20	-40.5429564	24.9499998

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-40.6117716	8.2500000	6.2500001
2	-40.6162195	8.3499999	6.3500000
3	-40.6651263	8.4499999	6.4500000
4	-40.6837897	8.5500000	6.5500000
5	-40.7205945	8.6500000	6.6500000
6	-40.6949120	8.7500000	6.7500001
7	-40.1503239	9.1999999	7.2000000
8	-40.6384926	9.5999999	7.6000000
9	-40.6909232	9.6999999	7.7000000
10	-40.7249076	9.8000000	7.8000000
11	-40.6973291	9.9000000	7.9000000
12	-40.6434808	10.0000000	8.0000000
13	-5.3408642	16.1999999	14.1999998
14	-2.5463057	16.5999999	14.5999999
15	-7.9490004	17.0999999	15.0999999
16	-40.4089760	22.8499999	20.8499999
17	-40.4469256	22.9499999	20.9499998
18	-40.4972954	23.0500000	21.0500000
19	-40.5612282	23.1999999	21.1999998
20	-40.5762963	23.3000000	21.3000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-4.5308375	-4.0500000	-6.0500000
2	-40.6334852	-4.2500000	-6.2499999
3	-40.6871495	-4.3500000	-6.3500000
4	-40.6954754	-4.4500000	-6.4499999
5	-40.7114679	-4.5500000	-6.5500000
6	-40.7207860	-4.6500000	-6.6499999

NO FURTHER SIDE LOBES ON THIS SIDE



\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=4171T  
1-23, Pass#4

THE MAIN LOBE GAIN IS 45.3011589

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RAWK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	4.9999999
1	-12.8325224	5.6500000
2	-12.9156017	4.3500000
3	-17.1066046	7.9999999
4	-17.1510983	3.9000000
5	-17.4322457	6.1000000
6	-18.6072278	6.6000000
7	-18.6364379	3.4000000
8	-19.3693361	2.0000000
9	-19.8984404	3.1000000
10	-20.0768418	6.9000000
11	-22.8662930	7.4499999
12	-23.3056126	2.5500000
13	-24.6341152	8.6999999
14	-24.8616910	1.3500000
15	-25.8714886	-0.2500000
16	-26.0027361	11.0999999
17	-26.5033784	-1.0500000
18	-26.6322899	10.3000000
19	-27.3211093	-2.1500000
20	-27.7068319	12.1999999

RAWK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	5.4500000	
1	-12.8325224	5.6500000	0.6500000
2	-17.4322457	6.1000000	1.1000000
3	-18.6072278	6.6000000	1.6000000
4	-20.0768418	6.9000000	1.9000000
5	-22.8662930	7.4499999	2.4500000
6	-17.1066046	7.9999999	3.0000000
7	-24.6341152	8.6999999	3.7000000
8	-28.2117429	9.2500000	4.2500000
9	-29.0479412	9.6999999	4.7000000
10	-26.6322899	10.3000000	5.3000000
11	-26.0027361	11.0999999	6.1000000
12	-27.7068319	12.1999999	7.2000000
13	-30.1534753	13.4000000	8.4000000
14	-31.3760986	14.0500000	9.0500000
15	-35.8230948	14.9000000	9.9000000
16	-35.9558244	15.4499999	10.4500000
17	-34.3484225	15.9499999	10.9500000
18	-32.7574086	16.3999999	11.4000000
19	-37.3014741	17.2500000	12.2500000
20	-37.2819552	17.7500000	12.7500000

RAWK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	4.5500000	
1	-12.9156017	4.3500000	-0.6500000
2	-17.1510983	3.9000000	-1.1000000
3	-18.6364379	3.4000000	-1.6000000
4	-19.8984404	3.1000000	-1.9000000
5	-23.3056126	2.5500000	-2.4500000
6	-19.3693361	2.0000000	-3.0000000
7	-24.8616910	1.3500000	-3.6499999
8	-28.0751691	0.7500000	-4.2499999
9	-29.0480886	0.3500000	-4.6500000
10	-25.8714886	-0.2500000	-5.2499999
11	-26.5033784	-1.0500000	-6.0500000
12	-27.3211093	-2.1500000	-7.1499999
13	-28.8733954	-3.3000000	-8.3000000
14	-31.2834849	-3.9500000	-8.9499999
15	-35.1468053	-4.7500000	-9.7499999

NO FURTHER SIDE LOBES ON THIS SIDE

\* \* \* \* ANTENNA LOBE SCANNER \* \* \* \*

SNUMB=4171T  
1-23, Pass#3

THE MAIN LOBE GAIN IS 45.3062787

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	4.0000000
1	-12.9113693	4.6500000
2	-12.9867535	3.3500000
3	-16.9168215	0.6500000
4	-17.0769958	2.5000000
5	-17.2355175	5.1000000
6	-18.6066890	2.4000000
7	-18.7579422	5.6000000
8	-19.5047774	7.3500000
9	-20.0967965	5.9000000
10	-23.3996201	1.5500000
11	-24.1155694	6.4499999
12	-25.9086833	8.3000000
13	-26.2006450	-0.2500000
14	-26.3002996	-2.7000000
15	-26.6671405	-3.0000000
16	-27.4557061	11.1999999
17	-27.6302671	10.6999999
18	-27.6561465	10.6000000
19	-27.8421469	-1.3000000
20	-28.1754189	9.4000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	4.4500000	
1	-12.9113693	4.6500000	0.6500000
2	-17.2355175	5.1000000	1.1000000
3	-18.7579422	5.6000000	1.6000000
4	-20.0967965	5.9000000	1.9000000
5	-24.1155694	6.4499999	2.4500000
6	-19.5047774	7.3500000	3.3500000
7	-25.9086833	8.3000000	4.3000000
8	-28.1754189	9.4000000	5.4000000
9	-31.8925085	10.0999999	6.1000000
10	-27.6302671	10.6999999	6.7000000
11	-27.6561465	10.6000000	6.8000000
12	-27.4557061	11.1999999	7.2000000
13	-32.9786391	12.9999999	8.9999999
14	-35.2112956	13.9499999	9.9499999
15	-34.9890203	14.4000000	10.4000000
16	-29.8211980	15.1500000	11.1500000
17	-38.4251068	16.1999998	12.1999998
18	-38.3207850	16.6499999	12.6499999
19	-39.8752615	17.0500000	13.0500000
20	-42.8657665	17.5500000	13.5500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	3.5000000	
1	-12.9867535	3.3500000	-0.6500000
2	-17.0769958	2.9000000	-1.1000000
3	-18.6066890	2.4000000	-1.6000000
4	-23.3996201	1.5500000	-2.4500000
5	-16.9168215	0.6500000	-3.3500000
6	-26.2006450	-0.2500000	-4.2500000
7	-27.8421469	-1.3000000	-5.3000000
8	-31.2047071	-2.0000000	-5.9999999
9	-26.3002996	-2.7000000	-6.7000000
10	-26.6671405	-3.0000000	-6.9999999
11	-31.9049001	-4.9000000	-8.9000000

NO FURTHER SIDE LOBES ON THIS SIDE

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=4171T  
1-23, Pass#2

THE MAIN LOBE GAIN IS 45.4996330

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
1	0.0	3.0000000
2	-12.8041649	2.3500000
3	-12.9315119	3.6500000
4	-17.2201746	4.1000000
5	-17.4370646	1.9000000
6	-18.1365647	7.6999999
7	-18.6271539	1.6000000
8	-18.7666278	1.4000000
9	-19.9463053	4.9000000
10	-20.7159443	-1.7000000
11	-24.0719504	5.4500000
12	-24.2982287	0.5500000
13	-24.6273131	6.4999999
14	-25.2071514	5.9000000
15	-25.3677883	-0.4500000
16	-25.7374415	-0.6500000
17	-25.8415928	0.1000000
18	-26.4766302	12.6999999
19	-27.2476721	10.1999999
20	-28.2891641	-4.1500000
	-29.3659115	17.5500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	3.4500000	
1	-12.9315119	3.6500000	0.6500000
2	-17.2201746	4.1000000	1.1000000
3	-18.6271539	4.6000000	1.6000000
4	-19.9463053	4.9000000	1.9000000
5	-24.0719504	5.4500000	2.4500000
6	-25.2071514	5.9000000	2.9000000
7	-24.6273131	6.4999999	3.5000000
8	-18.1365647	7.6999999	4.7000000
9	-30.9420934	9.0000000	6.0000000
10	-31.4118605	9.4499999	6.4500000
11	-31.4162097	9.5500000	6.5500000
12	-27.2476721	10.1999999	7.2000000
13	-33.1407375	10.9000000	7.9000000
14	-33.2485013	11.4499999	8.4499999
15	-26.4766302	12.6999999	9.8999999
16	-33.3815856	13.7499999	10.7499999
17	-34.6035342	14.1500000	11.1500000
18	-36.0675902	14.6500000	11.6500000
19	-35.6888623	15.1500000	12.1500000
20	-34.1877036	15.5999999	12.5999999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	2.5000000	
1	-12.8041649	2.3500000	-0.6500000
2	-17.4370646	1.9000000	-1.1000000
3	-18.7666278	1.4000000	-1.6000000
4	-24.2982287	0.5500000	-2.4500000
5	-25.8415928	0.1000000	-2.9000000
6	-25.3677883	-0.4500000	-3.4500000
7	-25.7374415	-0.6500000	-3.6500000
8	-20.7159443	-1.7000000	-4.7000000
9	-31.5891590	-3.0500000	-6.0500000
10	-32.6192460	-3.5000000	-6.4999999
11	-28.2891641	-4.1500000	-7.1499999
12	-34.0846930	-4.8500000	-7.8500000

NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=4171T  
1-23, Pass#1

\* \* \* \* ANTENNA LOBE SCANNER \* \* \* \*

THE MAIN LOBE GAIN IS 45.3075547

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
BANK REL. GAIN ANGLE  
( DB ) ( DEG )

MAIN	0.0	2.0000000
1	-12.9362965	2.6500000
2	-12.9441814	1.3500000
3	-14.8226929	0.3500000
4	-16.2694435	3.6500000
5	-17.1349764	3.1000000
6	-17.2623854	0.9000000
7	-21.8583646	-1.3500000
8	-22.7438679	5.4000000
9	-23.3774176	-0.4500000
10	-23.7896094	4.4500000
11	-24.9378414	-0.9000000
12	-25.4495573	4.9000000
13	-26.7407475	-3.1500000
14	-27.2017274	32.4000001
15	-27.2725258	7.1500000
16	-27.6858468	9.1500000
17	-27.9687972	6.2499999
18	-28.0437083	-2.2500000
19	-28.1228499	6.7499999
20	-28.1240005	-5.0000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
BANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	** NULL **	2.4500000	
1	-12.9362965	2.6500000	2.6500000
2	-17.1349764	3.1000000	1.1000000
3	-16.2694435	3.6500000	1.6500000
4	-23.7896094	4.4500000	2.4500000
5	-25.4495573	4.9000000	2.9000000
6	-22.7438679	5.4000000	3.4000000
7	-27.9687972	6.2499999	4.2500000
8	-28.1228499	6.7499999	4.7500000
9	-27.2725258	7.1500000	5.1500000
10	-30.8247952	8.0500000	6.0500000
11	-27.6858468	9.1500000	7.1500000
12	-33.2294421	10.3499999	8.3499999
13	-32.1743531	11.2499999	9.2499999
14	-35.8339319	12.2499999	10.2499999
15	-33.1865144	13.0999999	11.0999999
16	-36.0003290	13.5500000	11.5500000
17	-36.9695959	14.0999999	12.0999999
18	-34.7104483	14.5999999	12.5999999
19	-34.9165044	14.8499999	12.8499999
20	-38.7324595	15.4000000	13.4000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
BANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	** NULL **	1.5500000	
1	-12.9441814	1.3500000	-0.6500000
2	-17.2623854	0.9000000	-1.1000000
3	-14.8226929	0.3500000	-1.6500000
4	-23.3774176	-0.4500000	-2.4500000
5	-24.9378414	-0.9000000	-2.9000000
6	-21.8583646	-1.3500000	-3.3500000
7	-28.0437083	-2.2500000	-4.2499999
8	-26.7407475	-3.1500000	-5.1500000
9	-30.3455691	-4.0500000	-6.0500000
10	-30.6853209	-4.5500000	-6.5500000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7542T  
3-06, Pass#1

THE MAIN LOBE GAIN IS 45.51780P4

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-12.9336786	1.6000000
2	-12.9984999	0.3000000
3	-17.3619432	2.0500000
4	-17.4870453	-0.1500000
5	-18.6779509	2.5500000
6	-18.8758287	-0.6500000
7	-20.3417430	-0.9500000
8	-24.3401027	3.4000000
9	-24.6396527	-1.5000000
10	-25.3795252	4.4000000
11	-25.7958112	-2.5000000
12	-25.8784709	4.6000000
13	-25.9462366	3.6500000
14	-26.2940965	-1.9500000
15	-27.5813603	8.0999999
16	-28.9479351	6.2499999
17	-29.5239973	14.9499999
18	-29.5283923	5.2000000
19	-29.6630654	-4.3500000
20	-30.0547667	-3.3000000

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	0.0	1.4000000	
1	-12.9336786	1.6000000	0.6500000
2	-17.3619432	2.0500000	1.1000000
3	-18.6779509	2.5500000	1.6000000
4	-24.3401027	3.4000000	2.4500000
5	-25.9462366	3.6500000	2.9000000
6	-25.3795252	4.4000000	3.4500000
7	-25.6784709	4.6000000	3.6500000
8	-29.5283923	5.2000000	4.2500000
9	-30.4930916	5.6500000	4.7000000
10	-26.9479351	6.2499999	5.3000000
11	-32.8918452	6.9999999	6.0500000
12	-33.2652771	7.4999999	6.5500000
13	-27.5813603	8.0999999	7.1499999
14	-35.3629227	9.3000000	8.3500000
15	-33.3142381	9.8499999	8.9000000
16	-36.1176085	10.6500000	9.7000000
17	-36.1871257	11.1500000	10.2000000
18	-34.2686520	11.5999999	10.6500000
19	-34.6440048	11.9999999	11.0500000
20	-36.1995406	12.4999999	11.5500000

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	0.0	0.5000000	
1	-12.9984999	0.3000000	-0.6500000
2	-17.4870453	-0.1500000	-1.1000000
3	-18.8758287	-0.6500000	-1.6000000
4	-20.3417430	-0.9500000	-1.9000000
5	-24.6396527	-1.5000000	-2.4500000
6	-26.2940965	-1.9500000	-2.9000000
7	-25.7958112	-2.5000000	-3.4500000
8	-30.0547667	-3.3000000	-4.2500000
9	-31.1425605	-3.7500000	-4.7000000
10	-29.6630654	-4.3500000	-5.3000000

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=2749T

1-21, Pass#1

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE GAIN IS 45.2987013.

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

BANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-12.7158108	0.3000000
2	-12.8724976	1.6000000
3	-16.8341303	-0.1500000
4	-17.1360111	2.0500000
5	-18.4243555	2.5500000
6	-18.5232530	-0.6500000
7	-20.5628164	7.6999999
8	-23.0474310	8.5500000
9	-23.7432332	-1.5000000
10	-24.0105276	3.4000000
11	-24.8879037	4.3500000
12	-25.1108494	-2.5000000
13	-25.5206466	3.8500000
14	-25.6071825	-1.9500000
15	-26.9224334	15.4000000
16	-27.7178550	6.1500000
17	-27.7554407	6.9000000
18	-27.9435573	6.6000000
19	-28.0817981	-4.2500000
20	-28.1378126	5.2000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000	
1	-12.8724976	1.6000000	0.6500000
2	-17.1360111	2.0500000	1.1000000
3	-18.4243555	2.5500000	1.6000000
4	-24.0105276	3.4000000	2.4500000
5	-25.5206466	3.8500000	2.9000000
6	-24.8879037	4.3500000	3.4000000
7	-28.1378126	5.2000000	4.2500000
8	-25.1108494	5.7000000	4.7500000
9	-27.7178550	6.1500000	5.2000000
10	-27.9435573	6.6000000	5.6500000
11	-27.7554407	6.9000000	5.9500000
12	-20.5628164	7.6999999	6.7499999
13	-23.0474310	8.5500000	7.6000000
14	-30.6624455	9.3499999	8.4000000
15	-34.8648167	11.1500000	10.2000000
16	-33.4099721	11.5999999	10.6500000
17	-34.0189075	11.9999999	11.0500000
18	-35.4603829	12.4999999	11.5500000
19	-35.1353903	12.9499999	12.0000000
20	-33.6322370	13.4499999	12.5000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000	
1	-12.7158108	0.3000000	-0.6500000
2	-16.8341303	-0.1500000	-1.1000000
3	-18.5232530	-0.6500000	-1.6000000
4	-23.7432332	-1.5000000	-2.4500000
5	-25.6071825	-1.9500000	-2.9000000
6	-25.1108494	-2.5000000	-3.4500000
7	-28.6913977	-3.2500000	-4.2000000
8	-29.2392578	-3.8000000	-4.7500000
9	-28.0817981	-4.2500000	-5.2000000
10	-28.4134472	-4.6500000	-5.6000000
11	-28.7490869	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=2646T  
5-07, Pass#1

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE GAIN IS 49.5214362

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN (DB)	ANGLE (DEG)
MAIN	49.5214362	0.9500000
1	-12.9568996	1.6000000
2	-13.0397501	0.3000000
3	-17.3801556	2.0500000
4	-17.4908304	-0.1500000
5	-18.6865082	2.5500000
6	-18.8793907	-0.6500000
7	-20.1321135	2.8500000
8	-20.3429904	-0.9500000
9	-24.3437490	3.4000000
10	-24.6498561	-1.5000000
11	-25.3926921	4.4000000
12	-25.7913504	-2.4500000
13	-25.9707303	3.8500000
14	-26.3281002	-1.9500000
15	-26.3384156	2.7500000
16	-26.8836168	15.4000000
17	-27.5755457	6.0999999
18	-28.9474473	6.2499999
19	-29.5227213	5.2000000
20	-29.5592103	14.9499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	49.5214362	0.9500000	
1	-12.9568996	1.6000000	0.6500000
2	-17.3801556	2.0500000	1.1000000
3	-18.6865082	2.5500000	1.6000000
4	-17.4908304	2.8500000	1.9000000
5	-20.1321135	3.4000000	2.4500000
6	-18.8793907	3.8500000	2.9000000
7	-25.3926921	4.4000000	3.4500000
8	-24.3437490	5.2000000	4.2500000
9	-25.7913504	5.6500000	4.7000000
10	-24.6498561	6.0999999	5.3000000
11	-25.9707303	6.2499999	6.0500000
12	-26.3281002	7.2499999	6.3000000
13	-26.3384156	7.4499999	6.4999999
14	-27.5755457	8.0999999	7.1499999
15	-28.9474473	8.8000000	7.8500000
16	-33.1375354	9.2500000	8.3000000
17	-33.2897491	9.8000000	8.8500000
18	-33.5959430	10.7999999	9.1500000
19	-36.1279292	10.6500000	9.7000000
20	-36.1445169	11.1500000	10.2000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	49.5214362	0.9500000	
1	-13.0397501	0.3000000	-0.6500000
2	-17.4908304	-0.1500000	-1.1000000
3	-18.8793907	-0.6500000	-1.6000000
4	-20.3429904	-0.9500000	-1.9000000
5	-24.6498561	-1.5000000	-2.4500000
6	-24.3437490	-1.9500000	-2.9000000
7	-25.7913504	-2.4500000	-3.4000000
8	-26.3281002	-2.7500000	-3.7000000
9	-26.3384156	-3.3000000	-4.2500000
10	-27.5755457	-3.7500000	-4.7000000
11	-29.5227213	-4.3000000	-5.2000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=8415T  
5-14, Pass#1

THE MAIN LOBE GAIN IS 45.4896536

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-12.9713039	1.6000000
2	-13.0046864	0.3000000
3	-17.0437965	2.0500000
4	-17.3399668	-0.1500000
5	-18.5267324	2.5500000
6	-18.7592630	-0.6500000
7	-20.0128393	2.8500000
8	-20.2436352	-0.9500000
9	-20.5804663	7.6999999
10	-23.4643621	6.5500000
11	-24.0202947	3.4000000
12	-24.1664543	-1.5000000
13	-24.9504261	4.3500000
14	-25.4805346	-2.4500000
15	-25.4995626	3.8500000
16	-25.5504098	4.6000000
17	-26.0685382	-1.9500000
18	-26.2704387	-2.7000000
19	-26.9396166	15.4000000
20	-27.8010349	6.1500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000	
1	-12.9713039	1.6000000	0.6500000
2	-17.0437965	2.0500000	1.1000000
3	-18.5267324	2.5500000	1.6000000
4	-20.0128393	2.8500000	1.9000000
5	-24.0202947	3.4000000	2.4500000
6	-25.4955626	3.8500000	2.9000000
7	-24.9504261	4.3500000	3.4000000
8	-25.5504098	4.6000000	3.6500000
9	-28.2651639	5.2100000	4.2500000
10	-28.9564364	5.7000000	4.7500000
11	-27.8010349	6.1500000	5.2000000
12	-27.8671651	6.6000000	5.6500000
13	-27.8619738	6.8500000	5.9000000
14	-20.5804663	7.6999999	6.7499999
15	-23.4643621	8.5500000	7.6000000
16	-30.7614455	9.3499999	8.4000000
17	-30.7693696	9.4499999	8.5000000
18	-34.7207232	10.5999999	9.6500000
19	-35.4199217	11.1500000	10.2000000
20	-34.0019740	11.5999999	10.6500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000	
1	-13.0046864	0.3000000	-0.6500000
2	-17.3399668	-0.1500000	-1.1000000
3	-18.7592630	-0.6500000	-1.6000000
4	-20.2436352	-0.9500000	-1.9000000
5	-24.1664543	-1.5000000	-2.4500000
6	-26.0685382	-1.9500000	-2.9000000
7	-25.4805346	-2.4500000	-3.4000000
8	-26.2704387	-2.7000000	-3.6500000
9	-29.0719711	-3.2500000	-4.2000000
10	-29.8747983	-3.8000000	-4.7500000
11	-28.4191017	-4.2500000	-5.2000000
12	-28.6790014	-4.7000000	-5.6500000
13	-28.7142353	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • ANTENNA LOBE SCANNER • • •

SNUMB=2661T  
5-07, Pass#1

THE MAIN LOBE GAIN IS 45.67652A

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN (DB)	ANGLE (DEG)
MAIN	0.0	0.9500000
1	-13.4261178	1.6000000
2	-13.5781263	0.3000000
3	-17.9251307	2.0500000
4	-18.038373	-0.1500000
5	-19.055248	2.5500000
6	-19.2533379	-0.6500000
7	-20.5251389	2.8500000
8	-20.7369347	-0.9500000
9	-25.0147522	3.4000000
10	-25.3142965	-1.5000000
11	-25.8181275	4.4000000
12	-25.2222805	-2.4500000
13	-26.3256531	4.6000000
14	-26.6527014	3.8500000
15	-26.7587833	-2.7500000
16	-26.9256537	15.4000000
17	-27.0198698	-1.9500000
18	-27.7647924	8.0999999
19	-29.3778172	6.2499999
20	-29.7655668	14.9499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **	1.4000000	
1	-13.4261178	1.6000000	0.6500000
2	-17.9251307	2.0500000	1.1000000
3	-19.055248	2.5500000	1.6000000
4	-20.5251389	2.8500000	1.9000000
5	-25.0147522	3.4000000	2.4500000
6	-26.652714	3.8500000	2.9000000
7	-25.8181275	4.4000000	3.4500000
8	-26.3256531	4.6000000	3.6500000
9	-35.2939854	5.2000000	4.2500000
10	-31.3024397	5.6500000	4.7000000
11	-29.3778172	6.2499999	5.3000000
12	-33.7921876	6.9999999	6.0500000
13	-34.1263981	7.4499999	6.4999999
14	-27.7647924	8.0999999	7.1499999
15	-35.351331	8.8000000	7.8500000
16	-36.2700834	9.2500000	8.3000001
17	-33.7737923	9.8000000	8.8500000
18	-34.0909605	10.0999999	9.1500000
19	-36.9668417	10.6500000	9.7000000
20	-36.9427652	11.1500000	10.2000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **	0.5000000	
1	-13.5081263	0.3000000	-0.6500000
2	-18.038373	-0.1500000	-1.1000000
3	-19.2533379	-0.6500000	-1.6000000
4	-20.7369347	-0.9500000	-1.9000000
5	-25.3042965	-1.5000000	-2.4500000
6	-27.0198698	-1.9500000	-2.9000000
7	-26.2222805	-2.4500000	-3.4000000
8	-26.7587833	-2.7500000	-3.7000000
9	-38.8093576	-3.3000000	-4.2500000
10	-31.9397650	-3.7500000	-4.7000000
11	-30.0744896	-4.3000000	-5.2500000

NO FURTHER SIDE LOBES ON THIS SIDE



• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7596T  
5-06, Pass#1

THE MAIN LOBE GAIN IS 45.6725545

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-13.451104	1.6000000
2	-13.4999638	0.3000000
3	-17.8695063	2.0500000
4	-17.9991722	-0.1500000
5	-19.0473843	2.5500000
6	-19.2402554	-0.6500000
7	-20.510842	2.6500000
8	-20.7308568	-0.9500000
9	-24.9879484	3.4000000
10	-25.2939482	-1.5000000
11	-25.8104029	4.4000000
12	-26.2153692	-2.4500000
13	-26.3183498	4.6000000
14	-26.638281	3.8500000
15	-26.7558813	-2.7500000
16	-26.9274454	15.4000000
17	-27.079184	-1.9500000
18	-27.7495937	8.0999999
19	-29.3704615	6.2499999
20	-29.7635841	14.9499999

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000		
1	-13.451104	1.6000000	0.6500000	
2	-17.869563	2.0500000	1.1000000	
3	-19.0473843	2.5500000	1.6000000	
4	-20.510842	2.6500000	1.9000000	
5	-24.9879484	3.4000000	2.4500000	
6	-26.638281	3.6500000	2.9000000	
7	-25.810429	4.4000000	3.4500000	
8	-26.3183498	4.6000000	3.6500000	
9	-30.2783699	5.2000000	4.2500000	
10	-31.2865917	5.6500000	4.7000000	
11	-29.3704615	6.2499999	5.3000000	
12	-33.7483969	6.9999999	6.0500000	
13	-33.9766788	7.4499999	6.4999999	
14	-27.7495937	8.0999999	7.1499999	
15	-35.2240896	8.8000000	7.8500000	
16	-36.2271452	9.2500000	8.3000001	
17	-33.7638931	9.8000000	8.8500000	
18	-34.0825710	10.0999999	9.1500000	
19	-36.9488945	10.6500000	9.7000000	
20	-36.935458	11.1500000	10.2000000	

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000		
1	-13.4999638	0.3000000	-0.6500000	
2	-17.9991722	-0.1500000	-1.1000000	
3	-19.242554	-0.6500000	-1.6000000	
4	-20.738588	-0.9500000	-1.9000000	
5	-25.2939482	-1.5000000	-2.4500000	
6	-27.0779184	-1.9500000	-2.9000000	
7	-26.2153692	-2.4500000	-3.4000000	
8	-26.7558813	-2.7500000	-3.7000000	
9	-30.7954521	-3.3000000	-4.2500000	
10	-31.9225893	-3.7500000	-4.7000000	
11	-31.673466	-4.3000000	-5.2500000	

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7478T  
5-16, Pass#1

THE MAIN LOBE GAIN IS 27.511397

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-2.4179893	15.4999999
2	-2.5291042	31.1499999
3	-5.8764405	30.1999998
4	-7.1596160	32.1999998
5	-12.9648924	1.6000000
6	-12.9734688	0.3000000
7	-16.1952119	14.4000000
8	-16.2600083	16.6499999
9	-17.298 251	29.3999999
10	-17.3439717	-0.1500000
11	-17.3596315	2.0500000
12	-17.4665236	33.0000000
13	-18.616941	2.5500000
14	-18.6192567	-0.6500000
15	-18.7315006	13.9000000
16	-18.8224468	17.1499999
17	-19.7478809	28.9499998
18	-19.9815393	-0.9500000
19	-19.9922085	2.8500000
20	-20.1955036	13.4499999

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4000000	
1	-12.9648924	1.6000000	0.6500000
2	-17.3596315	2.0500000	1.1000000
3	-18.6015941	2.5500000	1.6000000
4	-19.9922 85	2.8500000	1.9000000
5	-24.0703120	3.4000000	2.4500000
6	-25.5558171	3.8500000	2.9000000
7	-24.7677870	4.4000000	3.4500000
8	-25.1787148	4.6500000	3.7000000
9	-28.5097733	5.2000000	4.2500000
10	-29.2299409	5.6500000	4.7000000
11	-27.2774711	6.2499999	5.3000000
12	-30.6201596	6.9999999	6.0500000
13	-30.5573592	7.4499999	6.4999999
14	-24.2447600	8.1500000	7.2000000
15	-30.4030499	8.8000000	7.8500000
16	-30.5818605	9.3499999	8.4000000
17	-27.7503753	9.8499999	8.9000000
18	-27.7833452	9.9499999	9.0000000
19	-27.8167055	10.0999999	9.1500000
20	-29.2776437	10.6999999	9.7500000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.5000000	
1	-12.9734688	0.3000000	-0.6500000
2	-17.3439717	-0.1500000	-1.1000000
3	-18.6092567	-0.6500000	-1.6000000
4	-19.9815393	-0.9500000	-1.9000000
5	-24.0859356	-1.5000000	-2.4500000
6	-25.5649886	-1.9500000	-2.9000000
7	-24.7680664	-2.4500000	-3.4000000
8	-25.1424208	-2.7500000	-3.7000000
9	-28.4824642	-3.3000000	-4.2500000
10	-29.2396212	-3.7500000	-4.7000000
11	-27.2838240	-4.3500000	-5.3000000

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=8522T  
5-08, Pass#1

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 27.29 -177

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN (DB)	ANGLE (DEG)
MAIN	0.0	0.9500000
1	-2.4162817	15.4999999
2	-2.5144982	31.1499999
3	-5.8353839	30.1999998
4	-7.1772488	32.2500000
5	-12.7863779	1.6000000
6	-12.8343921	0.3000000
7	-15.8044491	14.4000000
8	-15.9701447	16.6499999
9	-16.8664536	-0.1500000
10	-16.9796360	2.0500000
11	-17.127508	29.3999999
12	-17.293317	33.0499997
13	-17.7106066	7.6999999
14	-18.2415919	-0.6500000
15	-18.2793303	23.0500000
16	-18.3392048	2.5500000
17	-18.3957810	13.9000000
18	-18.4994216	17.1499999
19	-19.2927209	22.3000000
20	-19.296777	28.9499998

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **		1.4000000	
1	-12.7863779	1.6000000	0.6500000	
2	-16.9095360	2.0500000	1.1000000	
3	-18.335248	2.5500000	1.6000000	
4	-19.407487	2.6500000	1.9000000	
5	-23.3069139	3.4000000	2.4500000	
6	-24.6850409	3.6900000	2.9000000	
7	-24.0437498	4.4000000	3.4500000	
8	-24.3697534	4.6500000	3.7000000	
9	-27.0157647	5.2000000	4.2500000	
10	-27.3168278	5.7000000	4.7500000	
11	-25.6818617	6.1500000	5.2000000	
12	-25.5513377	6.6000000	5.6500000	
13	-25.5773382	6.9499999	5.9999999	
14	-17.7106066	7.6999999	6.7499999	
15	-19.4323225	8.5500000	7.6000000	
16	-25.5333424	9.4000000	8.4500000	
17	-26.397524	10.1500000	9.2000000	
18	-27.4084406	10.6500000	9.7000000	
19	-27.1784940	11.1500000	10.2000000	
20	-25.6932465	11.6500000	10.7000000	

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **		0.5000000	
1	-12.8343921	0.3000000	-0.6500000	
2	-16.8664536	-0.1500000	-1.1000000	
3	-18.2415919	-0.6500000	-1.6000000	
4	-23.6360315	-1.5000000	-2.4500000	
5	-24.9736385	-1.9500000	-2.9000000	
6	-24.2316478	-2.4500000	-3.4000000	
7	-24.8684158	-2.7500000	-3.7000000	
8	-27.0044990	-3.3000000	-4.2500000	
9	-27.2272577	-3.8000000	-4.7500000	
10	-26.089544	-4.2500000	-5.2000000	

NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=3575T  
5-09, Pass#1

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE GAIN IS 27.2214271

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	27.2214271	1.0000000
1	-2.4192479	15.5500000
2	-3.5127292	31.2499999
3	-5.8351240	30.2499998
4	-7.1651194	32.2499997
5	-12.6486333	1.6500000
6	-12.9831276	0.3500000
7	-16.0374620	16.6999998
8	-16.0726223	14.4499999
9	-17.0177989	33.1999999
10	-17.1475930	2.1000000
11	-17.1505623	29.4999998
12	-17.2802095	-0.1000000
13	-17.5143529	2.6000000
14	-17.6651447	-0.6000000
15	-17.6736463	7.3500000
16	-19.1487446	17.1999998
17	-19.1643774	13.9499999
18	-19.1103326	29.0500000
19	-19.3791125	22.5500000
20	-19.4695767	33.5499997

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (AFTER) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	27.2214271	1.4500000	0.6500000
1	-12.2485333	1.6500000	1.1000000
2	-17.1475930	2.1000000	1.6000000
3	-17.5193529	2.6000000	2.4500000
4	-23.3497801	3.4500000	2.9000000
5	-24.1722125	3.9000000	3.4000000
6	-23.5079641	4.4000000	4.3000000
7	-26.7673359	5.3000000	4.7000000
8	-25.2342556	5.7000000	5.2499999
9	-25.7367504	6.2499999	5.4999999
10	-25.1559401	6.4999999	6.3500000
11	-17.6737563	7.3500000	7.1500000
12	-23.3514524	8.1500000	8.0500000
13	-19.9737152	9.0500000	8.9000000
14	-26.2505936	9.9000000	9.3000000
15	-26.2572300	10.3000000	9.7500000
16	-25.3300929	10.7500000	10.1500000
17	-24.5933793	11.1500000	10.7499999
18	-24.6129554	11.7499999	11.3500000
19	-23.9721283	12.0500000	11.5500000
20	-24.5528493	12.5500000	

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BEFORE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	27.2214271	0.5000000	-0.6500000
1	-12.9831276	0.3500000	-1.1000000
2	-17.2447295	-0.1000000	-1.6000000
3	-17.6681447	-0.6000000	-2.4500000
4	-23.6466649	-1.4500000	-2.9000000
5	-24.6189637	-1.9000000	-3.4000000
6	-25.2191415	-2.4000000	-4.3000000
7	-24.7723327	-3.7000000	-4.7000000
8	-25.477872	-4.2500000	-5.2500000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=3575T  
5-09, Pass#5

THE MAIN LOBE GAIN IS 27.283752

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	4.9999999
1	-2.7421927	19.6499999
2	-3.7377357	19.4499998
3	-10.3437749	20.4499998
4	-12.7466478	5.6500000
5	-12.9298654	4.3500000
6	-14.6797900	16.7500000
7	-14.7679067	34.4499998
8	-16.7721853	7.9999999
9	-16.9291110	21.0500000
10	-17.1822166	3.9000000
11	-17.2293844	6.1000000
12	-18.3126785	2.0000000
13	-18.3212624	18.2500000
14	-18.3383527	6.6000000
15	-18.5134997	3.4000000
16	-18.9931365	22.5999999
17	-19.0097526	21.5500000
18	-19.4007225	17.7500000
19	-19.4139371	33.3499999
20	-19.5624905	23.2500000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	5.4500000		
1	-12.7466478	5.6500000	0.6500000	
2	-17.2293844	6.1000000	1.1000000	
3	-18.3383527	6.6000000	1.6000000	
4	-19.662132	6.9000000	1.9000000	
5	-22.3354607	7.4499999	2.4500000	
6	-16.7721853	7.9999999	3.0000000	
7	-23.5872664	6.6999999	3.7000000	
8	-26.7357328	9.3000000	4.3000000	
9	-27.2913327	9.6999999	4.7000000	
10	-23.9398670	10.3499999	5.3500000	
11	-23.1265554	11.0999999	6.1000000	
12	-23.6911236	12.2499999	7.2499999	
13	-24.4839196	13.4000000	8.4000001	
14	-25.0424733	14.0999999	9.1000000	
15	-27.7037826	14.9999999	10.0000000	
16	-26.2326169	15.4999999	10.5000000	
17	-20.0784783	16.4499998	11.4499999	
18	-21.6340632	17.3499999	12.3500000	
19	-19.4077225	17.7500000	12.7500001	
20	-18.3212624	18.2500000	13.2500001	

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	4.5500000		
1	-12.9298654	4.3500000	-0.6500000	
2	-17.1822166	3.9000000	-1.1000000	
3	-18.5134997	3.4000000	-1.6000000	
4	-19.6117371	3.1000000	-1.9000000	
5	-22.7326317	2.5500000	-2.4500000	
6	-18.3126785	2.0000000	-3.0000000	
7	-24.025478	1.3000000	-3.7000000	
8	-27.3179355	0.8000000	-4.1999999	
9	-27.6218247	0.3000000	-4.6999999	
10	-24.4924466	-0.2500000	-5.2499999	
11	-28.9115783	-1.0500000	-6.0500000	
12	-23.692143	-2.1500000	-7.1499999	
13	-23.6977282	-3.3000000	-8.3000000	
14	-24.443272	-3.9500000	-8.9499999	
15	-27.1894817	-4.8000000	-9.8000000	

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=3575T  
5-09, Pass#4

• • • ANTENNA LOBE SCANNER • • •

THE MAIN LOBE GAIN IS 27.2861724

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN	REL. GAIN ( DB )	REL. ANGLE ( DEG )
1	-2.6253424	18.7500000
2	-2.7340664	15.9000000
3	-4.1695263	34.0000000
4	-12.832931	4.6500000
5	-13.6276029	3.3500000
6	-15.1986747	17.6499999
7	-15.6729248	33.1999999
8	-16.4481376	0.6500000
9	-16.6627817	19.9499999
10	-17.0129795	5.1000000
11	-17.1572070	2.9000000
12	-18.5992222	7.3500000
13	-18.2722547	15.1999999
14	-18.3286746	17.1499999
15	-18.4333196	5.6000000
16	-18.4877439	12.7500000
17	-18.9706472	30.6000000
18	-18.5742248	2.4000000
19	-18.9611697	20.4499999
20	-19.5999404	16.6999999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ARROW) MAIN LOBE  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN LOBE	REL. GAIN ( DB )	REL. ANGLE ( DEG )
1	-12.0038931	4.6500000
2	-17.1297795	5.1000000
3	-18.4333194	5.6000000
4	-19.7097674	5.9000000
5	-23.2479673	6.4499999
6	-23.0992272	7.3500000
7	-24.9042106	8.3000000
8	-26.1765575	9.4000000
9	-28.7235847	10.0000000
10	-23.0952777	11.2499999
11	-23.1872427	11.6500000
12	-25.6287196	12.9999999
13	-25.5656156	14.0500000
14	-18.2192547	15.1999999
15	-22.2341853	16.2500000
16	-19.5999996	16.6999999
17	-18.3285946	17.1499999
18	-15.1986747	17.6499999
19	-2.6253424	18.7500000
20	-16.6627617	19.9499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (ARROW) MAIN LOBE  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN LOBE	REL. GAIN ( DB )	REL. ANGLE ( DEG )
1	-13.0275429	3.3500000
2	-17.1572070	2.9000000
3	-18.5992248	2.4000000
4	-19.5986747	2.1000000
5	-23.4594844	1.5500000
6	-16.4481376	0.6500000
7	-24.4724223	-0.3000000
8	-25.6291434	-1.4000000
9	-28.7234956	-2.0500000
10	-27.1566220	-2.7000000
11	-28.1243559	-3.1000000
12	-26.2156134	-4.9000000

NO FURTHER SIDE-LOBES AT THIS SITE



SNUMB-3575T  
5-09, Pass#3

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 27.2667446

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN (DB)	ANGLE (DEG)
MAIN	0.0	3.0000000
1	-2.513 277	17.6999999
2	-2.4074615	33.7500000
3	-4.857899	32.7500000
4	-3.7522545	34.2499999
5	-12.8119221	2.3500000
6	-12.8413129	3.6500000
7	-15.9701443	16.5500000
8	-16.2541118	31.7499999
9	-16.5096825	18.6499999
10	-17.111351	4.1000000
11	-17.2214642	7.6999999
12	-17.3792605	1.9000000
13	-18.4261961	4.6000000
14	-18.5294156	-1.7000000
15	-18.5484853	1.4000000
16	-18.6286335	16.0500000
17	-18.8374228	19.3499999
18	-19.0806193	31.4499999
19	-19.277 119	22.2500000
20	-19.3400926	12.7499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. MAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **	3.4500000	
1	-12.6413129	3.6500000	0.6500000
2	-17.1010351	4.1000000	1.1000000
3	-18.4261961	4.6000000	1.6000000
4	-19.7370558	4.9000000	1.9000000
5	-23.4965569	5.4500000	2.4500000
6	-24.6274210	5.9000000	2.9000000
7	-23.9365197	6.4499999	3.4500000
8	-24.2567201	6.6500000	3.6500000
9	-17.2214642	7.6999999	4.7000000
10	-28.4400587	9.0500000	6.0500000
11	-28.4193501	9.4499999	6.4500000
12	-28.4574442	9.5500000	6.5500000
13	-23.6342910	10.1999999	7.2000000
14	-29.0391301	10.9000000	7.9000000
15	-29.0493107	11.0000000	8.0000000
16	-19.3400526	12.7499999	9.7499999
17	-24.3263130	13.8000000	10.8000000
18	-24.8927226	14.1999999	11.1999999
19	-24.9080659	14.6999999	11.6999999
20	-22.9940531	15.1999999	12.1999999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
MAIN LOBE	** NULL **	2.5500000	
1	-12.8119221	2.3500000	-0.6500000
2	-17.3792605	1.9000000	-1.1000000
3	-18.5484853	1.4000000	-1.6000000
4	-23.6179507	0.5500000	-2.4500000
5	-25.1637340	0.1000000	-2.9000000
6	-24.1261204	-0.4500000	-3.4500000
7	-24.3279558	-0.6500000	-3.6500000
8	-18.5294156	-1.7000000	-4.7000000
9	-28.6372848	-3.0500000	-6.0500000
10	-29.042259	-3.5000000	-6.4999999
11	-29.0599168	-3.6000000	-6.6000000
12	-23.6240211	-4.1000000	-7.1499999
13	-28.4467164	-4.9000000	-7.8999999

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=3575T  
5-09, Pass#2

\*\*\*\*\* ANTENNA LOSS SCANNER \*\*\*\*\*

THE MAIN LOBE GAIN IS 27.29 DB

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN (DB) ANGLE (DEG)

RANK	REL. GAIN (DB)	ANGLE (DEG)
1	-2.4603772	16.5999999
2	-2.5725873	32.5000000
3	-5.2641076	31.4999999
4	-7.7905817	33.5499997
5	-12.8614954	1.3500000
6	-12.9326366	2.6500000
7	-15.0344773	0.3500000
8	-15.3737724	15.4999999
9	-15.6707854	3.6500000
10	-15.9295179	17.8000000
11	-15.9822423	30.6999998
12	-16.4211345	14.9499999
13	-16.7111540	14.3499996
14	-16.9257755	30.3499999
15	-16.9973479	0.9000000
16	-17.2023172	18.3000000
17	-17.2302755	3.1000000
18	-17.4722281	14.6500000
19	-18.4946463	29.5999999
20	-21.1755479	-1.4000000

MAIN LOBE GAIN AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN (DB) ANGLE (DEG)

RANK	REL. GAIN (DB)	ANGLE (DEG)
1	-12.9353368	2.6500000
2	-17.2382795	3.1000000
3	-15.6707554	3.6500000
4	-22.8539558	4.4500000
5	-24.3914571	4.9000000
6	-21.4019121	5.4000000
7	-25.4490123	6.2499999
8	-24.9463205	7.1500000
9	-23.1790326	7.9999999
10	-23.7740606	9.1999999
11	-27.8455159	10.4000000
12	-25.1140313	11.3000000
13	-26.7080275	12.3000000
14	-22.3294779	13.0999999
15	-24.0045073	13.5999999
16	-17.4722281	14.6500000
17	-16.4711345	14.9499999
18	-15.3737736	15.4999999
19	-2.4603772	16.5999999
20	-15.8295179	17.8000000

MAIN LOBE GAIN AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN (DB) ANGLE (DEG)

RANK	REL. GAIN (DB)	ANGLE (DEG)
1	-12.5814588	1.3500000
2	-15.9973479	0.9000000
3	-15.0344773	0.3500000
4	-23.4712763	-0.4000000
5	-25.4490123	-0.9000000
6	-21.1755479	-1.4000000
7	-24.7045073	-2.2500000
8	-24.6050146	-3.1500000
9	-27.5449387	-4.0500000

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=8712T  
5-08, Pass#1

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 96.782654

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-26.0666218	1.6000000
2	-26.1738284	0.3000000
3	-34.2516775	2.0000000
4	-34.9482164	-0.1000000
5	-40.8091312	2.5000000
6	-41.3501396	-0.6000000
7	-45.1561392	2.9500000
8	-45.7956123	-1.0500000
9	-48.8303165	3.4000000
10	-48.8942461	-1.5000000
11	-49.8733263	7.6999999
12	-51.6463060	19.4000000
13	-51.6609583	3.8500000
14	-52.8736649	-1.9500000
15	-53.6742058	4.3000000
16	-54.2353220	8.5500000
17	-54.6396017	14.9999999
18	-54.6734762	-2.4000000
19	-56.1661337	4.7499999
20	-56.7862787	5.1500000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4500000	
1	-26.0666218	1.6000000	0.6500000
2	-34.2516775	2.0000000	1.0500000
3	-40.8091312	2.5000000	1.5500000
4	-45.1561392	2.9500000	2.0000000
5	-48.8303165	3.4000000	2.4500000
6	-51.6609583	3.8500000	2.9000000
7	-53.6742058	4.3000000	3.3500000
8	-54.6396017	4.7499999	3.8000000
9	-56.1661337	5.1500000	4.2000000
10	-56.7862787	5.9000000	4.9500000
11	-57.1964912	6.8000000	5.6500000
12	-49.8733263	7.6999999	6.7499999
13	-54.2353220	8.5500000	7.6000000
14	-63.5139732	9.3499999	8.4000000
15	-67.8194142	10.2500000	9.3000001
16	-69.3636065	10.5999999	9.6500000
17	-70.9153433	11.1500000	10.2000000
18	-71.8954372	11.5500000	10.6000000
19	-71.9993391	12.0500000	11.1000000
20	-72.2177620	12.4999999	11.5500000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.4500000	
1	-26.1738284	0.3000000	-0.6500000
2	-34.9482164	-0.1000000	-1.0500000
3	-41.3501396	-0.6000000	-1.5500000
4	-45.7956123	-1.0500000	-2.0000000
5	-48.8942461	-1.5000000	-2.4500000
6	-52.8736649	-1.9500000	-2.9000000
7	-54.6734762	-2.4000000	-3.3500000
8	-56.1294418	-2.8500000	-3.8000000
9	-58.4149742	-3.2500000	-4.2000000
10	-59.5294666	-4.0500000	-5.0000000
11	-58.7815491	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE



1950-1951

SNUMB=8430T  
06-19, Pass#2

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THE MAIN LOPE OF THE

LOCATION AND RELATIVE SIZE OF HIGHEST 20-50-100

WAVE

REL. SIZE

ANGLE

(DEG)

WAVE	REL. SIZE	ANGLE (DEG)
1	0.07-7.19	1.55
2	0.07-7.19	1.55
3	0.07-7.19	1.55
4	0.07-7.19	1.55
5	0.07-7.19	1.55
6	0.07-7.19	1.55
7	0.07-7.19	1.55
8	0.07-7.19	1.55
9	0.07-7.19	1.55
10	0.07-7.19	1.55
11	0.07-7.19	1.55
12	0.07-7.19	1.55
13	0.07-7.19	1.55
14	0.07-7.19	1.55
15	0.07-7.19	1.55
16	0.07-7.19	1.55
17	0.07-7.19	1.55
18	0.07-7.19	1.55
19	0.07-7.19	1.55
20	0.07-7.19	1.55

REL. SIZE

ANGLE

(DEG)

WAVE	REL. SIZE	ANGLE (DEG)
1	0.07-7.19	1.55
2	0.07-7.19	1.55
3	0.07-7.19	1.55
4	0.07-7.19	1.55
5	0.07-7.19	1.55
6	0.07-7.19	1.55
7	0.07-7.19	1.55
8	0.07-7.19	1.55
9	0.07-7.19	1.55
10	0.07-7.19	1.55
11	0.07-7.19	1.55
12	0.07-7.19	1.55
13	0.07-7.19	1.55
14	0.07-7.19	1.55
15	0.07-7.19	1.55
16	0.07-7.19	1.55
17	0.07-7.19	1.55
18	0.07-7.19	1.55
19	0.07-7.19	1.55
20	0.07-7.19	1.55

REL. SIZE

ANGLE

(DEG)

WAVE	REL. SIZE	ANGLE (DEG)
1	0.07-7.19	1.55
2	0.07-7.19	1.55
3	0.07-7.19	1.55
4	0.07-7.19	1.55
5	0.07-7.19	1.55
6	0.07-7.19	1.55
7	0.07-7.19	1.55
8	0.07-7.19	1.55
9	0.07-7.19	1.55
10	0.07-7.19	1.55
11	0.07-7.19	1.55
12	0.07-7.19	1.55
13	0.07-7.19	1.55
14	0.07-7.19	1.55
15	0.07-7.19	1.55
16	0.07-7.19	1.55
17	0.07-7.19	1.55
18	0.07-7.19	1.55
19	0.07-7.19	1.55
20	0.07-7.19	1.55

SNUMB=3732T  
5-29.Pass#1

• • • • ANTENNA LOBE SCANNER • • • •

THE MAIN LOBE GAIN IS 91.5960197

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	1.0000000
1	+26.0382833	1.6500000
2	+26.1622267	0.3500000
3	+34.9811382	2.1000000
4	+35.1812410	-0.1000000
5	+36.2163143	-0.6000000
6	+36.4496956	2.6000000
7	+48.4974327	3.4500000
8	+48.7085667	7.3500000
9	+49.3990908	4.4000000
10	+49.5082874	-1.4500000
11	+50.2500629	3.9000000
12	+50.2763987	-2.4000000
13	+50.8110867	-1.9500000
14	+52.6775875	15.4499999
15	+53.8558178	5.6500000
16	+54.8858557	8.9499999
17	+54.9535942	-3.6500000
18	+55.3048296	8.1500000
19	+55.7013588	15.0500000
20	+57.0573597	6.2000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	0.0	1.5000000	
1	-26.0382833	1.6500000	0.6500000
2	-34.9811382	2.1000000	1.1000000
3	-36.4496956	2.6000000	1.6000000
4	-48.4974327	3.4500000	2.4500000
5	-50.2500629	3.9000000	2.9000000
6	-49.3990908	4.4000000	3.4000000
7	-57.4847221	5.2499999	4.2499999
8	-53.8558178	5.6500000	4.6500000
9	-57.0573597	6.2000000	5.2000000
10	-48.7085667	7.3500000	6.3500000
11	-55.3048296	8.1500000	7.1500000
12	-54.8858557	8.9499999	7.9499999
13	-66.1152020	9.8499999	8.8499999
14	-65.8678863	10.1999999	9.1999999
15	-65.8178797	10.6500000	9.6500000
16	-68.2848251	11.6999999	10.6999999
17	-67.8466425	11.9999999	10.9999999
18	-70.7128019	12.3499999	11.3499999
19	-72.0573369	13.0500000	12.0500000
20	-67.8950653	13.4999999	12.4999999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	0.0	0.5000000	
1	-26.1622267	0.3500000	-0.6500000
2	-35.1812410	-0.1000000	-1.1000000
3	-36.2163143	-0.6000000	-1.6000000
4	-49.5082874	-1.4500000	-2.4500000
5	-50.8110867	-1.9500000	-2.9500000
6	-50.2763987	-2.4000000	-3.4000000
7	-58.8643456	-3.2500000	-4.2500000
8	-54.9535942	-3.6500000	-4.6500000
9	-58.6245213	-4.2000000	-5.2000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=3732T

5-29, Pass#2

THE MAIN LOBE GAIN IS 91.0984230

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	2.0000000
1	+13.5852003	0.3500000
2	-16.9246168	1.0000000
3	-17.7893343	1.3500000
4	+25.3000479	2.6500000
5	+26.7220535	3.7000000
6	-32.3995099	-1.3500000
7	-33.7192883	3.1000000
8	-37.1383023	-0.3000000
9	-37.5718284	5.3500000
10	+41.6713243	4.4999999
11	+41.9627337	-3.0000000
12	+44.3799043	7.0500000
13	+45.2296977	-2.2500000
14	+46.7913661	6.2499999
15	+49.3744941	-3.9000000
16	-49.6418691	7.9499999
17	+50.0995593	+4.7000000
18	-50.6817908	8.7500000
19	-51.6629291	30.3999999
20	-51.7154050	32.4499998

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	2.5000000	
1	-25.3000479	2.6500000	0.6500000
2	-33.7192883	3.1000000	1.1000000
3	+26.7220535	3.7000000	1.7000000
4	-41.6713243	4.4999999	2.5000000
5	-37.5718284	5.3500000	3.3500000
6	-46.7913661	6.2499999	4.2500000
7	-44.3799043	7.0500000	5.0500000
8	-49.6418691	7.9499999	5.9500000
9	-50.6817908	8.7500000	6.7500001
10	-52.2115121	9.5999999	7.6000000
11	-55.8265767	10.4000000	8.4000000
12	-53.6677060	11.3000000	9.3000000
13	-61.0627646	12.0500000	10.0500000
14	-54.8582520	13.0500000	11.0500000
15	-55.5122752	14.4000000	12.4000000
16	-51.9100146	14.8000000	12.8000000
17	-55.8025813	15.1999999	13.1999999
18	-70.9027805	16.3499999	14.3499999
19	-68.2287655	16.8000000	14.8000000
20	-71.4153032	17.3000000	15.3000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.5000000	
1	-17.7893343	1.3500000	-0.6500000
2	-16.9246168	1.0000000	-1.0000000
3	+13.5852003	0.3500000	-1.6500000
4	-37.1383023	-0.3000000	-2.3000000
5	-32.3995099	-1.3500000	-3.3500000
6	-45.2296977	-2.2500000	-4.2499999
7	-41.9627337	-3.0000000	-4.9999999
8	-49.3744941	-3.9000000	-5.9000000
9	-50.0995593	-4.7000000	-6.6999999

NO FURTHER SIDE LOBES ON THIS SIDE



\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=3765T

2-19, Pass#1

THE MAIN LOBE GAIN IS 91.4039421

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
 BANK REL. GAIN ANGLE  
 ( DB ) ( DEG )

BANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-25.4287643	0.3000000
2	-25.4585829	1.5500000
3	-34.2078018	2.0500000
4	-37.3320942	2.5500000
5	-37.6329222	-0.6500000
6	-47.7754259	-1.5000000
7	-48.2605524	3.4000000
8	-49.6163158	7.6999999
9	-50.4163465	4.3500000
10	-50.9727116	-2.5000000
11	-51.3043976	3.8500000
12	-51.5849543	-1.9000000
13	-53.0992708	8.5000000
14	-54.4399223	14.9999999
15	-56.2053366	5.1500000
16	-56.9352055	6.1000000
17	-56.9948692	6.8000000
18	-57.6355646	-4.2000000
19	-58.8070431	-4.8500000
20	-63.3834143	9.3499999

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.5000000	
1	-25.4585829	1.5500000	0.6000000
2	-34.2078018	2.0500000	1.1000000
3	-37.3320942	2.5500000	1.6000000
4	-48.2605524	3.4000000	2.4500000
5	-51.3043976	3.8500000	2.9000000
6	-50.4163465	4.3500000	3.4000000
7	-56.2053366	5.1500000	4.2000000
8	-56.9352055	6.1000000	5.1500000
9	-56.9948692	6.8000000	5.8500000
10	-49.6163158	7.6999999	6.7499999
11	-53.0992708	8.5000000	7.5500000
12	-63.3834143	9.3499999	8.4000000
13	-64.9997416	10.1500000	9.2000000
14	-69.4696217	11.1999999	10.2500000
15	-67.2222033	11.6500000	10.7000000
16	-68.1311665	11.9499999	11.0000000
17	-71.0880833	12.4999999	11.5500000
18	-70.2191401	12.9999999	12.0500000
19	-67.5275393	13.4499999	12.5000000
20	-67.4471712	13.8499999	12.9000000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

BANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.4000000	
1	-25.4287643	0.3000000	-0.6500000
2	-37.6329222	-0.6500000	-1.6000000
3	-47.7754259	-1.5000000	-2.4500000
4	-51.5849543	-1.9000000	-2.8500000
5	-50.9727116	-2.5000000	-3.4500000
6	-57.6355646	-4.2000000	-5.1500000
7	-58.8070431	-4.8500000	-5.8000000

NO FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7468T  
5-08, Pass#1

THE MAIN LOBE GAIN IS 91.5894156

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.9500000
1	-26.0764497	1.6000000
2	-26.0449476	0.3000000
3	-34.0612292	2.0000000
4	-34.7594805	-0.1000000
5	-37.5037069	2.5500000
6	-37.9344568	-0.6500000
7	-48.3997517	3.4000000
8	-48.510393	-1.5000000
9	-49.7387686	7.6999999
10	-51.519617	4.4000000
11	-51.3700469	3.8500000
12	-51.571467	-2.4500000
13	-51.6452904	15.4000000
14	-51.6556263	4.6000000
15	-52.474219	-1.9500000
16	-53.6536570	8.5000000
17	-54.639486	14.9999999
18	-56.4693995	5.1500000
19	-56.8878470	15.8499999
20	-57.0143080	6.8000000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.4500000	
1	-26.0764497	1.6000000	0.6500000
2	-34.0612292	2.0000000	1.0500000
3	-37.5037069	2.5500000	1.6000000
4	-48.3997517	3.4000000	2.4500000
5	-51.3700469	3.8500000	2.9000000
6	-51.571467	4.4000000	3.4500000
7	-51.6556263	4.6000000	3.6500000
8	-56.4693995	5.1500000	4.2000000
9	-56.8878470	5.7499999	4.8000000
10	-57.0143080	6.1000000	5.1500000
11	-57.0143080	6.8000000	5.8500000
12	-49.7387686	7.6999999	6.7499999
13	-53.6536570	8.5000000	7.5500000
14	-63.3744755	9.3499999	8.4000000
15	-63.4181690	9.4499999	8.5000000
16	-65.4244848	10.1500000	9.2000000
17	-68.9583289	10.5999999	9.6500000
18	-77.3941860	11.1500000	10.2000000
19	-68.0864237	11.5999999	10.6500000
20	-68.6143289	11.9499999	11.0000000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.4500000	
1	-26.0449476	0.3000000	-0.6500000
2	-34.7594805	-0.1000000	-1.0500000
3	-37.9344568	-0.6500000	-1.6000000
4	-48.510393	-1.5000000	-2.4500000
5	-52.474219	-1.9500000	-2.9000000
6	-51.571467	-2.4500000	-3.4000000
7	-58.147259	-3.2500000	-4.2000000
8	-61.2528236	-3.8000000	-4.7500000
9	-58.1119112	-4.2000000	-5.1500000
10	-58.6129650	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

SNUMB=3590T  
5-07, Pass#1

THE MAIN LOBE GAIN IS 91.4041138

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

MAIN	0.0	0.9500000
1	-25.2950783	1.5500000
2	-25.6395798	0.3000000
3	-33.6926465	2.0000000
4	-37.4550595	2.5500000
5	-37.4968895	-0.6500000
6	-47.5103965	3.4000000
7	-48.6561856	-1.5000000
8	-49.6474443	7.6999999
9	-50.1221690	4.4000000
10	-50.4528909	3.8500000
11	-51.2186065	-2.4500000
12	-51.5714927	15.4000000
13	-51.7110171	-1.9500000
14	-53.3004870	8.5000000
15	-54.5120130	14.9999999
16	-56.2282033	5.1500000
17	-56.6609893	6.1500000
18	-56.8073106	6.7499999
19	-56.8201480	15.8499999
20	-57.2254500	-3.2500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	1.5000000	
1	-25.2950783	1.5500000	0.6000000
2	-33.6926465	2.0000000	1.0500000
3	-37.4550595	2.5500000	1.6000000
4	-47.5103965	3.4000000	2.4500000
5	-50.4528909	3.8500000	2.9000000
6	-50.1221690	4.4000000	3.4500000
7	-56.2282033	5.1500000	4.2000000
8	-57.9623609	5.7000000	4.7500000
9	-56.6609893	6.1500000	5.2000000
10	-56.8073106	6.7499999	5.8000000
11	-49.6474443	7.6999999	6.7499999
12	-53.3004870	8.5000000	7.5500000
13	-62.7252059	9.3499999	8.4000000
14	-65.4245472	10.1500000	9.2000000
15	-67.8767443	10.5999999	9.6500000
16	-69.4651878	11.1500000	10.2000000
17	-67.9285603	11.5999999	10.6500000
18	-68.3380470	11.9499999	11.0000000
19	-71.0148697	12.4999999	11.5500000
20	-70.9014616	12.9999999	12.0500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	0.4000000	
1	-25.6395798	0.3000000	-0.6500000
2	-37.4968895	-0.6500000	-1.6000000
3	-48.6561856	-1.5000000	-2.4500000
4	-51.7110171	-1.9500000	-2.9000000
5	-51.2186065	-2.4500000	-3.4000000
6	-57.2254500	-3.2500000	-4.2000000
7	-58.0714040	-4.1500000	-5.1000000
8	-58.4516976	-4.9000000	-5.8500000

NO FURTHER SIDE LOBES ON THIS SIDE



SNUMB=7546T  
5-30, Pass#1

\*\*\*\*\* ANTENNA LIST SUMMARY \*\*\*\*\*

THE MAIN LOBE GAIN IS 51,593.032

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN	REL. GAIN	REL. ANGLE
1	0.0	0.950000
2	-26.10 9378	1.60 0000
3	-26.20 57315	0.30 0000
4	-35.06 4176	2.05 0000
5	-35.33 1581	-0.15 0000
6	-37.64 8881	2.55 0000
7	-38.25 1101	-0.65 0000
8	-41.00 5701	2.85 0000
9	-41.44 03451	-0.95 0000
10	-49.13 7023	3.40 0000
11	-49.71 78700	-1.50 0000
12	-51.36 1087	4.35 0000
13	-51.64 1101	15.40 0000
14	-52.14 0981	-2.45 0000
15	-52.31 1738	3.65 0000
16	-52.51 1581	-4.60 0000
17	-53.20 0919	-1.95 0000
18	-53.43 4431	-2.70 0000
19	-54.65 6400	14.99 0999
20	-55.36 1099	6.00 0999
21	-56.28 5741	15.84 9999

MAIN LOBE GAIN AND FIRST 20 SIDE LOBES TO RIGHT OF (BELOW) MAIN LOBE  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN	REL. GAIN	REL. ANGLE
1	0.0	0.950000
2	-26.10 9378	1.60 0000
3	-26.20 57315	0.30 0000
4	-35.06 4176	2.05 0000
5	-35.33 1581	-0.15 0000
6	-37.64 8881	2.55 0000
7	-38.25 1101	-0.65 0000
8	-41.00 5701	2.85 0000
9	-41.44 03451	-0.95 0000
10	-49.13 7023	3.40 0000
11	-49.71 78700	-1.50 0000
12	-51.36 1087	4.35 0000
13	-51.64 1101	15.40 0000
14	-52.14 0981	-2.45 0000
15	-52.31 1738	3.65 0000
16	-52.51 1581	-4.60 0000
17	-53.20 0919	-1.95 0000
18	-53.43 4431	-2.70 0000
19	-54.65 6400	14.99 0999
20	-55.36 1099	6.00 0999
21	-56.28 5741	15.84 9999

MAIN LOBE GAIN AND FIRST 20 SIDE LOBES TO LEFT OF (BELOW) MAIN LOBE  
REL. GAIN REL. ANGLE  
( DB ) ( DEG )

MAIN	REL. GAIN	REL. ANGLE
1	0.0	0.950000
2	-26.20 57315	0.30 0000
3	-35.33 1581	-0.15 0000
4	-37.64 8881	2.55 0000
5	-38.25 1101	-0.65 0000
6	-41.00 5701	2.85 0000
7	-41.44 03451	-0.95 0000
8	-49.13 7023	3.40 0000
9	-49.71 78700	-1.50 0000
10	-51.36 1087	4.35 0000
11	-51.64 1101	15.40 0000
12	-52.14 0981	-2.45 0000
13	-52.31 1738	3.65 0000
14	-52.51 1581	-4.60 0000
15	-53.20 0919	-1.95 0000
16	-53.43 4431	-2.70 0000
17	-54.65 6400	14.99 0999
18	-55.36 1099	6.00 0999
19	-56.28 5741	15.84 9999

ALL FURTHER SIDE LOBES ON THIS SIDE

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=7462T  
06-17, Pass#1

THE MAIN LOBE GAIN IS 91.5956818

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

MAIN	0.0	2.0000000
1	-26.0259552	1.3500000
2	-26.1778134	2.6500000
3	-32.2269335	0.3500000
4	-33.8849640	3.6500000
5	-34.7722073	0.9000000
6	-35.2179423	3.1000000
7	-46.4150753	-1.3500000
8	-47.0176103	5.4000000
9	-47.7498157	4.4500000
10	-48.8347768	-0.4500000
11	-51.4675833	32.4499999
12	-51.9836366	-0.9000000
13	-52.2319713	4.9000000
14	-54.1929227	31.4499999
15	-54.9821907	-3.0500000
16	-55.1995178	7.1000000
17	-56.1631239	6.2499999
18	-56.1935902	9.1500000
19	-57.0036057	-2.2500000
20	-57.0430957	-5.0000000

RANK	MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **		2.5000000	
1	-26.1794134	2.6500000		0.6500000
2	-35.2179823	3.1000000		1.1000000
3	-33.8347640	3.6500000		1.6500000
4	-47.7498157	4.4500000		2.4500000
5	-52.2319713	4.9000000		2.9000000
6	-47.0174003	5.4000000		3.4000000
7	-56.1651239	6.2499999		4.2500000
8	-55.1995178	7.1000000		5.1000000
9	-60.9742702	7.9000000		5.9000000
10	-62.5395567	8.5999999		6.6000000
11	-56.1339302	9.1500000		7.1500000
12	-68.6917561	10.1500000		8.1500000
13	-47.4105502	10.3499999		8.3499999
14	-67.7934425	10.5999999		8.5999999
15	-67.1977606	10.9000000		8.9000000
16	-65.5187568	11.2499999		9.2499999
17	-72.6025667	12.1999999		10.1999999
18	-73.1557474	12.4000000		10.4000000
19	-69.7171221	12.7499999		10.7499999
20	-66.2298746	13.0500000		11.0500000

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE				
RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )	
MAIN LOBE	** NULL **	1.5000000		
1	-26.0259552	1.3500000		-0.6500000
2	-34.7722073	0.9000000		-1.1000000
3	-32.2269335	0.3500000		-1.6500000
4	-48.8347768	-0.4500000		-2.4500000
5	-51.9836366	-0.9000000		-2.9000000
6	-46.4150753	-1.3500000		-3.3500000
7	-57.0176103	-2.2500000		-4.2499999
8	-54.9821907	-3.0500000		-5.0500000
9	-51.4374411	-3.9000000		-5.9000000
10	-51.5719326	-4.0000000		-5.9999999

NO FURTHER SIDE LOBES ON THIS SIDE

SNUMB=8430T  
06-19, Pass#1

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THE MAIN LOGS ARE

LOCATION AND RELATIVE CALIBRATION OF HIGHEST 20 TIDE LOGS

REL. CAL (FEET)

1	-27.851244	1.600000
2	-27.721577	1.700000
3	-27.704014	1.800000
4	-27.741016	1.900000
5	-27.711017	2.000000
6	-27.711768	2.100000
7	-27.711768	2.200000
8	-27.711768	2.300000
9	-27.711768	2.400000
10	-27.711768	2.500000
11	-27.711768	2.600000
12	-27.711768	2.700000
13	-27.711768	2.800000
14	-27.711768	2.900000
15	-27.711768	3.000000
16	-27.711768	3.100000
17	-27.711768	3.200000
18	-27.711768	3.300000
19	-27.711768	3.400000
20	-27.711768	3.500000

1	-27.851244	1.600000	1.600000
2	-27.721577	1.700000	1.700000
3	-27.704014	1.800000	1.800000
4	-27.741016	1.900000	1.900000
5	-27.711017	2.000000	2.000000
6	-27.711768	2.100000	2.100000
7	-27.711768	2.200000	2.200000
8	-27.711768	2.300000	2.300000
9	-27.711768	2.400000	2.400000
10	-27.711768	2.500000	2.500000
11	-27.711768	2.600000	2.600000
12	-27.711768	2.700000	2.700000
13	-27.711768	2.800000	2.800000
14	-27.711768	2.900000	2.900000
15	-27.711768	3.000000	3.000000
16	-27.711768	3.100000	3.100000
17	-27.711768	3.200000	3.200000
18	-27.711768	3.300000	3.300000
19	-27.711768	3.400000	3.400000
20	-27.711768	3.500000	3.500000

1	-27.851244	1.600000	1.600000
2	-27.721577	1.700000	1.700000
3	-27.704014	1.800000	1.800000
4	-27.741016	1.900000	1.900000
5	-27.711017	2.000000	2.000000
6	-27.711768	2.100000	2.100000
7	-27.711768	2.200000	2.200000
8	-27.711768	2.300000	2.300000
9	-27.711768	2.400000	2.400000
10	-27.711768	2.500000	2.500000
11	-27.711768	2.600000	2.600000
12	-27.711768	2.700000	2.700000
13	-27.711768	2.800000	2.800000
14	-27.711768	2.900000	2.900000
15	-27.711768	3.000000	3.000000
16	-27.711768	3.100000	3.100000
17	-27.711768	3.200000	3.200000
18	-27.711768	3.300000	3.300000
19	-27.711768	3.400000	3.400000
20	-27.711768	3.500000	3.500000



• • • ANTENNA LOBE SCANNER • • •

SNUMB=3389T  
07-22, Pass#1

THE MAIN LOBE GAIN IS 71.0271816

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ( DB ) ANGLE ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
1	0.0	0.004547
2	-1.3844624	-0.013149
3	-7.9706368	0.013787
4	-13.4691548	0.003335
5	-13.5447807	0.0047302
6	-14.6051344	-0.011013
7	-14.8436485	-0.015286
8	-17.9545498	-0.021465
9	-18.0071068	0.001809
10	-18.1287599	0.008828
11	-19.1149130	-0.009487
12	-19.4661136	-0.016812
13	-20.5273795	0.011650
14	-20.8074951	0.000283
15	-20.9712996	0.000354
16	-21.0898099	0.015923
17	-21.9583702	-0.007961
18	-22.5747981	-0.018337
19	-22.8492928	0.008757
20	-23.0487814	0.001880
21	-28.0554190	-0.0026436

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	0.004547	0.004547	0.0001831
2	-13.5447807	0.0048428	0.0003357
3	-18.1287599	0.0050354	0.0004883
4	-20.9712996	0.0051800	0.0006409
5	-23.0487814	0.0053406	0.0007935
6	-24.7613158	0.0054332	0.0009460
7	-26.1544643	0.0056458	0.0010986
8	-27.4194727	0.0057183	0.0012512
9	-28.5879087	0.0059409	0.0014038
10	-29.6958852	0.006135	0.0015564
11	-30.8243442	0.0062756	0.0016785
12	-31.3915586	0.0063782	0.0018311
13	-31.9643657	0.0065408	0.0019836
14	-32.5433310	0.0066433	0.0021362
15	-33.1247699	0.0068459	0.0022888
16	-33.8124199	0.0069485	0.0024414
17	-34.3715324	0.0071411	0.0025940
18	-35.0650401	0.0072632	0.0027466
19	-35.5471311	0.0074458	0.0028992
20	-36.1754923	0.0075684	0.0030518

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	0.0043945	0.0043945	-0.0002136
2	-13.4691548	0.004109	-0.0003662
3	-18.0071068	0.0040283	-0.0005188
4	-20.8074951	0.0038757	-0.0006714
5	-22.8492928	0.003731	-0.0008240
6	-24.4312495	0.0035706	-0.0009766
7	-25.8401670	0.003480	-0.0011292
8	-27.0665145	0.0032654	-0.0012817
9	-28.1934853	0.003128	-0.0014343
10	-29.2613511	0.0029602	-0.0015869
11	-30.2451959	0.0028481	-0.0017395
12	-31.3761858	0.0026555	-0.0018921
13	-31.9055331	0.0025130	-0.0020447
14	-32.4477186	0.0023804	-0.0021973
15	-33.9674416	0.002278	-0.0023500
16	-33.6517534	0.0020752	-0.0025026
17	-34.2721308	0.0019726	-0.0026552
18	-36.6812849	0.001805	-0.0028078
19	-34.8774829	0.001679	-0.0029604
20	-35.0739861	0.0016554	-0.0031130

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=3389T  
07-22, Pass#2

THE MAIN LOBE GAIN IS 0.000000

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ANGLE  
( DB ) ( DEG )

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
1	0.0	-0.005340
2	-0.940628	0.001858
3	-8.3654737	-0.018975
4	-13.3220763	-0.0075542
5	-13.3234384	-0.004575
6	-14.2142100	0.003994
7	-14.3959265	0.009722
8	-15.1959032	0.0217427
9	-17.7445340	-0.0080049
10	-17.8222694	-0.007068
11	-18.8255205	0.0095520
12	-19.0156004	0.008501
13	-20.553549	-0.008523
14	-20.7249724	-0.0078594
15	-21.5849064	-0.016838
16	-21.645694	0.006975
17	-21.8511207	-0.021111
18	-21.9078288	0.007046
19	-22.7386117	-0.006997
20	-23.0051654	-0.0070120
21	-23.6300283	0.005449

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE)			MAIN LOBE
RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	-0.0052485	
1	-13.3234386	-0.005175	0.0001831
2	-17.7445340	-0.005049	0.0003357
3	-20.5581549	-0.004823	0.0004883
4	-22.7385117	-0.004697	0.0006419
5	-24.6257430	-0.004571	0.0007935
6	-26.2261056	-0.004450	0.0009455
7	-27.1384397	-0.004325	0.0010971
8	-28.0633073	-0.004199	0.0012487
9	-29.1221846	-0.003973	0.0013733
10	-30.2495098	-0.003847	0.0015259
11	-30.7401524	-0.003626	0.0016479
12	-31.2707205	-0.003500	0.0018005
13	-31.9151004	-0.003375	0.0019531
14	-32.7295313	-0.003249	0.0021057
15	-33.2693048	-0.003128	0.0022278
16	-33.5597234	-0.002902	0.0023804
17	-33.716583	-0.002876	0.0025330
18	-34.4144454	-0.002650	0.0026855
19	-35.0641847	-0.002530	0.0028076
20	-35.1354258	-0.002304	0.0029602

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW)			MAIN LOBE
RANK	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
MAIN LOBE	** NULL **	-0.0054932	
1	-13.3227753	-0.005542	-0.0002136
2	-17.8222694	-0.005768	-0.0003662
3	-20.7289724	-0.005894	-0.0005188
4	-23.0081654	-0.006020	-0.0006714
5	-25.0212088	-0.006146	-0.0008240
6	-26.4545121	-0.006266	-0.0009460
7	-27.4825482	-0.006492	-0.0010986
8	-28.5632571	-0.006548	-0.0012512
9	-29.6612396	-0.006744	-0.0014038
10	-30.8257065	-0.006865	-0.0015259
11	-31.3224983	-0.007090	-0.0016785
12	-31.8994355	-0.007116	-0.0018311
13	-32.6443648	-0.007342	-0.0019836
14	-33.5251249	-0.0074768	-0.0021362
15	-33.9523282	-0.007589	-0.0022583
16	-34.2432618	-0.007715	-0.0024109
17	-35.0100050	-0.007941	-0.0025635
18	-35.5782480	-0.008066	-0.0027161
19	-36.0846286	-0.008187	-0.0028381
20	-36.2213068	-0.008313	-0.0029907

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=3389T  
07-22, Pass#3

THE MAIN LOBE GAIN IS 70.881639

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
PANK REL. GAIN ( DB ) ANGLE ( DEG )

MAIN	REL. GAIN ( DB )	ANGLE ( DEG )
0	0.0	0.0
1	-4.0771418	-0.01-2822
2	-4.0771418	0.01-2822
3	-13.436486	-0.00 2136
4	-13.436486	0.00 2136
5	-17.5237703	-0.01-0686
6	-17.5237703	0.01-0686
7	-17.5371184	-0.01-4358
8	-17.5371184	0.01-4358
9	-18.2814709	-0.00 3662
10	-18.2814709	0.00 3662
11	-20.8976326	-0.00 4893
12	-20.8976326	0.00 4893
13	-21.9915057	-0.01 9455
14	-21.9915057	0.01 9455
15	-22.403484	-0.01 6479
16	-22.403484	0.01 6479
17	-22.9672651	-0.00 6409
18	-22.9672651	0.00 6409
19	-24.5659446	-0.01 7939
20	-24.5659446	0.01 7939

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
PANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-13.436486	0.0001526	0.0002136
2	-18.286709	0.0003662	0.0003662
3	-20.8976326	0.0004883	0.0004883
4	-22.9672651	0.0006409	0.0006409
5	-24.9291596	0.0007335	0.0007935
6	-26.3977703	0.0009155	0.0009155
7	-27.3809123	0.0010881	0.0010681
8	-28.5861907	0.0012707	0.0012207
9	-29.7519603	0.001328	0.0013428
10	-30.2682948	0.0014554	0.0014954
11	-31.0963516	0.001679	0.0016479
12	-32.1684532	0.0017700	0.0017700
13	-32.403392	0.0019226	0.0019226
14	-32.9899573	0.0020752	0.0020752
15	-33.9291765	0.002278	0.0022278
16	-34.0873079	0.0023499	0.0023499
17	-34.4947338	0.002524	0.0025024
18	-35.2692313	0.0026550	0.0026550
19	-35.4659462	0.002771	0.002771
20	-35.7294650	0.0029297	0.0029297

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
PANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

MAIN LOBE	REL. GAIN ( DB )	TRUE ANGLE ( DEG )	REL. ANGLE ( DEG )
1	-13.436486	-0.0001526	-0.0002136
2	-18.286709	-0.0003662	-0.0003662
3	-20.8976326	-0.0004883	-0.0004883
4	-22.9672651	-0.0006409	-0.0006409
5	-24.9291596	-0.0007335	-0.0007935
6	-26.3977703	-0.0009155	-0.0009155
7	-27.3809123	-0.0010881	-0.0010681
8	-28.5861907	-0.0012707	-0.0012207
9	-29.7519603	-0.001328	-0.0013428
10	-30.2682948	-0.0014554	-0.0014954
11	-31.0963516	-0.001679	-0.0016479
12	-32.1684532	-0.0017700	-0.0017700
13	-32.403392	-0.0019226	-0.0019226
14	-32.9899573	-0.0020752	-0.0020752
15	-33.9291765	-0.002278	-0.0022278
16	-34.0873079	-0.0023499	-0.0023499
17	-34.4947338	-0.002524	-0.0025024
18	-35.2692313	-0.0026550	-0.0026550
19	-35.4659462	-0.002771	-0.002771
20	-35.7294650	-0.0029297	-0.0029297



\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=3389T  
07-22, Pass#4

THE MAIN LOBE GAIN IS 70.163-985

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK	REL. GAIN ( DB )	ANGLE ( DEG )
MAIN	0.0	0.006042
1	-0.390051	-0.0000261
2	-9.1534715	0.02 0806
3	-12.7116203	-0.0270947
4	-13.0638710	0.0038289
5	-13.1806879	0.00 2256
6	-13.9306396	-0.0002397
7	-14.0348844	-0.00 8125
8	-17.6648612	0.0006763
9	-17.7982745	0.00 3782
10	-18.2402203	-0.0006904
11	-18.6415195	-0.00 3618
12	-20.9473114	0.0005542
13	-21.0313020	-0.00 5378
14	-21.2195935	0.00 5308
15	-21.3402227	-0.00 5144
16	-22.5954751	0.00 5975
17	-22.6758500	0.00 4016
18	-22.8855753	0.02 2942
19	-23.0075420	0.00 6528
20	-23.5611772	-0.00 3853

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	** NULL **	0.0061646	
1	-13.1806879	0.0062556	0.0001831
2	-17.7982745	0.0063782	0.0003357
3	-21.2195835	0.0065108	0.0004883
4	-23.0095620	0.0066528	0.0006409
5	-24.8424240	0.0068054	0.0007935
6	-26.5344640	0.0069775	0.0009461
7	-27.4832940	0.0070001	0.0010987
8	-28.8833518	0.0072027	0.0011902
9	-29.6853976	0.0073447	0.0013123
10	-30.5147181	0.0075773	0.0014648
11	-31.6880172	0.0076994	0.0015869
12	-32.0253940	0.0077420	0.0017395
13	-33.0024584	0.0079446	0.0018921
14	-33.0721443	0.0080566	0.0020142
15	-33.8197570	0.008292	0.0021667
16	-34.8763042	0.0083618	0.0023193
17	-34.9124006	0.0084439	0.0024414
18	-35.5367770	0.0086665	0.0025940
19	-36.0362091	0.0087785	0.0027461
20	-36.2629919	0.0089111	0.0028687

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN TRUE ANGLE REL. ANGLE  
( DB ) ( DEG ) ( DEG )

MAIN LOBE	** NULL **	0.0058899	
1	-13.0638719	0.0058899	-0.0002136
2	-17.6648612	0.0056663	-0.0003662
3	-20.9487314	0.0055442	-0.0004883
4	-22.6758900	0.005416	-0.0006409
5	-24.5160203	0.005290	-0.0007935
6	-26.0109596	0.005170	-0.0009461
7	-26.9680044	0.0049744	-0.0010987
8	-28.3730521	0.004818	-0.0012207
9	-28.9845762	0.004697	-0.0013428
10	-29.8090572	0.004571	-0.0014954
11	-30.7984829	0.004450	-0.0016174
12	-31.1063862	0.0042725	-0.0017700
13	-31.9080706	0.004199	-0.0019226
14	-32.8002052	0.003978	-0.0020447
15	-32.9480376	0.003852	-0.0021973
16	-33.7375655	0.003731	-0.0023193
17	-33.7743152	0.003506	-0.0024719
18	-34.4109276	0.003480	-0.0026245
19	-34.7033286	0.003259	-0.0027466
20	-34.9442163	0.003133	-0.0028992

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=3389T  
07-22, Pass#5

THE MAIN LOBE GAIN IS 70.258791

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN (DB) ANGLE (DEG)

RANK	REL. GAIN (DB)	ANGLE (DEG)
1	-13.0719099	-0.006146
2	-18.0633210	-0.006020
3	-20.5184202	-0.005899
4	-22.9893827	-0.005773
5	-24.3762286	-0.005652
6	-26.0877004	-0.005426
7	-26.9924340	-0.005306
8	-28.2995371	-0.005180
9	-28.9265540	-0.005059
10	-30.0457816	-0.004933
11	-30.4815969	-0.004793
12	-31.4425478	-0.004667
13	-31.7360935	-0.004566
14	-32.6272459	-0.004340
15	-32.8040972	-0.004219
16	-33.6272922	-0.004094
17	-33.7086210	-0.003973
18	-34.4895491	-0.003847
19	-34.4752536	-0.003692
20	-35.2643590	-0.003540

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN (DB) TRUE ANGLE (DEG) REL. ANGLE (DEG)

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
1	-13.0719099	-0.006146	0.0002136
2	-18.0633210	-0.006020	0.0003662
3	-20.5184202	-0.005899	0.0004883
4	-22.9893827	-0.005773	0.0006409
5	-24.3762286	-0.005652	0.0007629
6	-26.0877004	-0.005426	0.0009155
7	-26.9924340	-0.005306	0.0010376
8	-28.2995371	-0.005180	0.0011902
9	-28.9265540	-0.005059	0.0013123
10	-30.0457816	-0.004933	0.0014648
11	-30.4815969	-0.004793	0.0015869
12	-31.4425478	-0.004667	0.0017395
13	-31.7360935	-0.004566	0.0018616
14	-32.6272459	-0.004340	0.0020142
15	-32.8040972	-0.004219	0.0021362
16	-33.6272922	-0.004094	0.0022888
17	-33.7086210	-0.003973	0.0024109
18	-34.4895491	-0.003847	0.0025635
19	-34.4752536	-0.003692	0.0026855
20	-35.2643590	-0.003540	0.0028381

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN (DB) TRUE ANGLE (DEG) REL. ANGLE (DEG)

RANK	REL. GAIN (DB)	TRUE ANGLE (DEG)	REL. ANGLE (DEG)
1	-13.1510777	-0.0065613	-0.0001831
2	-18.1207824	-0.0067139	-0.0003357
3	-20.7545094	-0.0068359	-0.0004578
4	-23.2408285	-0.0069485	-0.0006104
5	-24.7934713	-0.0071106	-0.0007324
6	-26.4538657	-0.0072632	-0.0008850
7	-27.5298929	-0.0073853	-0.0010071
8	-28.8396142	-0.0075378	-0.0011597
9	-29.6377177	-0.0076999	-0.0012817
10	-30.7009635	-0.0078125	-0.0014343
11	-31.3118243	-0.0079466	-0.0015564
12	-32.2614855	-0.0080872	-0.0017090
13	-32.7325158	-0.008292	-0.0018311
14	-33.5717311	-0.0083618	-0.0019836
15	-33.9354949	-0.0084399	-0.0021057
16	-34.7201190	-0.0086365	-0.0022583
17	-34.9925299	-0.0087885	-0.0023804
18	-35.7348830	-0.0089111	-0.0025330
19	-35.9405408	-0.0090332	-0.0026550
20	-36.6177163	-0.0091558	-0.0028076

7015-0218  
100-10-10

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=3389T  
07-22, Pass#6

THE MAIN LOBE GAIN IS 71.2974668

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN ( DB ) ANGLE ( DEG )

MAIN	0.0	0.000424
1	-3.5930748	-0.017258
2	-4.7226242	0.013433
3	-13.4659348	0.000071
4	-13.6019511	0.006409
5	-16.7247262	-0.015122
6	-16.8451421	-0.0129089
7	-17.7144024	0.011602
8	-17.8118229	0.004883
9	-17.8737583	0.001597
10	-18.0223069	0.015569
11	-21.0616384	0.002817
12	-21.1944563	0.003662
13	-21.3267379	-0.013901
14	-22.0312123	-0.010310
15	-22.5335313	0.015381
16	-22.9515204	0.002136
17	-22.9841994	0.016790
18	-23.0633162	0.004343
19	-24.0321965	-0.012375
20	-24.5228772	-0.014836

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

MAIN LOBE	** NULL **	0.0009460	
1	-13.4659348	0.001071	0.0001631
2	-17.8797949	0.0011597	0.0003357
3	-21.0616384	0.001217	0.0004578
4	-23.0683149	0.001443	0.0006104
5	-24.8735061	0.001564	0.0007324
6	-26.3520017	0.001790	0.0008850
7	-27.4689746	0.001811	0.0010071
8	-28.6049645	0.001936	0.0011597
9	-29.4710913	0.002157	0.0012817
10	-30.8213544	0.002278	0.0014038
11	-31.0994225	0.002304	0.0015564
12	-32.0667491	0.002524	0.0016785
13	-32.5552506	0.002650	0.0018311
14	-33.0991125	0.002771	0.0019531
15	-33.7799675	0.002997	0.0021057
16	-34.1193650	0.0030518	0.0022278
17	-35.0198164	0.003243	0.0023804
18	-35.0237913	0.003364	0.0025024
19	-35.7956085	0.003465	0.0026245
20	-35.8615632	0.003611	0.0027771

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANK REL. GAIN ( DB ) TRUE ANGLE ( DEG ) REL. ANGLE ( DEG )

MAIN LOBE	** NULL **	0.0006714	
1	-13.6019511	0.000609	-0.0001831
2	-17.8118229	0.000483	-0.0003357
3	-21.1984563	0.000362	-0.0004578
4	-22.9519806	0.000236	-0.0006104
5	-24.9763432	0.000216	-0.0007324
6	-26.1937399	-0.000010	-0.0008850
7	-27.4775105	-0.000131	-0.0010071
8	-28.6365709	-0.000357	-0.0011597
9	-29.3620181	-0.000478	-0.0012817
10	-30.5867200	-0.000604	-0.0014038
11	-30.9245051	-0.000724	-0.0015564
12	-32.0807679	-0.000845	-0.0016785
13	-32.2599139	-0.001071	-0.0018311
14	-33.1491699	-0.001192	-0.0019531
15	-33.5447454	-0.001217	-0.0021057
16	-33.9922433	-0.001438	-0.0022278
17	-34.6511387	-0.001564	-0.0023804
18	-34.8183942	-0.0016785	-0.0025024
19	-35.7722073	-0.001811	-0.0026550
20	-35.6244732	-0.0019531	-0.0027771

J-53

COPY AVAILABLE TO DDC DOES NOT  
PERMIT FULLY LEGIBLE PRODUCTION



SNUMB=2730T

07-22, Pass#1

44 MAY 1965 14:00 7 14347

[illegible]

1	757 459	757 459
2	757 459	757 459
3	757 459	757 459
4	757 459	757 459
5	757 459	757 459
6	757 459	757 459
7	757 459	757 459
8	757 459	757 459
9	757 459	757 459
10	757 459	757 459
11	757 459	757 459
12	757 459	757 459
13	757 459	757 459
14	757 459	757 459
15	757 459	757 459
16	757 459	757 459
17	757 459	757 459
18	757 459	757 459
19	757 459	757 459
20	757 459	757 459

MAIL LOGS  
MAIL LOGS  
MAIL LOGS

1	-26.1394177	0.00000000	0.00000000
2	-1.8262877	0.00000000	0.00000000
3	-13.8158374	0.00000000	0.00000000
4	-15.1845510	0.00000000	0.00000000
5	-17.6755949	0.00000000	0.00000000
6	-19.7355557	0.00000000	0.00000000
7	-41.1312167	0.00000000	0.00000000
8	-41.9348595	0.00000000	0.00000000
9	-41.4247501	0.00000000	0.00000000
10	-41.9725443	0.00000000	0.00000000
11	-42.7184529	0.00000000	0.00000000
12	-42.4757674	0.00000000	0.00000000
13	-42.6381759	0.00000000	0.00000000
14	-42.1132733	0.00000000	0.00000000
15	-41.8332441	0.00000000	0.00000000
16	-41.3427790	0.00000000	0.00000000
17	-39.9232922	0.00000000	0.00000000
18	-35.3385359	0.00000000	0.00000000
19	-35.1535938	0.00000000	0.00000000
20	-31.2782688	0.00000000	0.00000000

MAIN LOBBY HALL AND FIRST 20 SIDE-LOBBIES TO LEFT OF (BELOW) MAIN LOBBY			
RANK	REL. MAIN	TRF. ANGLE	REL. ANGLE
(OR)	(OR)	(DEG)	(DEG)
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			

NAME	DOB	SSN	DOB	SSN
1	-17.5892149	0000000000	0000000000	-0.00000000
2	-27.144773	0000000000	0000000000	-0.00000000
3	-31.5112773	0000000000	0000000000	-0.00000000
4	-33.6485536	0000000000	0000000000	-0.00000000
5	-35.5094716	0000000000	0000000000	-0.00000000
6	-36.4912344	0000000000	0000000000	-0.00000000
7	-37.7481926	0000000000	0000000000	-0.00000000
8	-38.5519865	0000000000	0000000000	-0.00000000
9	-39.3672676	0000000000	0000000000	-0.00000000
10	-40.445459	0000000000	0000000000	-0.00000000
11	-39.7114556	0000000000	0000000000	-0.00000000
12	-39.9534718	0000000000	0000000000	-0.00000000
13	-39.5715719	0000000000	0000000000	-0.00000000
14	-39.3794324	0000000000	0000000000	-0.00000000
15	-38.7643492	0000000000	0000000000	-0.00000000
16	-37.6931323	0000000000	0000000000	-0.00000000
17	-36.7417935	0000000000	0000000000	-0.00000000
18	-35.3432290	0000000000	0000000000	-0.00000000
19	-33.0167802	0000000000	0000000000	-0.00000000
20	-29.7449808	0000000000	0000000000	-0.00000000

\*\*\* ANTENNA LOBE SCANNER \*\*\*

SNUMB=2730T  
07-22, Pass#2

THE MAIN LOBE IS

LOCATED TO RELATIVE 141 BY ANGLE OF SITE 12.3  
REL. ANGLE (DEG)

REL. ANGLE (DEG)	REL. ANGLE (DEG)	REL. ANGLE (DEG)
1	-1.3256716	-1.3256716
2	-1.3414770	-1.3414770
3	-1.3566109	-1.3566109
4	-1.3717149	-1.3717149
5	-1.3863726	-1.3863726
6	-1.4004926	-1.4004926
7	-1.4140727	-1.4140727
8	-1.4271124	-1.4271124
9	-1.4396116	-1.4396116
10	-1.4515703	-1.4515703
11	-1.4629885	-1.4629885
12	-1.4738662	-1.4738662
13	-1.4842034	-1.4842034
14	-1.4940001	-1.4940001
15	-1.5032562	-1.5032562
16	-1.5119717	-1.5119717
17	-1.5201466	-1.5201466
18	-1.5277809	-1.5277809
19	-1.5348746	-1.5348746
20	-1.5414276	-1.5414276

MAIN LOBE FULL AND FIRST 20 SITE-LOBES TO RIGHT OF (ASDAS) MAIN LOBE  
REL. ANGLE (DEG)

REL. ANGLE (DEG)	REL. ANGLE (DEG)	REL. ANGLE (DEG)
1	-26.3764210	-26.3764210
2	-31.2777563	-31.2777563
3	-33.6741971	-33.6741971
4	-35.6357316	-35.6357316
5	-37.2157617	-37.2157617
6	-38.2819975	-38.2819975
7	-39.7331391	-39.7331391
8	-39.7277525	-39.7277525
9	-39.6194439	-39.6194439
10	-39.6117125	-39.6117125
11	-39.1170962	-39.1170962
12	-38.6724070	-38.6724070
13	-37.9431491	-37.9431491
14	-37.1253637	-37.1253637
15	-35.4737575	-35.4737575
16	-33.2697795	-33.2697795
17	-29.7440939	-29.7440939
18	-22.354376	-22.354376
19	-1.6264916	-1.6264916
20	-26.5457754	-26.5457754

MAIN LOBE FULL AND FIRST 20 SITE-LOBES TO LEFT OF (ASDAS) MAIN LOBE  
REL. ANGLE (DEG)

REL. ANGLE (DEG)	REL. ANGLE (DEG)	REL. ANGLE (DEG)
1	-18.9337149	-18.9337149
2	-28.5234140	-28.5234140
3	-32.6744497	-32.6744497
4	-35.5337795	-35.5337795
5	-37.7117999	-37.7117999
6	-39.7337771	-39.7337771
7	-41.3467339	-41.3467339
8	-41.2543957	-41.2543957
9	-42.0355105	-42.0355105
10	-42.8725792	-42.8725792
11	-42.6199236	-42.6199236
12	-42.6121793	-42.6121793
13	-42.5250714	-42.5250714
14	-42.257796	-42.257796
15	-41.4477656	-41.4477656
16	-41.1752172	-41.1752172
17	-38.4461917	-38.4461917
18	-34.8333632	-34.8333632
19	-24.8722523	-24.8722523
20	-8.3485970	-8.3485970

..... ANTENNA LOBE SCANNER .....

SNUMB=2730T  
07-22, Pass#3

THE MAIN LOBE DATA IS AS FOLLOWS:

LOCATION AND RELATIVE DATA OF HIGHEST 20 SIDE LOBES  
RANK REL. GAIN (DB) REL. ANGLE (DEG)

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-21.515777	0.0142522
2	-21.515777	0.0142522
3	-21.513445	0.0141351
4	-21.513445	0.0141351
5	-21.512231	0.0141227
6	-21.512231	0.0141227
7	-32.7353777	0.013 615
8	-32.7353777	0.013 615
9	-32.735 513	0.012752
10	-32.735 513	0.012752
11	-33.732352	0.015529
12	-33.732352	0.015529
13	-33.727633	0.017277
14	-33.727633	0.017277
15	-35.822451	0.017277
16	-35.822451	0.017277
17	-37.641953	0.013744
18	-37.641953	0.013744
19	-38.7847845	0.0113525
20	-38.7847845	0.0113525

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (BEHIND) MAIN LOBE  
RANK REL. GAIN (DB) REL. ANGLE (DEG)

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-20.516231	0.0112297
2	-22.997513	0.012752
3	-35.729533	0.012297
4	-37.641953	0.0137542
5	-39.735377	0.0146397
6	-40.7943677	0.0154932
7	-41.789392	0.0163477
8	-41.789392	0.0177871
9	-41.789392	0.0179346
10	-41.789392	0.0187891
11	-41.789392	0.0194436
12	-39.4749316	0.011699
13	-35.822451	0.0113525
14	-35.822451	0.012277
15	-32.735377	0.013 615
16	-21.2134455	0.0141351
17	-21.2134455	0.0142522
18	-33.732352	0.015529
19	-38.7847845	0.0163574
20	-41.9382226	0.0172119

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BEFORE) MAIN LOBE  
RANK REL. GAIN (DB) REL. ANGLE (DEG)

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-25.5267236	-0.0112297
2	-22.997513	-0.012752
3	-35.729533	-0.012297
4	-37.641953	-0.0137542
5	-39.735377	-0.0146397
6	-40.7943677	-0.0154932
7	-41.789392	-0.0163477
8	-41.789392	-0.0177871
9	-41.789392	-0.0179346
10	-41.789392	-0.0187891
11	-41.789392	-0.0194436
12	-39.4749316	-0.011699
13	-35.822451	-0.0113525
14	-35.822451	-0.012277
15	-32.735377	-0.013 615
16	-21.2134455	-0.0141351
17	-21.2134455	-0.0142522
18	-33.732352	-0.015529
19	-38.7847845	-0.0163574
20	-41.9382226	-0.0172119



• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=2730T  
07-22, Pass#4

THE MAIN LOBE AND FIRST 20 SIDE-LOBES TO RIGHT OF (ANGLE) MAIN LOBE

LOCATION OF RELATIVE POSITION OF HIGHEST 20 SIDE-LOBES  
REL. MAIN (DEG) REL. MAIN (DEG)

MAIN LOBE	REL. MAIN (DEG)	REL. MAIN (DEG)
1	-27.4772911	0.0000000
2	-17.3297132	0.0000000
3	-11.9216818	0.0000000
4	-27.1128721	0.0000000
5	-28.3716564	0.0000000
6	-26.7453111	0.0000000
7	-24.1216916	0.0000000
8	-24.7334166	0.0000000
9	-27.1726599	0.0000000
10	-31.1141444	0.0000000
11	-31.7511367	0.0000000
12	-31.7986544	0.0000000
13	-37.1156183	0.0000000
14	-32.1134763	0.0000000
15	-37.7256599	0.0000000
16	-31.4177457	0.0000000
17	-34.5733353	0.0000000
18	-34.7476146	0.0000000
19	-34.7553346	0.0000000
20	-35.2793357	0.0000000

MAIN LOBE FULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ANGLE) MAIN LOBE  
REL. MAIN (DEG) REL. MAIN (DEG)

MAIN LOBE	REL. MAIN (DEG)	REL. MAIN (DEG)
1	-27.1726599	0.0000000
2	-31.5214644	0.0000000
3	-34.5714353	0.0000000
4	-36.3372413	0.0000000
5	-37.1128721	0.0000000
6	-37.8227616	0.0000000
7	-38.4626920	0.0000000
8	-38.4173317	0.0000000
9	-37.8213414	0.0000000
10	-36.8415219	0.0000000
11	-35.4156774	0.0000000
12	-34.4177957	0.0000000
13	-31.1141444	0.0000000
14	-23.3715564	0.0000000
15	-11.4772911	0.0000000
16	-25.9463100	0.0000000
17	-32.1134763	0.0000000
18	-35.2793357	0.0000000
19	-37.7256599	0.0000000
20	-39.2411357	0.0000000

MAIN LOBE FULL AND FIRST 20 SIDE-LOBES TO LEFT OF (ANGLE) MAIN LOBE  
REL. MAIN (DEG) REL. MAIN (DEG)

MAIN LOBE	REL. MAIN (DEG)	REL. MAIN (DEG)
1	-22.1754711	0.0000000
2	-37.8481367	0.0000000
3	-34.7426146	0.0000000
4	-37.8481367	0.0000000
5	-39.7412310	0.0000000
6	-41.1731119	0.0000000
7	-42.1195646	0.0000000
8	-43.2116933	0.0000000
9	-43.2452232	0.0000000
10	-43.7731133	0.0000000
11	-43.4565619	0.0000000
12	-42.9119639	0.0000000
13	-41.4473532	0.0000000
14	-34.5743534	0.0000000
15	-11.4772911	0.0000000
16	-32.3134763	0.0000000
17	-45.1174100	0.0000000
18	-51.9792217	0.0000000
19	-37.3414951	0.0000000
20	-83.9565592	0.0000000

• • • • ANTENNA LOBE SCANNER • • • •

SNUMB=2730T  
07-22, Pass#5

THE MAIN LOBE IS 71.231 223

LOCATION AND RELATIVE DASH OF HIGHEST 20 SIDE LOBES  
RANGE REL. DATA ANGLE  
( DEG ) ( DEG )

MAIN LOBE	REL. DATA	ANGLE
1	-17.5154146	-0.0061477
2	-12.1271906	0.0073242
3	-14.1571462	-0.0000192
4	-22.1931637	0.0011132
5	-27.8326463	-0.0000594
6	-26.1122419	0.0007134
7	-24.0231721	0.0047930
8	-31.5461999	-0.0000135
9	-31.6477165	0.0004670
10	-31.4158375	-0.0000125
11	-31.9476743	0.0004434
12	-35.1352743	-0.0004932
13	-35.4152507	0.0004410
14	-35.5445364	-0.0004445
15	-35.7126849	0.0004432
16	-35.7405267	-0.0004410
17	-37.1746546	0.0004410
18	-37.1746546	-0.0004410
19	-37.1746546	0.0004410
20	-38.3422306	-0.0004410

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE  
RANGE REL. DATA ANGLE  
( DEG ) ( DEG )

MAIN LOBE	REL. DATA	ANGLE
1	-22.3931637	-0.0000000
2	-31.4761375	0.0004893
3	-35.1352743	0.0017290
4	-37.1746546	0.0024277
5	-38.3422306	0.004283
6	-39.0274440	0.0051270
7	-39.1027494	0.0057296
8	-38.5721114	0.0073242
9	-37.3981566	0.0084279
10	-35.4132639	0.0094436
11	-31.9476743	0.0107472
12	-23.8755433	0.0115418
13	-0.5104146	0.013515
14	-30.5346899	0.013719
15	-35.7922257	0.015146
16	-39.0274224	0.0162354
17	-41.0941172	0.0173340
18	-42.0135875	0.0184326
19	-43.0262653	0.019313
20	-44.0561964	0.020570

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE  
RANGE REL. DATA ANGLE  
( DEG ) ( DEG )

MAIN LOBE	REL. DATA	ANGLE
1	-31.6677465	-0.0014646
2	-35.7029849	-0.0025615
3	-38.5614672	-0.0037842
4	-40.8124320	-0.0044878
5	-41.9594916	-0.0059314
6	-42.022618	-0.0077891
7	-43.2011116	-0.0086173
8	-43.5944332	-0.0092773
9	-42.5691302	-0.0104940
10	-41.274323	-0.0115957
11	-35.5142664	-0.0123174
12	-12.1271509	-0.0134719
13	-19.3531672	-0.0147705
14	-47.7794745	-0.0154601
15	-53.5427175	-0.0170898
16	-59.5472250	-0.0181809
17	-65.5461714	-0.0192371
18	-74.5772294	-0.0202637
19	-78.7121142	-0.0217245
20	-70.0076170	-0.0227091

SNUMB=2730T  
07-22, Pass#6

\*\*\*\*\* ANTENNA LOBE SCANNER \*\*\*\*\*

THE MAIN LOBE POINT IS 7.5141686

LOCATION AND RELATIVE GAIN OF HIGHEST 20 SIDE LOBES

RANK REL. GAIN REL. ANGLE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-27.7241028	0.0000000
2	-27.9441837	0.00144048
3	-28.1115000	0.00165669
4	-28.4878002	0.00168500
5	-29.6113457	0.00397749
6	-29.7761145	0.00400100
7	-31.7517127	0.00575588
8	-32.9946911	0.00586019
9	-33.8716053	0.00629297
10	-34.2576085	0.00624451
11	-34.6574216	0.00617422
12	-34.8149157	0.00619531
13	-35.1128554	0.00614732
14	-35.8725173	0.00467229
15	-37.5175836	0.00117188
16	-37.4013132	0.00031733
17	-37.1845996	0.00093994
18	-33.0037225	0.00274541
19	-25.6502177	0.00549932
20	-27.0277487	0.00643945

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO RIGHT OF (ABOVE) MAIN LOBE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-25.1117815	0.0000000
2	-32.9714153	0.0029297
3	-36.6720373	0.0042725
4	-38.6821777	0.0054932
5	-39.6702141	0.0067139
6	-41.5123124	0.0079346
7	-41.3151557	0.0092773
8	-39.3497229	0.0104940
9	-37.3173336	0.0117156
10	-32.5733501	0.0131415
11	-25.5441837	0.0144043
12	-31.6712121	0.0157558
13	-19.9023470	0.0166010
14	-44.5458153	0.0178223
15	-47.3712143	0.0191550
16	-50.6022635	0.0203857
17	-53.4041190	0.0216064
18	-55.5424957	0.0228271
19	-56.0352625	0.0241099
20	-41.2545165	0.0253915

MAIN LOBE NULL AND FIRST 20 SIDE-LOBES TO LEFT OF (BELOW) MAIN LOBE

RANK	REL. GAIN (DB)	REL. ANGLE (DEG)
1	-29.7761145	-0.0000000
2	-34.8149157	-0.00144048
3	-37.4861332	-0.00165669
4	-39.7787889	-0.00168500
5	-39.9144126	-0.00397749
6	-39.9432722	-0.00400100
7	-39.2251279	-0.00575588
8	-37.8385296	-0.00586019
9	-34.6574206	-0.00629297
10	-25.4573032	-0.00624451
11	-2.9241128	-0.00617422
12	-35.1127594	-0.00619531
13	-40.6492743	-0.00614732
14	-44.2945640	-0.00467229
15	-46.9595957	-0.00117188
16	-49.1197922	-0.00031733
17	-50.3332515	-0.00093994
18	-52.2281546	-0.00274541
19	-53.3327477	-0.00549932
20	-53.8054329	-0.00643945



A P P E N D I X   K  
I N T E R A C T I V E   R A D A R   S I M U L A T O R  
D E S I G N   S T U D Y

K.1   I N T R O D U C T I O N

This appendix documents the results of a study and investigation directed toward the design of an Interactive Radar Simulation system. The Interactive Radar Simulation system described herein will significantly improve the efficiency of design engineers in performing radar system evaluations, in testing new concepts, and in predicting the effect of subsystem parameter changes on total system performance. The suggested design includes features that will streamline the process by which the RADC Radar System Simulation Model (RADSIM) computer program is used.

This streamlining consists of eliminating the menial, time-consuming tasks which are associated with the present method for submission of batch or time sharing computer jobs. An example of this is the typing of simulation control and module parameter cards on either a keypunch machine or a time sharing terminal. At the output end of the simulation process, the digestion of output data by the user is improved by the use of a high resolution CRT graphics display. This device will allow the plotting of output data directly from the host computer. In addition, all information required to convert a radar system block diagram into a form suitable for simulation model usage will be stored locally on magnetic tape in a catalog form complete with index and cross references so that it can be used in the same manner as a reference document. The hardware system for implementing these improvements will be referred to as the Dedicated User Interface (DUI). The Interactive Radar Simulator system described herein consists of the Radar System Simulation Model (RADSIM) computer program, the Honeywell 635 host computer (H635) and the Dedicated User Interface (DUI).

## K.2 INTERACTIVE RADAR SIMULATOR BACKGROUND AND REQUIREMENTS

In this section the background and shortcomings of the existing RADSIM computer are discussed and the Dedicated User Interface (DUI) is described in functional terms.

### K.2.1 Simulation Model Usage

The RADSIM computer program in its present configuration consists of two segments which are executed as separate activities. These segments are referred to as the Simulation Data Initializer and the Simulation Controller/Modules.

The Simulation Data Initializer serves as the interface between the user and the Simulation Controller. This segmentation of the simulation model computer program was necessary since input data in a format convenient to the user must be converted to a form suitable for use by the simulation modules. The user defines the simulation via two types of punch cards: simulation control cards and module parameter data cards. The term punch card is used here in the sense of either a physical punch card or of a card image if the job is submitted through the CARDIN time sharing subsystem of the H635.

The simulation control cards determine what operations are to be performed in the simulation activity. This includes the following: (1) scheduling of modules for execution, (2) data transfer to and from temporary disc files, and (3) modification of parameters for multiple executions of a simulation model configuration.

The module parameter data cards define the parameters of the simulation modules to be executed in the simulation activity. Each module requiring input data has a unique name-list which contains the input parameters. Upon completion of the Data Initialization activity, the Simulation activity is executed.

At the present time the output data of a simulation job is written onto a permanent disc file or magnetic tape, or punched on cards. The user then picks up the output data at the central site of the host computer or uses the time sharing system to dump data stored on permfile to paper tape or to listing paper.

## K.2.2 Simulation Model Limitations

In subsection K.2.1 the use of the existing RADSIM computer program was briefly reviewed. In this subsection those aspects of the computer program which restrict or otherwise hinder the use of the simulation model will be discussed. In performing a simulation job there are two phases which consume the majority of the user's time, i.e. the operations of data input and data retrieval. In other words, the major bottleneck is the interface between the user and the host computer. Most of the time spent in performing these tasks is not engineering design time, e.g. the keypunching of control and module parameter cards or alternatively, typing the cards into a time sharing file. In addition to the typing task, the user must constantly refer to tables of module names, reference numbers, parameters, and units of measure during the process of converting a radar system block diagram into a form suitable for input into the RADSIM computer program.

At the present time, the output of a simulation job is written onto a permanent disc file or on magnetic tape, or is punched on cards. This aspect of the process of accomplishing a simulation is a significant factor in job turn around and is probably the most expensive portion when the manhours expended in the manual handling of data are considered.

In order to summarize the limitations described above, the following example of a simulation job is offered:

1. The user defines the block diagram complete with the parameters of a system to be simulated.  
(Elapsed time = 2.0 Hours, User Time = 2.0)
2. The user converts the block diagram into a deck of cards suitable for input to the data loader activity.  
(Elapsed Time = 2.0 Hours, User Time = 2.0)
3. The user submits the job to the host computer and the job is executed. (Elapsed Time = 1.0 Hours, User Time = 0.25 Hours)
4. The user retrieves the output data in the form of punch cards or magnetic tape, transports the data to an off line plotter system, and plots the data.  
(Elapsed Time = 2.0 Hours, User Time = 2.0 Hours)



In the above example the user spent 6.25 hours performing a complete simulation job of which only 2.0 hours were used in performing an engineering design task. Approximately 60% of the design engineer's time was consumed by non-engineering tasks. In the following subsection a system is described from a functional viewpoint which will improve the productivity of the radar design engineer by freeing him from the menial tasks which must be performed in order to use the current RADSIM computer program. In the example presented above, if the data were dumped to paper tape via an ASR 33 teletype, the time required would be even greater since the ASR 33 data transfer rate is only 10 characters per second (cps). Since 10 to 13 characters are required to represent one floating point number this corresponds to one point of data per second or less. A plot of 3000 points would therefore, require almost one hour to punch on paper tape.

### K.2.3 Dedicated User Interface

A Dedicated User Interface for the submission of simulation jobs and retrieval of output data should, as a minimum, have the following capabilities:

- (1) Storage for all computer program data required by the user for the specification of parameters
- (2) The capability of producing block diagrams of the simulation job
- (3) Storage for the job definition file such that it can be used in the construction of future simulation jobs
- (4) A high data rate channel for communication with the host computer. The upper bound on data rate will be determined by characteristics of a voice grade direct dial telephone channel
- (5) A high resolution CRT display capable of plotting the output data
- (6) A device capable of producing a high quality paper copy of anything presented on the CRT display.

With a system having these capabilities, the procedure of job setup will simply be a matter of the user answering a sequence of questions posed by the DUI. When the job definition is complete, the user will have a paper copy of the

simulation block diagram and a magnetic tape cassette containing the job definition file in a form compatible with the RADSIM computer program. The user then connects the DUI system to the host computer, selects CARDIN TSS subsystem, transfers the contents of the cassette to the TSS current file, and gives the RUN command. The DUI is then disconnected from the host computer.

After the simulation job has been executed, the user connects the DUI to the host computer. Again a question/answer sequence is entered where the system asks the user what is to be plotted and some parameters of the plots. The data generated by the simulation job are then plotted on the CRT display. The CRT display can subsequently be reproduced on paper if the user desires a permanent copy. In addition to immediate plotting, the user has the option of transmitting the contents of the simulation job output file to the DUI for recording on a magnetic tape cassette. The stored data can subsequently be plotted off-line. In addition, the data generated by the host computer can be used as input data for programs executed by the DUI as a stand alone computer system.

### K.3 DEDICATED USER INTERFACE HARDWARE

A functional block diagram of the suggested Interactive Radar simulator is shown in Figure K.3-1. The DUI subsystem is indicated by a dashed line. Two hardware designs which satisfy the DUI requirements delineated in paragraph K.2.3 are described in this section. The two designs differ primarily in the minicomputer selected for the communications buffer. Design #1 is configured around a Hewlett-Packard 2100A minicomputer. Design #2 is configured around a Digital Equipment Corporation PDP-11/05 minicomputer. Design #1 offers performance superior to that of Design #2 in every respect, but does so at a higher cost. The details of each design are discussed and a comparison made between them in the remainder of this subsection.

#### K.3.1 System Design #1

The block diagram of the Design #1 system is presented in Figure K.3-2. The features and parameters of the subsystems which make up this design are discussed in the following paragraphs.

##### K.3.1.1 Hewlett-Packard 2100A Minicomputer

The HP2100A minicomputer is a user microprogrammable general purpose machine. A summary of the HP2100A parameters is presented in paragraph K.3.3 which compares the HP and DEC minicomputers.

The memory requirements for the HP2100A are determined by the combined size (13K) of the minicomputer Basic Control System (4K), the DUI executive program (3K), and the Simulation Job Setup program (6K). Since memory is supplied in either 8K or 16K increments, the memory size chosen for the minicomputer is 16K.

Eleven Input/Output (I/O) channel slots are required to connect the peripheral devices and special processing modules to the HP2100A. The required I/O interface cards and other processor modules are given by the following list:

1. 12587B EIA RS232 Asynchronous data set interface
2. 12531C Current loop interface to operator's console



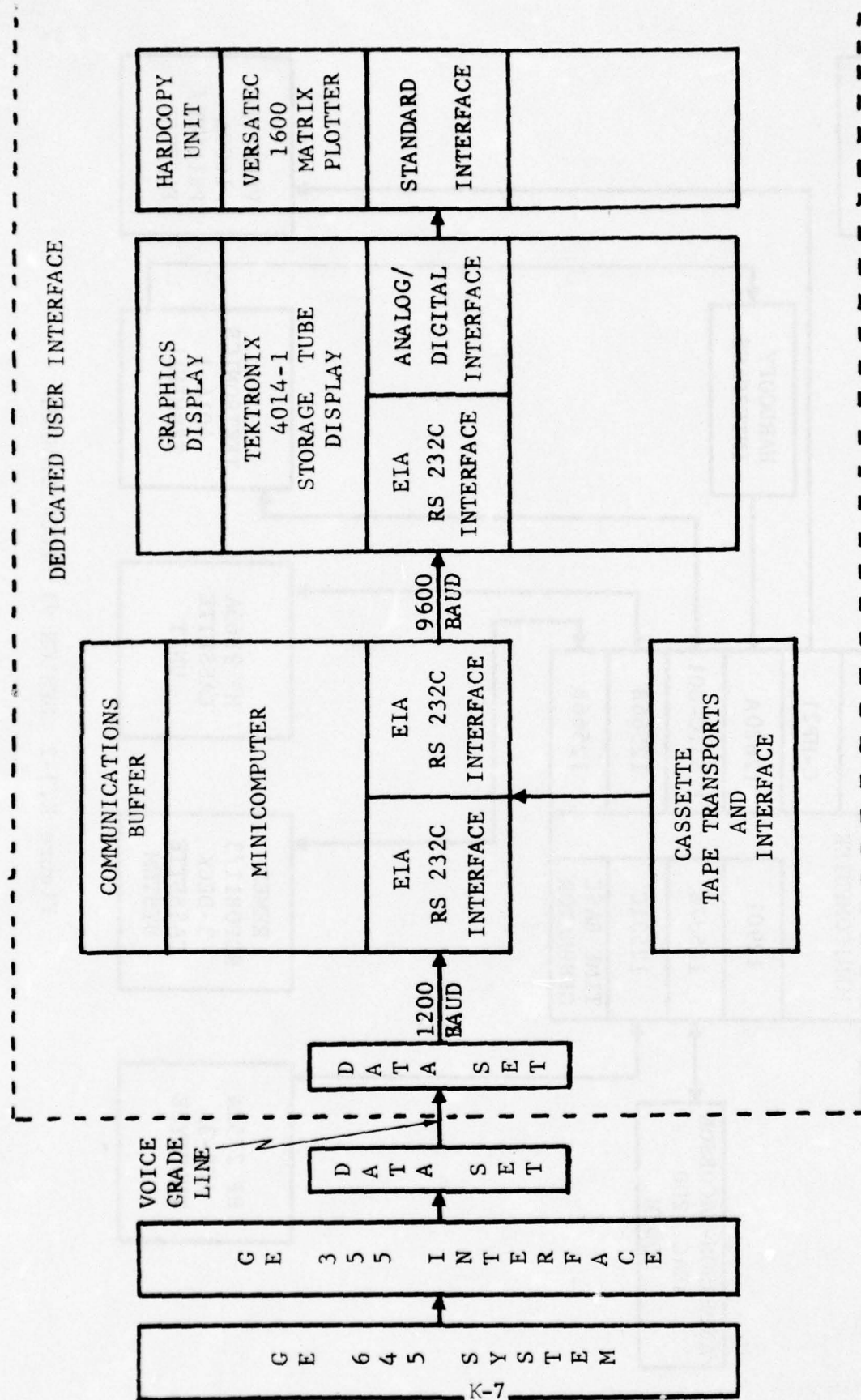


Figure K.3-1 INTERACTIVE RADAR SIMULATOR SYSTEM BLOCK DIAGRAM

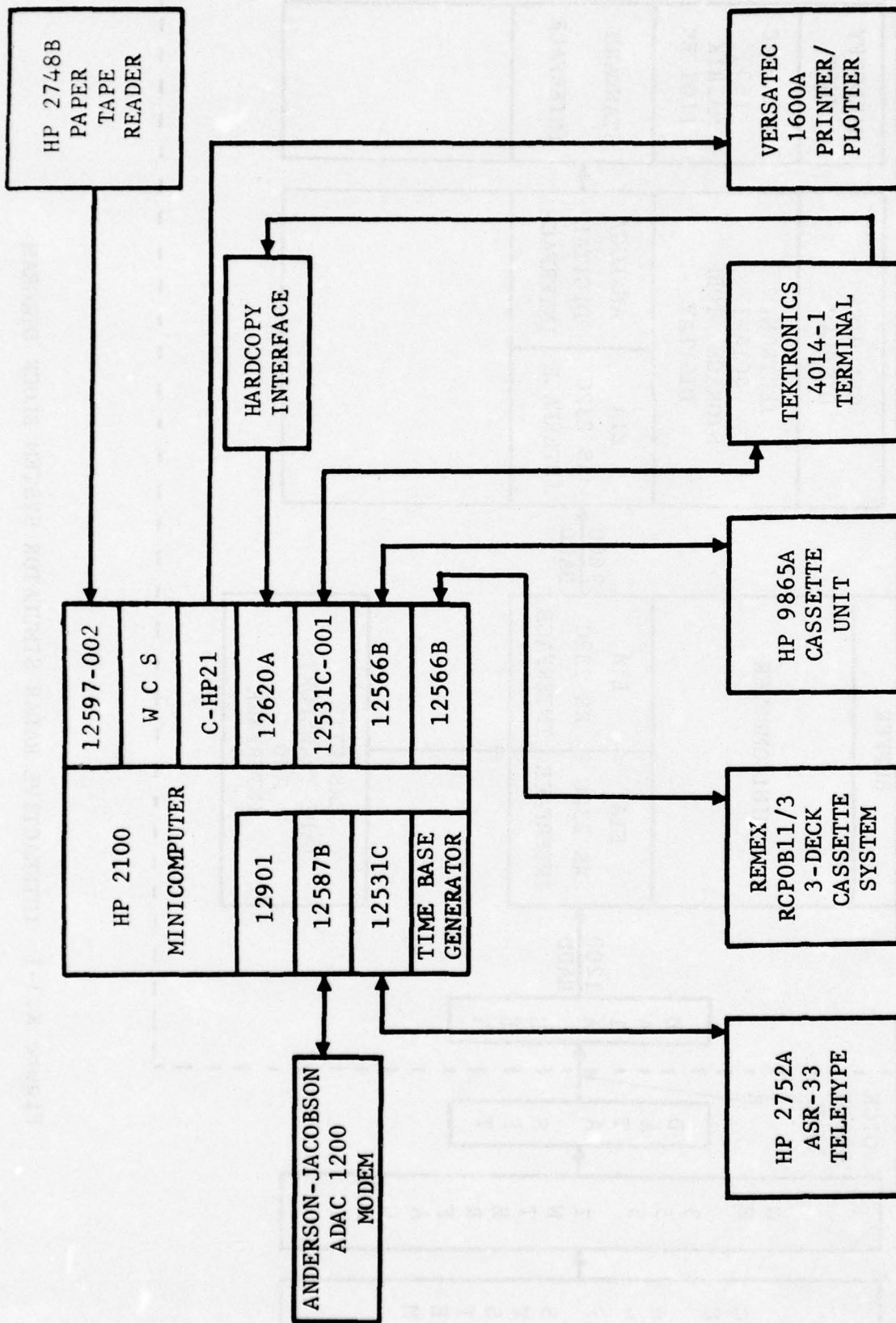


Figure K.3-2 DESIGN #1 BLOCK DIAGRAM

3. 12539C Time base generator to provide timed system interrupts
4. 12908A Write control store for user microprogram development
5. C-HP21 Controller and interface to the Versatec 1600A printer/plotter (this item available from Versatec)
6. 12620A General Purpose interface to hard copy interface unit
7. 12531C-001 Serial asynchronous interface to Tektronix 4014-1 graphics display
8. 12566B General purpose interface for fabricating interface to the Remex Cassette system and to the HP9865A cassette memory unit (2 cards required)
9. 12597-002 General purpose interface to the HP2748B paper tape reader
10. 12901A Floating point hardware.

#### K.3.1.2 Anderson-Jacobson Modem

The A-J Model ADAC 1200 Data coupler transmits and receives data at 1200 baud over the dial-up telephone network by wires through a DAA or acoustically via a telephone handset. The ADAC 1200 is compatible with the Bell System 202C Data Set.

#### K.3.1.3 Teletype

Since the Tektronix display is primarily intended to be a simulation data I/O device, an inexpensive teletype was included in the system to act as an operator's console and also to provide a low speed paper tape punch/read capability.

#### K.3.1.4 Remex Magnetic Tape Cassette

The Remex RCP0B11/3 serves as the bulk storage device of the DUI. By choosing a 3-deck device, one deck can be permanently allocated for operating system and library storage. The remaining two decks will, in general, serve the



same function as the paper tape reader and punch do in other systems. That is, one will normally be the input file to an executing program and the other will be the output file.

#### K.3.1.5 H-P Cassette Unit

In order to allow data transfer between the DUI system and the RADC HP9820A Calculator system, the following approach will be used. An additional interface for the HP2100A must be fabricated which is capable of driving a HP9865A cassette memory unit. In addition, a new software I/O driver must be written to properly format the data written to the cassette. Once accomplished, this will allow the HP9820A Calculator to read tapes generated by the DUI and vice versa.

#### K.3.1.6 Tektronix Display

The Tektronix 4014-1 graphics display is the primary device for information interchange between the computers and the user. This display is available with an extended graphics mode which allows 4096 x 3120 points to be plotted on the display viewing area.

The Tektronix 4014 graphics display is based on a direct view storage tube and requires no local mass storage for display refresh. In addition to the store mode, the Tektronix display has a non-store display capability which is called the write-thru mode. Data presented to the user via this mode is not stored on the tube face and appears only as long as the computer commands it to be displayed. Data presented in this mode must be refreshed approximately thirty times per second.

A capability is provided by Tektronix for scanning the storage tube surface and outputting a video signal which is proportional to intensity. This output video can then be processed and printed by the Versatec printer/plotter. The time required to scan the display face is ten seconds.

#### K.3.1.7 Hard Copy Device

The Versatec 1600A printer/plotter unit will provide for the generation of paper copies of data presented on the Tektronix display. The Versatec printer/plotter is capable of plotting 1600 points across ten inches at the rate of 120 scans/second. In addition to its capabilities as a plotter, the 1600A is useful as a high speed line printer capable of

300 lines/minute. The type font is a 16 x 16 dot matrix. The 96 ASCII character set is standard.

The alternative to specifying the 1600A would be to use the 1600 plotter unit and then perform the ASCII character to dot matrix conversion in the DUI minicomputer. This approach would be more expensive and would increase the processing load on the DUI minicomputer.

The additional one line buffer option is suggested so that a new line of data can be transmitted to the printer/plotter while the previous line is being plotted or printed.

#### K.3.1.8 Hard Copy Interface Unit

The hard copy interface unit converts the video, produced by scanning the graphics display storage surface, into a digital form suitable for input to the Versatec printer/plotter. The operation of this unit is described in the following paragraphs.

The video from the Tektronix display is passed through a threshold device which outputs a binary "1" if the video exceeds the threshold and a binary "0" otherwise. The threshold setting is adjustable so that compensation can be made if video noise level varies. Since the resolution of the Tektronix display is 4096 points and that of the Versatec printer/plotter is 1600 points, a reduction in the resolution of the Tektronix output will be required. Therefore, the output of the threshold must be stretched and then sampled at a rate which corresponds to  $4096/3 = 1365$  samples per scan line, which is within the capabilities of the Versatec printer/plotter. The sampler output is accumulated in a 16-bit serial in/parallel out shift register. When the shift register is filled, the output word is passed to the minicomputer through a Direct Memory Access (DMA) I/O channel.

In the minicomputer, the incoming data words from the hard copy interface are stored in a buffer area which is 1600 bits in length. After a scan line is loaded into the buffer, the hard copy interface is inhibited for the next two scan lines. This must be done to maintain the geometric fidelity of the Tektronix display in producing the hard copy, i.e. both dimensions are reduced by a factor of three. During the dead time, the Versatec unit will request a new scan line and the buffer will be transmitted to the Versatec at the maximum rate of the DMA channel.

The following is a brief analysis of the data rates anticipated in performing the data transfer from the tektronix graphics display to the Versatec hard copy device. The time required to scan the display face containing 3120 lines is 10 seconds. Therefore, 312 lines per second are transmitted to the hard copy interface. The number of samples taken of one scan line is 1365, therefore the 16-bit word rate out of the hard copy interface is given by the following calculation.

$$\begin{aligned}\text{data rate} &= (1365 \text{ samples/line}) \cdot (312 \text{ lines/sec}) / (16 \text{ samples/word}) \\ &= 26618 \text{ words/sec.}\end{aligned}$$

This data rate is easily handled by the minicomputer DMA channel which is capable of over 1 million words/second. Since every third scan line from the display is passed to the hard copy device, the scan line transmission rate out of the hard copy interface will be 104 scans/second. The Versatec plotter is capable of accepting up to 120 scans/second.

In producing a hard copy of the Tektronix graphics display, the DUI minicomputer is used simply for buffer storage.

#### K.3.1.9 Paper Tape Reader

Since Hewlett-Packard software is provided on paper tape a high speed paper tape reader is highly desirable. So an interface should be purchased so that the HP2748B paper tape reader currently in place at RADC (OCSA) can be used with the system.

#### K.3.2 System Design #2

The block diagram of the Design #2 system is shown in Figure K.3-3. The features and parameters of the subsystems which make up this design are discussed in the following paragraphs. The description of those subsystems which are common to both system designs will not be repeated.

Since the DEC CAPS-11 operating system is resident on the DEC cassette unit, a high speed paper tape reader is not needed in this system.

##### K.3.2.1 Digital Equipment Corporation PDP-11/05 Minicomputer

The PDP-11/05 minicomputer is a general purpose machine which is widely used in scientific applications. A summary



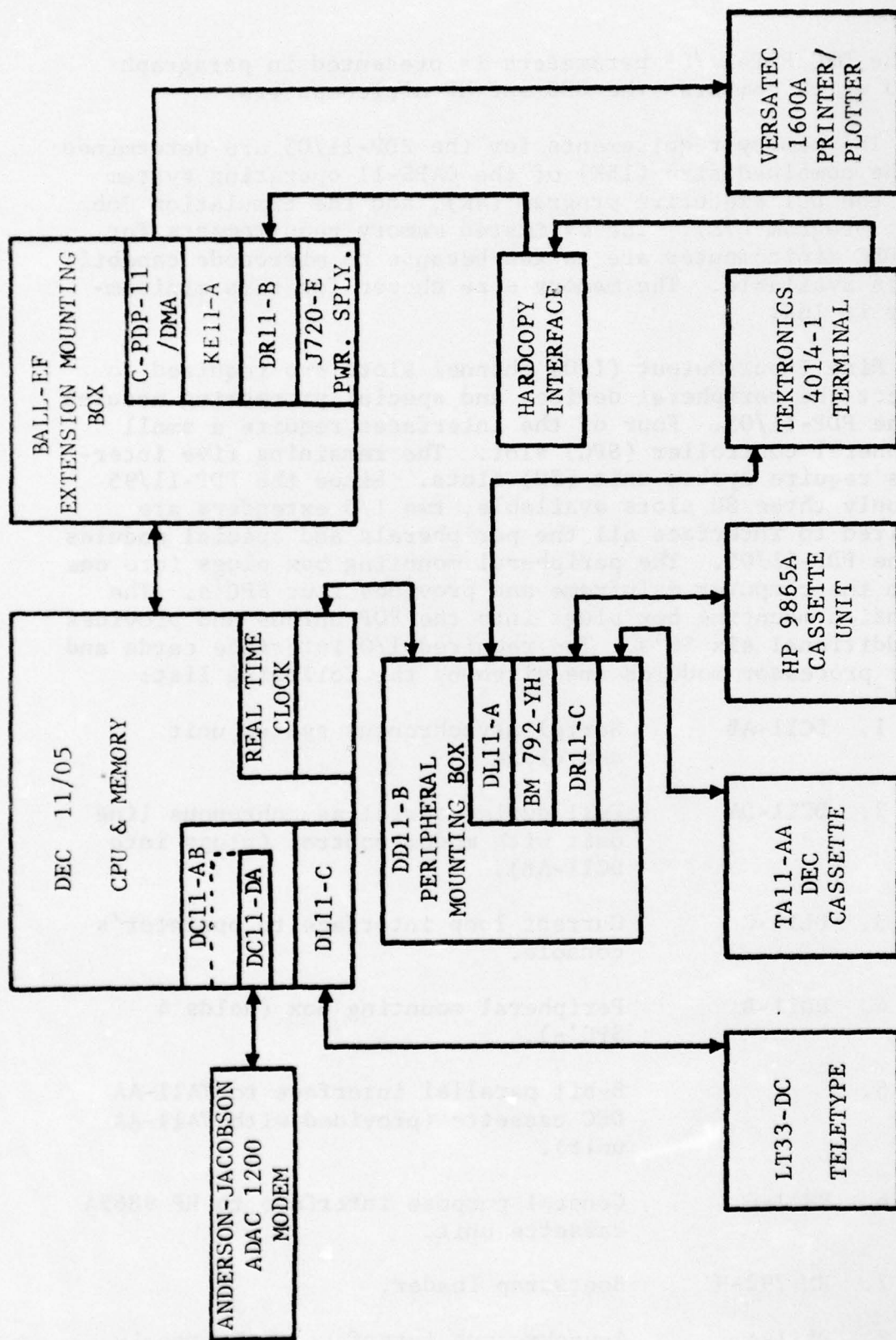


Figure K.3-3 DESIGN #2 BLOCK DIAGRAM

of the DEC PDP-11/05 parameters is presented in paragraph K.3.3 which compares the DEC and HP minicomputers.

The memory requirements for the PDP-11/05 are determined by the combined size (15K) of the CAPS-11 operating system (4K) the DUI executive program (4K), and the Simulation Job Setup program (7K). The estimated memory requirements for the DEC minicomputer are larger because no microcode capability is available. The memory size chosen for this minicomputer is 16K.

Nine Input/Output (I/O) channel slots are required to connect the peripheral devices and special processing modules to the PDP-11/05. Four of the interfaces require a small peripheral controller (SPC) slot. The remaining five interfaces require system unit (SU) slots. Since the PDP-11/95 has only three SU slots available, two I/O extenders are required to interface all the peripherals and special modules to the PDP-11/05. The peripheral mounting box plugs into one SU in the computer mainframe and provides four SPC's. The extension mounting box plugs into the PDP unibus and provides an additional six SU's. The required I/O interface cards and other processor modules are given by the following list:

1. DC11-AB      Serial asynchronous system unit and clock
2. DC11-DA      Full duplex serial asynchronous line unit with modem control (plugs into DC11-AB).
3. DL11-C      Current loop interface to operator's console.
4. DD11-B      Peripheral mounting box (holds 4 SPC's).
5.              8-bit parallel interface to TA11-AA DEC cassette (provided with TA11-AA unit).
6. DR11-C      General purpose interface to HP 9865A cassette unit.
7. BM 792-H      Bootstrap loader.
8. DL11-A      Asynchronous interface to Tektronix 4014-1 graphics display.

- |     |              |   |
|-----|--------------|---|
| 9.  | BA11-EF      | Extension mounting box (holds 6 SU's)   |
| 10. | H720-E       | Power supply for BA11-EF  |
| 11. | DR11-B       | DMA general purpose interface to the hard copy interface unit                                       |
| 12. | C-PDP-11/DMA | Controller and interface to the Versatec 1600A printer/plotter (this item available from Versatec). |

#### K.3.2.2 TA11 DEC Cassette Tape System

The TA11 DEC cassette tape system will serve as the bulk storage device of the DUI.

#### K.3.3 Comparison of Designs

The important difference between the systems are the minicomputer characteristics, therefore the remainder of this paragraph will consider only the minicomputers. In Table K.3-1, some parameters and capabilities of the two minicomputers are listed. The outstanding differences between the devices are the following:

1. The floating point arithmetic operations of the DEC PDP 11/05 are performed by subroutines and therefore are extremely slow compared to the HP2100A which performs these operations with a combination of hardware and microprogramming.
2. The microprogram in the DEC PDP 11/05 is not accessible to the user. The HP2100A is user microprogrammable. The advantages of microprogramming are: increased speed, reduction of memory space required for the program, and flexibility to adapt the instruction set to a particular application.
3. The DEC PDP 11/05, as configured, can be programmed only in assembly language, whereas the HP2100A can be programmed in FORTRAN II and ALGOL as well as assembly language. The ability to use FORTRAN will significantly reduce the programming task and enhance stand-alone capability.
4. Hewlett-Packard maintains a large library of HP contributed and user contributed programs and micro-



Table K.3-1 HP2100A/DEC PDP-11/05 COMPARISON

	<u>HP2100A</u>	<u>DEC PDP-11/05</u>
Maximum Memory (16 bits/wrd)	32K	28K
Memory Cycle Time (ms)	0.980	0.900
Fixed Point Arithmetic (ms)		
Add	1.96	3.7
Multiply	10.7	4.3
Divide	16.7	4.8
Floating Point Arithmetic (ms)		
Add	24-60	376
Multiply	33-41	1017
Divide	52-56	2169
No I/O Channels	14	3
User Microprogrammable.	Yes	No
Programming Languages	FORTTRAN ALGOL Assembly Language	Assembly Language

programs for the 2100 series minicomputers. These programs are available to the user for a small handling charge.

5. The HP2100A is more expensive than the DEC PDP 11/05. The cost of the system configured around the HP minicomputer is approximately 10% higher than the system configured around the DEC minicomputer.

#### K.4 DEDICATED USER INTERFACE SOFTWARE

The new software to be developed and the modification to be performed on the existing RADSIM computer program are described in this subsection. Before proceeding with the software description, it is felt that the philosophy which guided the allocation of tasks between the DUI minicomputer and the host computer should be discussed.

##### K.4.1 Allocation of Processing Tasks

The data processing task of the Interactive Radar Simulator is performed by the DUI minicomputer and the H635 host computer. The pertinent factors to consider are:

1. More storage is available in the H635. However, it should be recognized that although the H635 memory is quite large, 256K, the percentage of this available to a particular user during normal working hours is usually less than 25%.
2. The Central Processing Unit (CPU) of the H635 is faster. Although the H635 CPU is an order of magnitude faster than that of the DUI minicomputer, the H635 CPU is time shared by a number of users. Therefore the difference in speed between the dedicated minicomputer and the time shared H635 will probably be less than a factor of three.
3. The data transferred over the phone line should be minimized. Minimizing connect time should be understood to mean not only the problem of obtaining a channel into the time sharing system, but also the latency of the host computer in servicing the TSS user's requests. Experience has shown that the best approach is to move the desired data out of the machine in the quickest possible manner. If binary data (the most compact form) is transmitted to the DUI this will, of course, increase the load on the DUI minicomputer.
4. The DUI minicomputer is dedicated to the performance of one function, whereas the H635 is time shared by a number of users.



5. Since the RADC host computer is already installed, its resources can be considered to have a very low marginal cost and therefore, in configuring a system, it would be prudent to maximize the use of these resources.

In view of the above factors, especially 1, 2, and 5, the portion of the RADSIM computer program which performs the simulation, i.e., the simulation activity, should be executed by the host computer. The function served by the Simulation Data Loader will be moved to the DUI system. By moving the data initialization function to the DUI, all processing of user input data will be done by the minicomputer off-line and the data in a compact form, will then be passed to the host computer over the phone line. This will minimize the amount of data passed over the phone line during job submission.

In the case of the plot programs, the trade offs are not as clear-cut. If minimizing connect time is important, it would be preferable to have the plotter programs executed by the DUI minicomputer with data from the host computer transmitted in binary form. The binary data would then be recorded on magnetic tape cassette and processed for plotting by the DUI minicomputer at a later time. The disadvantage of this approach is that the Tektronix plotter software packages (Terminal Control System (TCS), Advanced Graphics-II (AG-II) and Cal Comp Preview) require more core space than is available in the DUI minicomputer. Therefore, a plotter program executed by the DUI minicomputer could not have all the features provided in the Tektronix software package. An additional advantage of this approach is that since job output data are stored on tape cassette, the data can be reused a number of times in any manner desired by user.

On the other extreme, the simulation output data would be processed by plot programs in the H635. The data transmitted to the DUI would then be in the form of commands to the Tektronix display. The disadvantage of this is that connect time to the host computer will be longer and the data received will be usable by the Tektronix display only. Rather than compromise between these two approaches, the system should be configured such that either technique can be used. If the user wants only a basic plot capability, the plot program in the DUI minicomputer will suffice. For more complicated work, the user will have the full Tektronix software package in the H635 available to him.

In addition to the above, a mode of operation should be included whereby the user can have tabular data transmitted to the DUI under format control and printed by the hard copy device. This will be useful for retrieving tabular output data or program listings. If the user desires only to view the data and requires no hard copy, then the data can be displayed on the Tektronix display. The remainder of the subsection contains a description of the new software to be developed or purchased and the modification to be performed on the existing radar system simulation model.

#### K.4.2 Communications Buffer Executive

The communications Buffer Executive program (EXEC) executed by the DUI minicomputer serves as a "data traffic cop." The EXEC supervises all input/output operations, provides linkage to job set up routines and plot programs, determines which tasks have the highest priority, handles user requests/answers and system answers/requests.

#### K.4.3 Radar System Simulation Model

The modifications to be performed on the Radar System Simulation Model (RADSIM) are the following:

1. Develop a new Simulation Data Loader computer program which will accept the job definition file from the DUI system and load the data into a permfile.
2. Modify the existing Simulation Data Loader computer program to write its output data into a permfile instead of to system allocated public disc space. This will be done so that RADSIM can still be available to non-DUI users.
3. Develop a new Data Retrieval computer program which reads simulation output data from permfile, processes it according to mode selected by the user and then transmits the data to the DUI system. The Terminal Control System and Advanced Graphics-II plot programs available from Tektronix should be included in this computer program.

The portion of RADSIM which performs the simulation is unchanged. Therefore, it is not degraded in any way by the addition of the DUI system.



#### K.4.4 Plot Programs

The programs for converting the simulation output data to a form compatible with the graphics display are available from Tektronix. Some modification of the Tektronix software to be installed on the H635 will be required since it is written for computers having 8-bit bytes and the RADC computer utilizes 9-bit bytes when operating in TSS mode.

The plot program for installation in the DUI minicomputer is also available from Tektronix. This program should require no modification.

The program for generating a hard copy of the Tektronix display will have to be developed. This program will issue commands to the graphics display to start the read scan of the storage surface, accept output data from the hard copy interface and store it in a buffer area, and output the data to the Versatec printer/plotter at the appropriate time.

Since the Versatec printer/plotter is essentially slaved to the Tektronix graphics display for plot hard copy generation there will be no plotter software required for the Versatec printer/plotter.

#### K.4.5 Simulation Job Setup Program

The computer program for the minicomputer which assists the user in the setting up of a simulation job is, for the most part, composed of four subprograms. These are briefly described in the following paragraphs.

##### K.4.5.1 Job Setup Controller

This subprogram serves as the supervisor of all operations performed during the job setup procedure. The Job Setup Controller asks questions of the user, accepts and processes the user answers, and passes commands to the appropriate subprograms.

##### K.4.5.2 Block Diagram Generator

This subprogram processes the information provided by the user and outputs the necessary commands to cause a block diagram to be formed on the graphics display. The user provides the tabular data for identification of modules through



the graphics display keyboard and the positional data for the location of blocks through the graphics display cursors.

#### K.4.5.3 Job Definition File Generator

The input data to this subprogram is basically the same as that provided the Block Diagram Generator, but the output is in a form that is compatible with the simulation program executed by the host computer. The structure of this data will be the same as the output data from the current Data Initialization activity. The Job Definition File which is the output from this subprogram is written onto a magnetic tape cassette. The tape cassette will then be the user's record of the input data for the simulation to be performed. A pictorial representation of the recommended data structure on the tape is shown in Figure K.4-1. The simulation job represented in this figure is composed of two configurations. The first configuration is to be executed twice for two sets of input data. The second configuration is to be executed only once.

#### K.4.5.4 RADSIM Catalog and Data Retrieval

As part of the Job Setup Program development effort, all data associated with the RADSIM computer program pertinent to the process of job definition should be cataloged and stored on a tape cassette. During the process of job setup, the user may at any time request that data from this file be presented either on the graphics display in the scratch pad area, or printed on the operator's console.

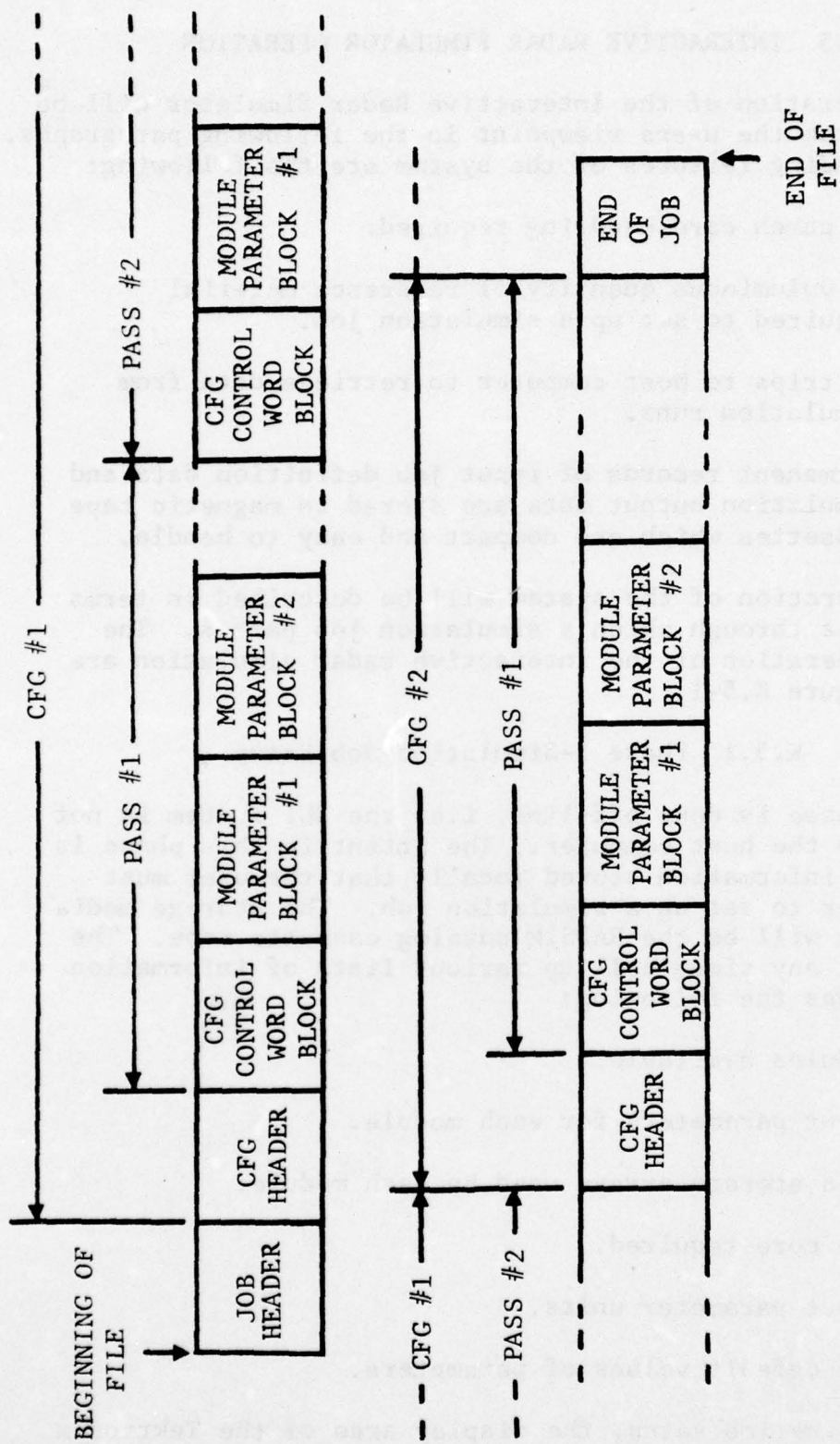


Figure K.4-1 JOB DEFINITION FILE STRUCTURE

## K.5 INTERACTIVE RADAR SIMULATOR OPERATION

The operation of the Interactive Radar Simulator will be described from the users viewpoint in the following paragraphs. Four outstanding features of the system are the following:

1. No punch card handling required.
2. No voluminous quantity of reference material required to set up a simulation job.
3. No trips to host computer to retrieve data from simulation runs.
4. Permanent records of input job definition data and simulation output data are stored in magnetic tape cassettes which are compact and easy to handle.

The operation of the system will be described in terms of the phases through which a simulation job passes. The phases of operation of the interactive radar simulation are shown in Figure K.5-1.

### K.5.1 Phase I-Simulation Job Setup

This phase is done off-line, i.e. the DUI system is not connected to the host computer. The intent in this phase is to have all information stored locally that the user must know in order to set up a simulation job. The storage media for the data will be the RADSIM catalog cassette tape. The user can, at any time, call up various lists of information which includes the following:

1. Modules available.
2. Input parameters for each module.
3. Data storage arrays used by each module.
4. The core required.
5. Input parameter units.
6. The default values of parameters.

During the job setup, the display area of the Tektronix graphics display is divided into two areas, a scratch pad



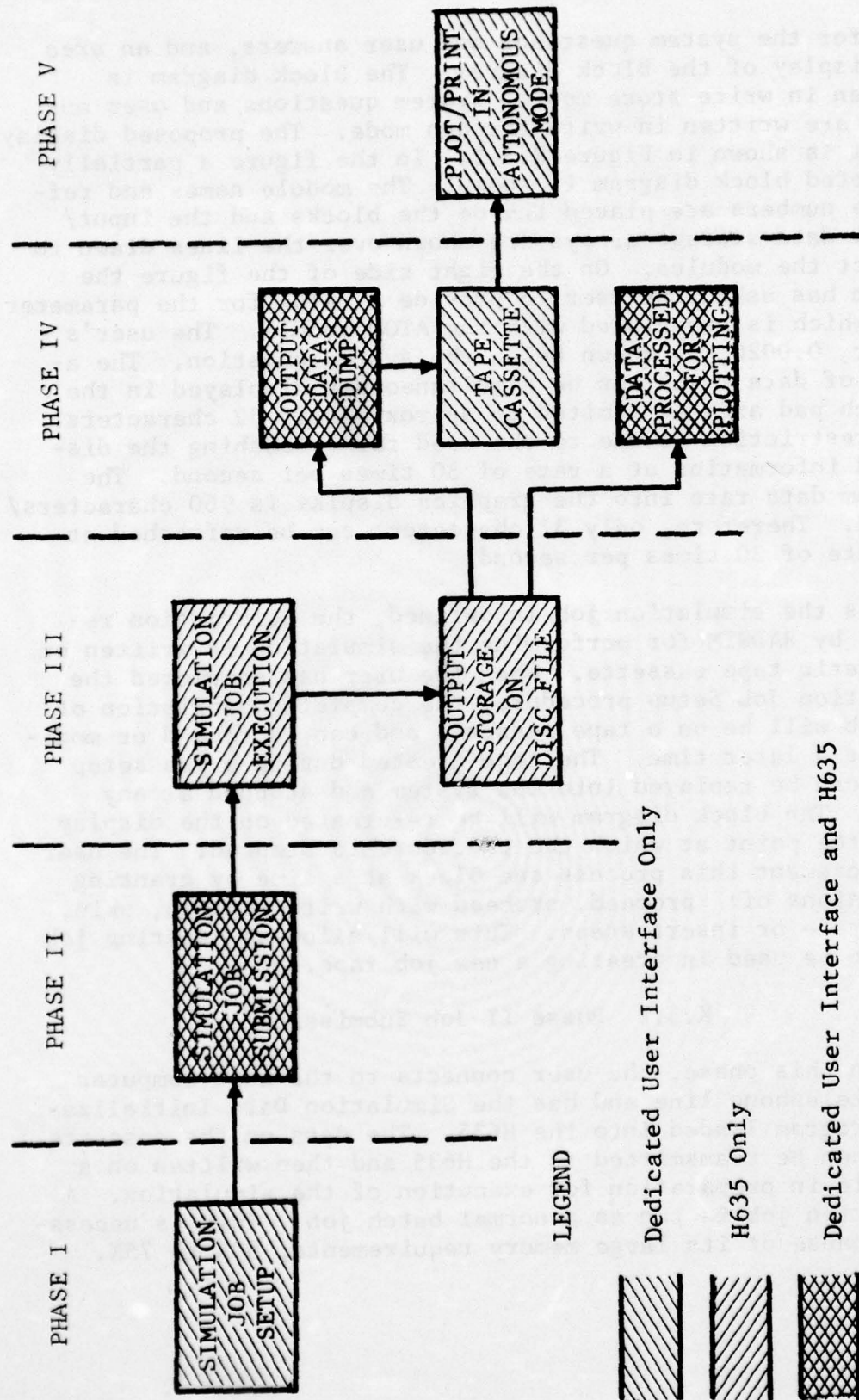


Figure K.5-1 INTERACTIVE RADAR SIMULATOR FUNCTIONAL BLOCK DIAGRAM

area for the system questions and user answers, and an area for display of the block diagram. The block diagram is written in write store mode. System questions and user answers are written in write-through mode. The proposed display layout is shown in Figure K.5-2. In the figure a partially completed block diagram is shown. The module names and reference numbers are placed inside the blocks and the input/output data storage arrays are shown over the lines drawn to connect the modules. On the right side of the figure the system has asked the user to provide a value for the parameter, LSB, which is associated with the ATOD module. The user's answer, 0.0020, is shown below the system question. The amount of data which can be simultaneously displayed in the scratch pad area is limited to approximately 32 characters. This restriction is due to the need for refreshing the displayed information at a rate of 30 times per second. The maximum data rate into the graphics display is 960 characters/second. Therefore, only 32 characters can be refreshed at the rate of 30 times per second.

As the simulation job is defined, the information required by RADSIM for performing the simulation is written on a magnetic tape cassette. When the user has completed the Simulation Job Setup procedure, the complete description of the job will be on a tape cassette and can be reused or modified at a later time. The tape created during a job setup phase can be replayed into the system and stopped at any point. The block diagram will be re-created on the display up to the point at which the procedure is stopped. The user may increment this process one block at a time by granting permissions of: proceed, proceed with write through, skip, substitute or insert steps. This will allow an existing job tape to be used in creating a new job tape.

#### K.5.2 Phase II-Job Submission

In this phase, the user connects to the host computer via a telephone line and has the Simulation Data Initialization program loaded into the H635. The data on the cassette will then be transmitted to the H635 and then written on a permfile in preparation for execution of the simulation. A simulation job is run as a normal batch job. This is necessary because of its large memory requirements, 60K to 75K.

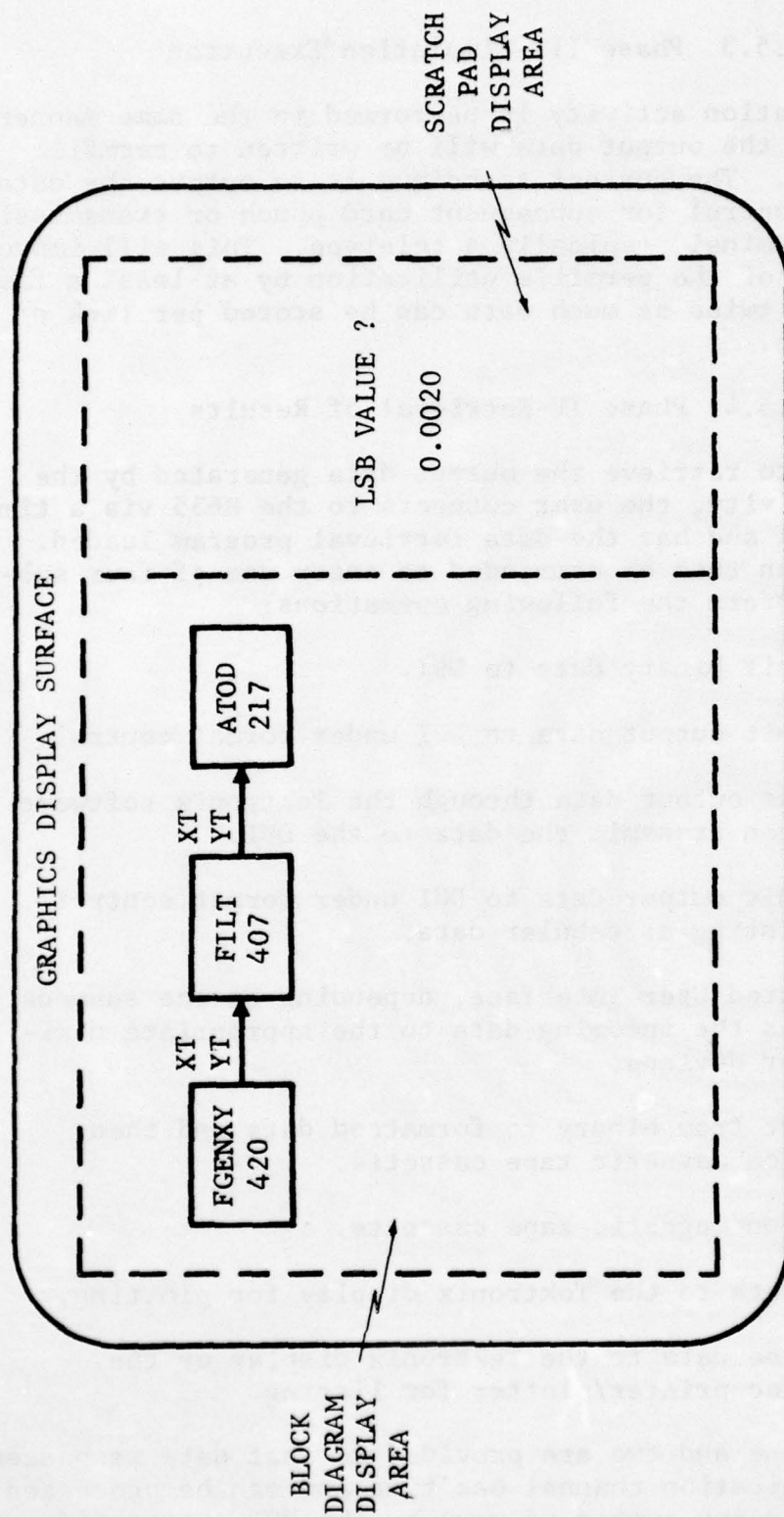


Figure K.5-2 DISPLAY DURING SIMULATION JOB SETUP



AD-A031 480

GENERAL DYNAMICS FORT WORTH TEX CONVAIR AEROSPACE DIV F/G 17/9  
ENDO ATMOSPHERIC-EXO ATMOSPHERIC RADAR MODELING. APPENDICES, A---ETC(U)  
JUN 76 R J HANCOCK, F H CLEVELAND F30602-73-C-0380

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### K.5.3 Phase III-Simulation Execution

The simulation activity is performed in the same manner as now, except the output data will be written to permfile in binary form. The current technique is to output the data under format control for subsequent card punch or transmission to a remote terminal, typically a teletype. This will improve the efficiency of the permfile utilization by at least a factor of 2, i.e. twice as much data can be stored per link of disc file space.

### K.5.4 Phase IV-Retrieval of Results

In order to retrieve the output data generated by the simulation activity, the user connects to the H635 via a time sharing channel and has the data retrieval program loaded. This program can then be commanded to enter one of four submodes which perform the following operations:

1. Transmit binary data to DUI.
2. Transmit output data to DUI under format control.
3. Process output data through the Tektronix software and then transmit the data to the DUI.
4. Transmit output data to DUI under format control for listing as tabular data.

The Dedicated User Interface, depending on the submode selected, passes the incoming data to the appropriate peripheral device or devices.

1. Convert from binary to formatted data and then store on magnetic tape cassette.
2. Store on magnetic tape cassette.
3. Pass data to the Tektronix display for plotting.
4. Pass the data to the Tektronix display or the Versatec printer/plotter for listing.

Submodes one and two are provided so that data is passed over the communication channel one time and can be processed and displayed in any number of ways by the DUI system off-line from the host computer. The disadvantage associated

with this is that the DUI plot programs will not have as much capability as the H635 plot programs.

#### K.5.5 Phase V-Autonomous Operation

In addition to serving as the user's interface of the Interactive Radar Simulator, the DUI system can be operated as a stand-alone minicomputer system. RADC personnel who are familiar with FORTRAN can easily make the transition to the computer system configured about the 2100A, i.e. the Design #1 system. The transition to the DEC 11/05 offered in Design #2 will not be as simple since the DEC system will not support a FORTRAN compiler and must therefore be programmed in assembly language. The following two items available from Hewlett-Packard would significantly enhance the stand-alone capabilities of the Design #1 system:

- HP12907A - Fast FORTRAN Processor (Scientific Instruction Set). This board plugs into an I/O slot and provides 13 microcoded subroutines which greatly enhance the through-put efficiency of FORTRAN and other high level languages.
- HP12892A - Memory Protect Fence. This board plugs into the memory section and aids the operating system in running multiple programs.

The addition of a 7 or 9 track magnetic tape transport or a disc subsystem should be considered if the number of autonomous progressing jobs are sufficient to justify the cost.



A P P E N D I X   L

R A D A R   C R O S S   S E C T I O N

A N A L Y T I C   M O D E L   D E S C R I P T I O N S

Published in Part 2 of this volume.

APPENDIX M  
HEWLETT PACKARD 9820A  
COMPUTER PROGRAM FOR PLOTTING  
FILTER TRANSFER FUNCTIONS

M.1 INTRODUCTION

The S-domain transfer function for a general filter can be represented by the ratio of two polynomials as shown in the following expression

$$H(S) = \frac{(S-Z_1)(S-Z_2)(S-Z_3) \dots (S-Z_{NZ})}{(S-P_1)(S-P_2)(S-P_3) \dots (S-P_{NP})} \cdot SF$$

where:

$Z_i$  represents the  $i^{\text{th}}$  complex zero,

$P_i$  represents the  $i^{\text{th}}$  complex pole and

SF is a scale factor.

The frequency units used in the expression above can be any frequency; i.e., KHz, MHz, GHz etc. as long as all inputs are consistent in the same units.

M.2 PROGRAM OPERATION

The filter program plots the baseband filter impulse response based on normalized pole-zero locations. The program can be used to plot magnitude in either voltage vs. frequency or power in dB vs. frequency. The theory of operation is shown on page 4-61 of the RADSIM report Vol. II, Part 1. The following are the user supplied inputs required by the program:

1. BYPASS - Flag set to zero or one; a value of one indicates that the user desires to key in the plot parameters such as frequency range and magnitude of impulse response for plotting; a value of zero indicates that the previous set of plot parameters are to be used for the next plot.

2. FSTART - Starting frequency for plot (frequency Hz, KHz, MHz, etc.)
3. FSTOP - Ending frequency for plot (frequency Hz, KHz, MHz, etc.)
4. LOG PLOT - Flag set to zero or one; zero indicates the magnitude of the impulse response will be plotted in units of voltage vs. frequency; one indicates a plot of dB power vs. frequency.
5. TOP - Maximum magnitude to be plotted (volts or dB).
6. BOTTOM - Minimum magnitude to be plotted (volts or dB).
7. INPUT - Flag set to zero or one; zero indicates use same pole zero locations as for previous plot; one indicates that new pole zero locations are to be entered.
8. NO. POLES - Number of poles to be entered.
9. NO. ZEROES - Number of zeroes to be entered.
10. SCALE - Scale factor: used to normalize magnitude of impulse response to unity.
11. POLE-R - Real part of complex pole.
12. I - Imaginary part of complex pole.
13. ZERO-R - Real part of complex zero.
14. I - Imaginary part of complex zero.

Once all the required input data has been supplied by the user, the filter impulse response is plotted; however, no axes will be drawn or labeled. All inputs are listed on the HP9820 calculator printer so that the user may label the plot if desired. Tables of normalized pole-zero locations for Chebyshev filters are listed in Volume IV, Part 1, Appendix E.



### M.3 SAMPLE PROBLEM

The following sample problem will be a plot of the impulse response of a six pole Chebyshev filter with 0.1 dB ripple. The HP9820 calculator printer listing which shows user supplied inputs is shown in Figure M.3-1.

The output impulse response plotted in volts vs. frequency is shown in Figure M.3-2 and in dB vs. frequency is shown in Figure M.3-3. The axes and labels have been done by the user based on the input listing shown in Figure M.3-1.

### M.4 HOW TO USE THE FILTER PROGRAM RESULTS WITH RADSIM

The primary purpose of running the filter program is to generate accurate input data for RADSIM and in particular for Module FILT in RADSIM. This subroutine simulates a continuous filter which is defined by an S-domain polynomial transfer function.

When executing FILT, the user must use the impulse response in terms of voltage vs. frequency. The amplitude must be normalized to unity gain and the pole-zero locations must be modified to reflect the desired bandwidth of the filter to be used in the simulation job.

Suppose the input job stream, for this example, has been set up to reflect consistent frequency inputs in gigahertz (GHz) and time inputs in nanoseconds (ns). The frequency scale in Figures M.3-2 and M.3-3 is now constrained to units in GHz. Suppose that the desired six-pole Chebyshev filter with 0.1 dB ripple has a 3 dB bandwidth of 50 MHz and unity gain at the peak of the impulse response. The following procedure would be used to modify the pole-zero locations to reflect the desired 50 MHz 3 dB bandwidth and to calculate a scale factor (SF) to normalize the peak of the impulse response to unity. In Figure M.4-1 the 3 dB bandwidth extends from -1 GHz to +1 GHz. If a lowpass filter is to be simulated, the 3 dB bandwidth would extend from DC (0 frequency) to 1 GHz; however, for a bandpass filter, the bandwidth will be measured symmetrically about zero. To modify the pole locations, the following procedure is used.

1>X1	1.00000	BYPASS
1		
-3>R451	-3.00000	FSTART
3>R461	3.00000	FSTOP
1>R471	10000	FI
0>R701	0.00000	LOG PLOT
2		
10>R541	10.00000	TOP
0>R551	0.00000	BOTTOM
FILE		
6>R431	6.00000	NO. POLES
0>R441	0.00000	NO. ZEROES
1>R511	1.00000	SCALE
19		
-10494112>R11	-10494	Real part of first complex pole
96668431>R12+10	96668	Imaginary part of first complex pole
2.00000		
19		
-10494112>R11	-10494	} 2nd complex pole
-96668431>R12+10	-96668	
4.00000		
19		
-28670448>R21	-28670	} 3rd complex pole
70766203>R22+10	70766	
6.00000		

Figure M.3-1 HP9820 LISTING SHOWING FILTER PROGRAM INPUTS

19	- 28670448→RZF	}	4th complex pole
	- 28670		
	- 78766200→R(Z+1		
	- 78766		
	8.00000		
19	- 39164560→RZF	}	5th complex pole
	- 39165		
	25902228→R(Z+1		
	25902		
	10.00000		
19	- 39164560→RZF	}	6th complex pole
	- 39165		
	- 25902228→R(Z+1		
	- 25902		
	12.00000		
20			
22	20.00000		

Figure M.3-1 HP9820 LISTING SHOWING FILTER PROGRAM INPUTS (Cont.)



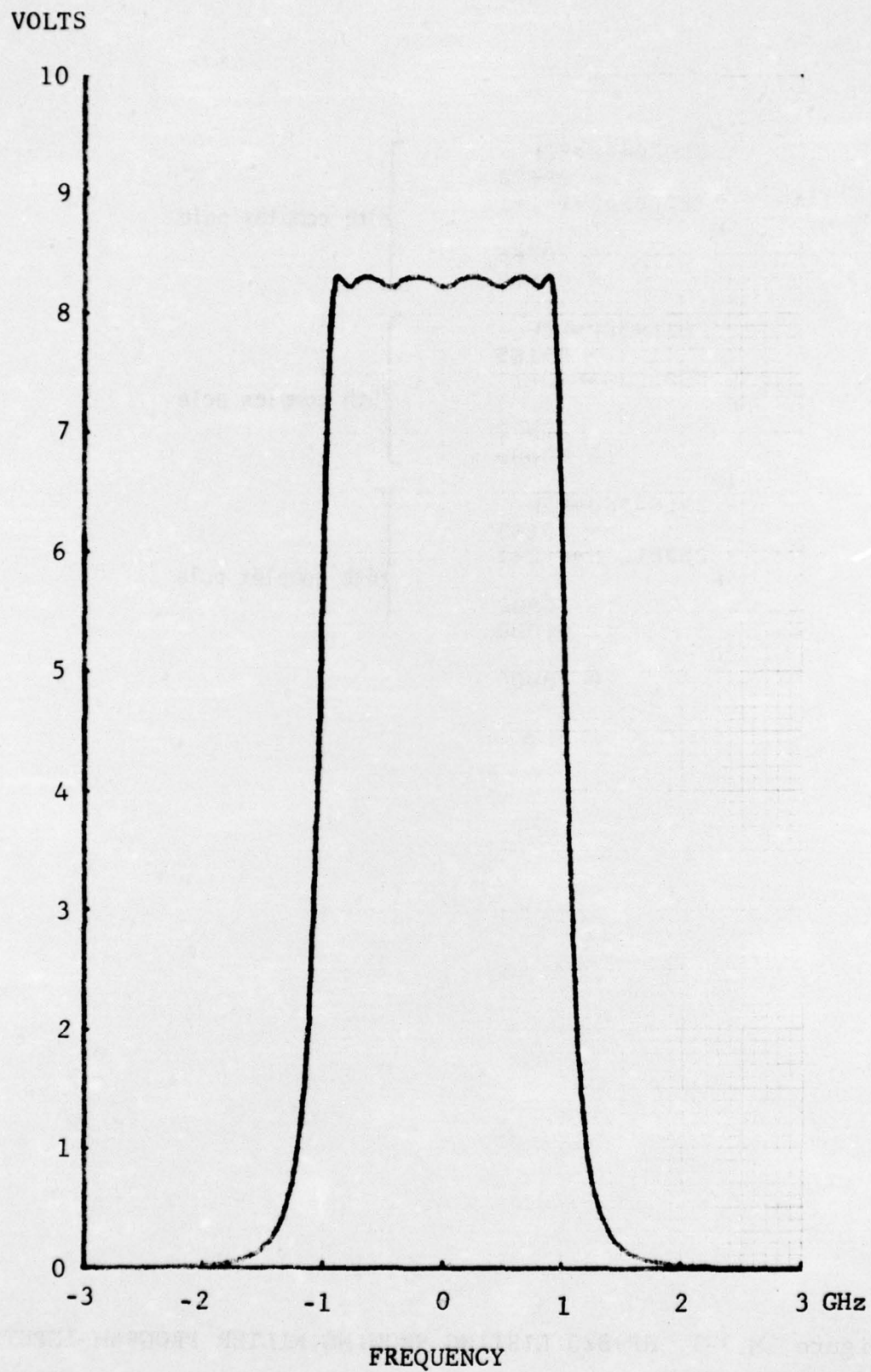


Figure M.3-2 6-POLE CHEBYSHEV FILTER, 0.1 dB RIPPLE

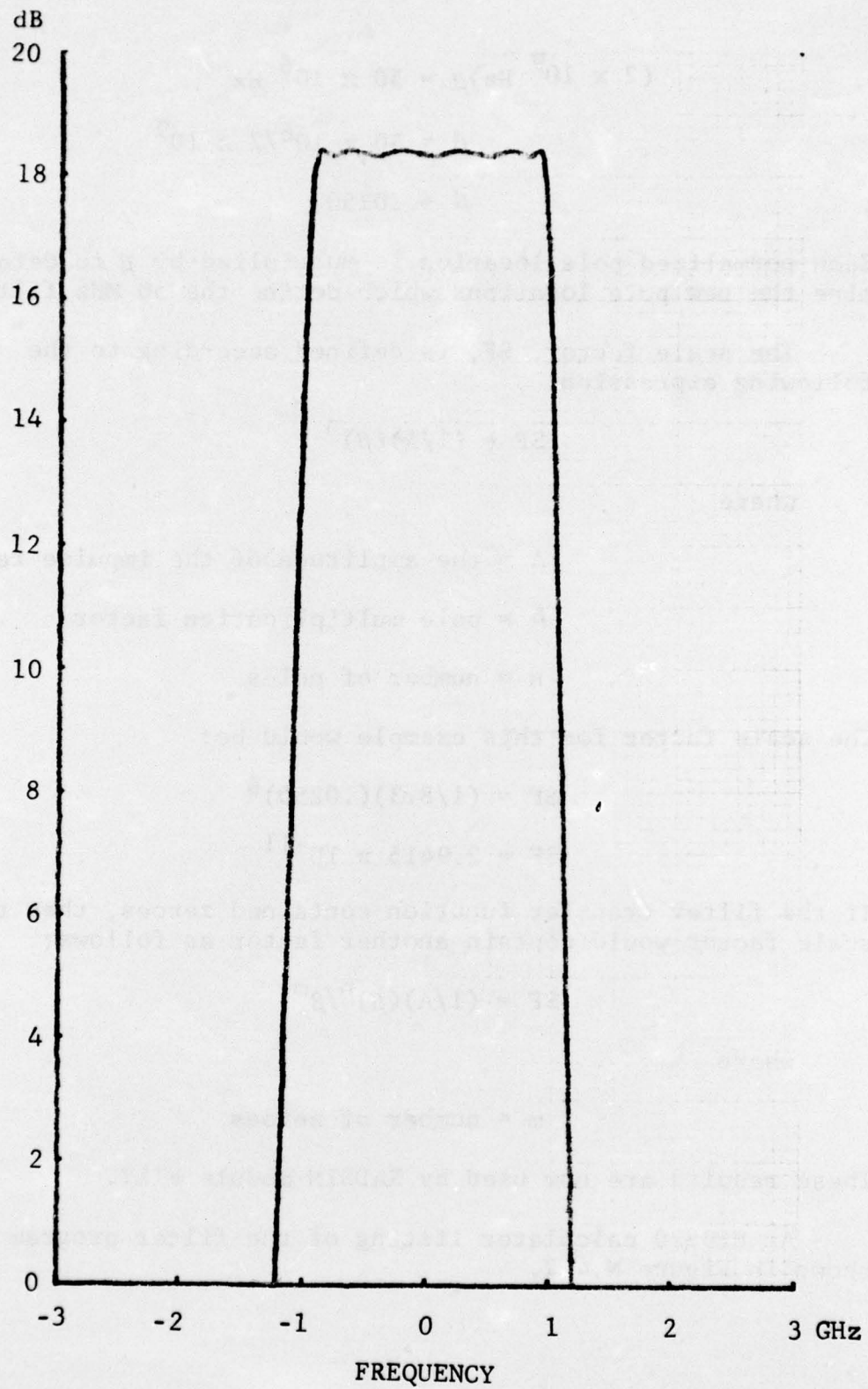


Figure M.3-3 6-POLE CHEBYSHEV FILTER, 0.1 dB RIPPLE

$$(2 \times 10^9 \text{ Hz})\beta = 50 \times 10^6 \text{ Hz}$$

$$\beta = 50 \times 10^6 / 2 \times 10^9$$

$$\beta = .0250$$

Each normalized pole location is multiplied by  $\beta$  to determine the new pole locations which define the 50 MHz filter.

The scale factor, SF, is defined according to the following expression.

$$SF = (1/A)(\beta)^n$$

where

A = the amplitude of the impulse response

$\beta$  = pole multiplication factor

n = number of poles

The scale factor for this example would be:

$$SF = (1/8.3)(.0250)^6$$

$$SF = 2.9415 \times 10^{-11}$$

If the filter transfer function contained zeroes, then the scale factor would contain another factor as follows:

$$SF = (1/A)(\beta)^n/\beta^m$$

where

m = number of zeroes

These results are now used by RADSIM module FILT.

An HP9820 calculator listing of the filter program is shown in Figure M.4-2.



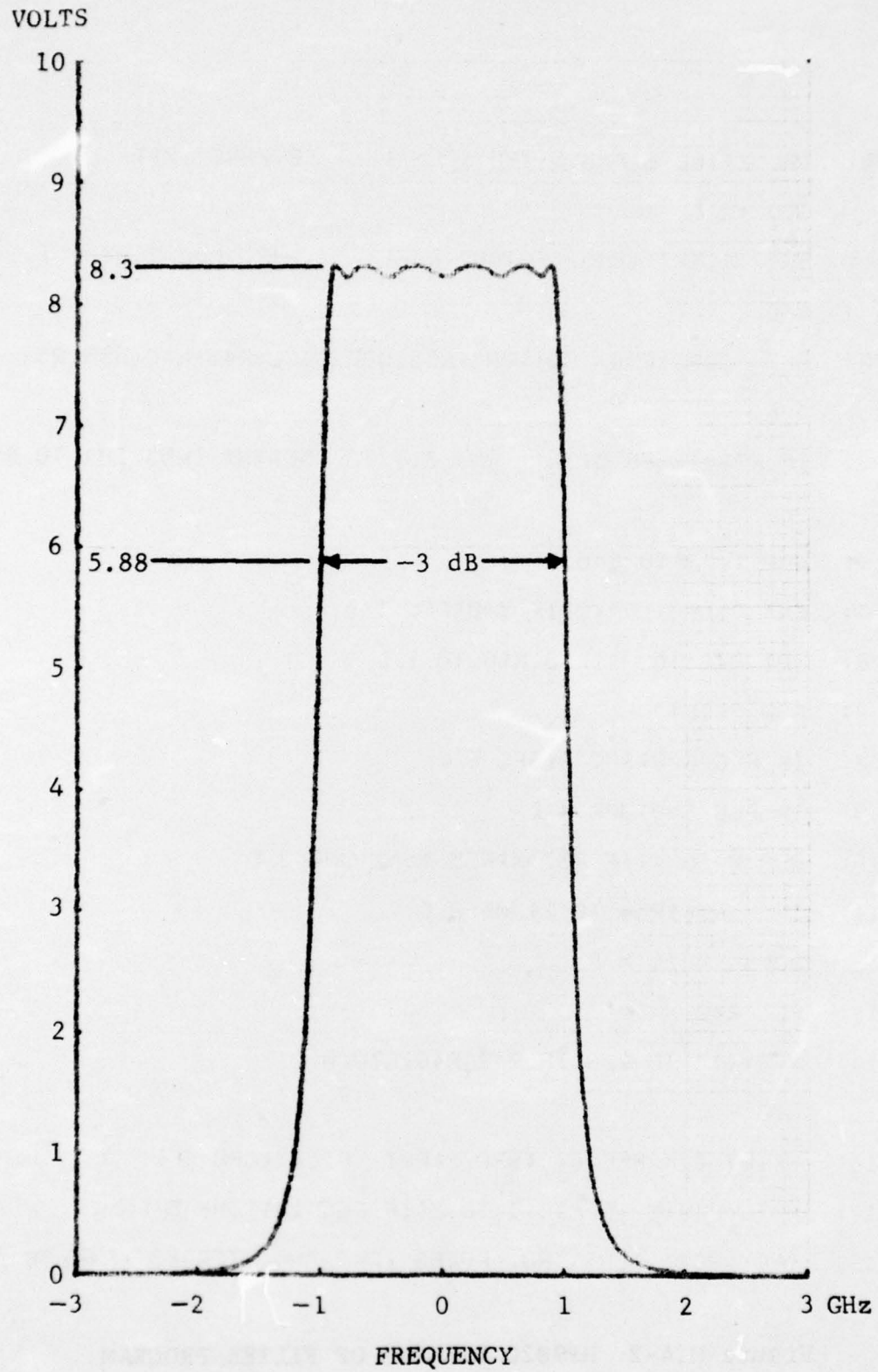


Figure M.4-1 6-POLE CHEBYSHEV FILTER, 0.1 dB RIPPLE

```

0:  TBL 3:TBL 6:FXD 5:TRC :PEN :ENT "BYPASS":X:IF X=0:
    GTO +3 [
1:  ENT "FSTRT",R45,"FSTOP",R46,"FI",R47,"LOG PLOT ?",
    R70 [
2:  ENT "TOP",R54,"BOTTOM",R55:NOR :SCL R45,R46,R55,R5
    4 [
3:  IF R70=1:SFG 5:TH+ (R54/20) TO R56:TH+ (R55/20) TO R57
    [
4:  NOR :R45 TO R48 [
5:  ENT "INPUT ?",Y:IF Y=0:SFG 1 [
6:  PI R48 TO R:1 TO X:0 TO Y [
7:  GSB "FILT" [
8:  IF FLG 6=0:SPC 3:SFG 6 [
9:  IF FLG 5=0:JMP 4 [
10: ABS X TO X:IF R57>X:R55 TO X:JMP 3 [
11: IF X>R56:R54 TO X:JMP 2 [
12: 20LOG X TO X [
13: PLT R48,X [
14: R48+R47 TO R48:IF R48>R46:GTO 0 [
15: GTO 6 [
16: "FILT":IF FLG 6=0:SPC 2:PRT "FILT":SPC 1 [
17: X TO R49:Y TO R50:0 TO Z:IF FLG 1=1:JMP 5 [
18: TRC :SFG 1:ENT "NO. POLES",R43,"NO. ZEROES",R44,"S

```

Figure M.4-2 HP9820 LISTING OF FILTER PROGRAM

```

19: ENT "POLE - R",RZ,"I",R(Z+1);Z+2 TO Z;JMP Z=2R43 [
20: 20 TO Z;JMP (R44=0)+1 [
21: ENT "ZERO - R",RZ,"I",R(Z+1);Z+2 TO Z;JMP Z=2R44 20 [
22: NOR ;0 TO C TO Z;1 TO B;IF R43=0;JMP 3 [
23: -RZ TO X;R48-R(Z+1) TO Y;GSB "POL" [
24: B/X TO B;C-Y TO C;Z+2 TO Z;IF 2R43>Z;JMP -1 [
25: 20 TO Z;IF R44=0;JMP 3 [
26: -RZ TO X;R48-R(Z+1) TO Y;GSB "POL" [
27: XB TO B;C-Y TO C;Z+2 TO Z;IF 2R44>Z-20;JMP -1 [
28: BR49R53 TO X;C+R50 TO Y;RET [
29: "POL";IF Y=0;ABS X TO X;RET [
30: IF X=0;ABS Y TO X;PI Y/2X TO Y;RET [
31: ATN (X/Y) TO R52; SQR (XX+YY) TO X;R52 TO Y;RET [
32: END [

```

**Figure M.4-2 HP9820 LISTING OF FILTER PROGRAM**



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